

A New Equation of State for Carbon Dioxide Covering the Fluid Region from the Triple- Point Temperature to 1100 K at Pressures up to 800 MPa

Cite as: Journal of Physical and Chemical Reference Data **25**, 1509 (1996); <https://doi.org/10.1063/1.555991>

Submitted: 25 May 1994 . Published Online: 15 October 2009

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A New Equation of State for Carbon Dioxide Covering the Fluid Region from the Triple-Point Temperature to 1100 K at Pressures up to 800 MPa

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Received 25 May 1994

This work reviews the available data on thermodynamic properties of carbon dioxide and presents a new equation of state in the form of a fundamental equation explicit in the Helmholtz free energy. The function for the residual part of the Helmholtz free energy was fitted to selected data of the following properties: (a) thermal properties of the single-phase region ($p\rho T$) and (b) of the liquid-vapor saturation curve (p_s , ρ' , ρ'') including the Maxwell criterion, (c) speed of sound w and (d) specific isobaric heat capacity c_p of the single phase region and of the saturation curve, (e) specific isochoric heat capacity c_v , (f) specific enthalpy h , (g) specific internal energy u , and (h) Joule-Thomson coefficient μ . By applying modern strategies for the optimization of the mathematical form of the equation of state and for the simultaneous nonlinear fit to the data of all these properties, the resulting formulation is able to represent even the most accurate data to within their experimental uncertainty. In the technically most important region up to pressures of 30 MPa and up to temperatures of 523 K, the estimated uncertainty of the equation ranges from $\pm 0.03\%$ to $\pm 0.05\%$ in the density, $\pm 0.03\%$ to $\pm 1\%$ in the speed of sound, and $\pm 0.15\%$ to $\pm 1.5\%$ in the isobaric heat capacity. Special interest has been focused on the description of the critical region and the extrapolation behavior of the formulation. Without a complex coupling to a scaled equation of state, the new formulation yields a reasonable description even of the caloric properties in the immediate vicinity of the critical point. At least for the basic properties such as pressure, fugacity, and enthalpy, the equation can be extrapolated up to the limits of the chemical stability of carbon dioxide. Independent equations for the vapor pressure and for the pressure on the sublimation and melting curve, for the saturated liquid and vapor densities, and for the isobaric ideal gas heat capacity are also included. Property tables calculated from the equation of state are given in the appendix. © 1996 American Institute of Physics and American Chemical Society.

Key words: carbon dioxide; correlation; critical region; data evaluation; equation of state; extrapolation; fundamental equation; melting line; property tables; sublimation line; thermal and caloric properties; and vapor-liquid coexistence curve.

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| | | $\alpha, \beta, \gamma, \Delta, \theta$ | Adjustable parameters |
| | | $\alpha, \beta, \gamma, \delta$ | Critical exponents |
| | | Δ | Difference in any quantity |
| | | Δ, θ, ψ | Functions |
| | | δ | Reduced density ($\delta = \rho/\rho_c$) |
| | | ∂ | Partial differential |
| | | φ | Fugacity |
| | | ϕ | Dimensionless Helmholtz energy [$\phi = A/(RT)$] |
| | | μ | Joule-Thomson coefficient |
| | | ρ | Mass density |
| | | σ | Variance |
| | | τ | Inverse reduced temperature ($\tau = T_c/T$) |
| | | χ^2 | Weighted sum of squares |
| | | Superscripts | |
| | | <i>o</i> | Ideal gas property |
| | | <i>r</i> | Residual |
| | | ' | Saturated liquid state |
| | | " | Saturated vapor state |
| | | - | Denotes a vector |
| | | Subscripts | |
| | | <i>c</i> | At the critical point |
| | | calc | Calculated |
| | | corr | Corrected |
| | | exp | Experimental |
| | | <i>i,j,k,l,m</i> | Indices |
| | | <i>m</i> | Denotes the melting pressure |
| | | <i>s</i> | Denotes the vapor pressure |
| | | sub | Denotes the sublimation pressure |
| | | <i>t</i> | At the triple point |
| | | wt | Weighting |
| | | σ | Along the saturated liquid curve |
| | | 0 | In the reference state |
| | | 0H | In the initial state of Hugoniot curve measurements |
| | | 90 | Temperatures according to the ITS-90 |
| | | 68 | Temperatures according to the IPTS-68 |
| | | 48 | Temperatures according to the IPTS-48 |

Nomenclature

| Symbol | Description |
|--------------------------|--|
| <i>A,B,C,D,a,b,d,n,t</i> | Adjustable parameters |
| <i>A</i> | Specific Helmholtz energy |
| <i>B</i> | Second virial coefficient |
| <i>C</i> | Third virial coefficient |
| <i>c_p</i> | Specific isobaric heat capacity |
| <i>c_v</i> | Specific isochoric heat capacity |
| <i>c_σ</i> | Specific heat capacity along the saturated liquid line |
| <i>g</i> | Specific Gibbs energy |
| <i>h</i> | Specific enthalpy |
| <i>i,j,k,l,m</i> | Serial numbers |
| <i>I,J</i> | Maximum number of the serial numbers <i>i,j</i> |
| <i>M</i> | Number of data, molar mass |
| <i>p</i> | Pressure |
| | |
| | |

Physical Constants for Carbon Dioxide

M Molar mass: $M = (44.0098 \pm 0.0016)$ g/mol; see Ref. 1

| | |
|----------|--|
| R_m | Molar gas constant: $R_m = (8.314\ 510 \pm 0.000\ 210)$ ^a J/(mol K); see Ref. 2 |
| R | Specific gas constant: $R = R_m/M = (0.188\ 924\ 1 \pm 0.000\ 011\ 6)$ kJ/(kg K) |
| T_c | Critical temperature: $T_c = (304.128\ 2 \pm 0.015)$ K; see Sec. 3.2 |
| p_c | Critical pressure: $p_c = (7.377\ 3 \pm 0.003\ 0)$ MPa; see Sec. 3.2 |
| ρ_c | Critical density: $\rho_c = (467.6 \pm 0.6)$ kg/m ³ ; see Sec. 3.2 |
| T_t | Triple-point temperature: $T_t = (216.592 \pm 0.002)$ K; see Sec. 3.1 |
| p_t | Triple-point pressure: $p_t = (0.517\ 95 \pm 0.000\ 10)$ MPa; see Sec. 3.1 |
| T_0 | Reference temperature: $T_0 = 298.15$ K |
| p_0 | Reference pressure: $p_0 = 0.101\ 325$ MPa |
| h_0^o | Reference enthalpy in the ideal gas state at T_0 : $h_0^o = 0$ kJ/kg |
| s_0^o | Reference entropy in the ideal gas state at T_0 , p_0 : $s_0^o = 0$ kJ/(kg K) |

1. Introduction

1.1 Background

Over the past fifteen years great interest in the properties of carbon dioxide has developed. This interest has evolved from both industrial and scientific applications. From an engineering angle, carbon dioxide has proved to be the most commonly used solvent for supercritical fluid extraction and to be an excellent tool for enhanced oil recovery. Carbon dioxide processing and pipelining technologies have become of considerable commercial importance. Furthermore, the discussion on the greenhouse effect has focused technical interest on carbon dioxide as the most significant combustion product which effects the atmosphere.

From a thermodynamic point of view, carbon dioxide usually serves as the best known reference for a molecule with a strong quadrupole moment and as a testing fluid for calibration purposes. However, in sciences related to thermodynamics, interest is mainly based on the widespread occurrence of carbon dioxide. Geophysical calculations of chemical equilibria, under outer mantle conditions for example, require reliable thermodynamic data of carbon dioxide at very high pressures and temperatures.

Besides this, investigations of thermodynamic properties of carbon dioxide have always been influenced by the location of the critical region. On the one hand, the critical temperature of approximately 304 K allows many technical processes, for example pipelining processes, to be carried out within the critical or at least in the extended critical region. Therefore, from a technical point of view a sufficiently accurate calculation of thermodynamic properties is more difficult for carbon dioxide than for other substances. On the other hand, the data situation in the critical region is exceptionally good, which makes carbon dioxide a reference sub-

stance for theoretical approaches dealing with the critical region of pure fluids. Almost every physical model for the description of the critical region has been tested for carbon dioxide.

In 1965, an international research project on the thermodynamic properties of carbon dioxide was established at the instigation of the International Union of Pure and Applied Chemistry (IUPAC). In 1976, Angus *et al.*³ published a monograph which reviewed the experimental data available up to 1973 and presented extensive tables of the thermal and caloric properties derived from the selected equation of state. Nevertheless, knowledge of the thermodynamic properties of carbon dioxide remained unsatisfactory. Thus, since 1973 numerous experiments including state-of-the-art experiments with significantly improved accuracy have been performed in order to improve the quality of the entire data set; a third of the data sets available today belongs to this group.

In addition to the increased amount of experimental data, correlation techniques have significantly improved during the last decade. Sophisticated "multi-property" fitting procedures^{4,5} and a new strategy for optimizing the structure of empirical correlation equations⁶ have resulted in a new basis for the development of an empirical equation of state.

1.2 Prior Correlations of Carbon Dioxide Properties and Demands on the New Correlation

Since 1960 numerous correlation equations for the thermodynamic properties of carbon dioxide have been developed, but only a few of them describe the properties within a sufficiently large range including the gas, liquid, and supercritical states. Table 1 summarizes the equations of state for carbon dioxide which have been developed since 1970. After examining the wide-range equations of state available in 1973, Angus *et al.*³ discussed three equations in the IUPAC monograph, namely the equations of Bender,⁷ Altunin and Gadetskii,⁸ and Stein,⁹ which form the beginning of Table 1. Finally, Angus *et al.* decided to use the equation of Altunin and Gadetskii⁸ as a basis for the IUPAC monograph. At that time, none of the existing wide-range equations of state offered a reasonable description of the critical region. Thus, Angus *et al.*³ combined the wide-range equation with a scaled equation of state developed by Schofield¹⁹ and a switching function developed by Chapela and Rowlinson.²⁰ Although it was known that the evaluation of the combined correlation equations causes numerical problems and yields incorrect results for derived properties in the switching region, the equation was generally accepted as a reference for carbon dioxide. In 1988, Pitzer and Schreiber¹⁶ took up the IUPAC compilation again and showed that very similar results can be achieved with less numerical expense if special terms for the description of the critical region are added to the equation of Altunin and Gadetskii.⁸

The only correlations which really improve the results of Angus *et al.*³ are the equations developed at the National Institute of Standards and Technology by Ely¹⁴ and Ely

^aReference 2 gives a standard deviation of $\pm 0.000\ 070$ J/(mol K).

TABLE 1. Available wide-range equations of state for carbon dioxide

| Authors | Year | Temperature range (K) | Pressure range (MPa) | Structure of the equation | Number of coeff. in residual part | Data used in the correlation |
|--|------|-----------------------|----------------------|------------------------------------|-----------------------------------|--|
| Bender ⁷ | 1970 | 216–1 076 | 0–50 | Extended BWR ^a | 20 | $p\rho T, p_s \rho' \rho''$ |
| Altunin and Gadetskii ⁸ | 1971 | 215–1 300 | 0–300 | Polynomial | 50 | $p\rho T, c_p$ |
| Stein ⁹ | 1972 | ... ^b | ... ^b | Polynomial | 44 | $p\rho T, p_s \rho' \rho''$ |
| Starling <i>et al.</i> ¹⁰ | 1972 | 243–413 | 0–48 | Extended BWR ^a | 11 | $p\rho T, h, p_s$ |
| Meyer-Pitroff ¹¹ | 1973 | 200–1 273 | 0–60 | Polynomial | 84 | $p\rho T, p_s \rho' \rho'', c_v, h$ |
| Angus <i>et al.</i> ³ (IUPAC) | 1976 | 220–1 100 | 0–100 | Combined | 50+5+4 | $p\rho T, c_p$ |
| Huang <i>et al.</i> ¹² | 1985 | 216–423 | 0–310 | Extended BWR ^{a,c} | 27 | $p\rho T, p_s \rho' \rho''$ |
| Ely ¹⁴ | 1986 | 216–1 023 | 0–300 | Schmidt and Wagner ⁴ | 32 | $p\rho T, p_s \rho' \rho'', c_v, c_\sigma$ |
| Ely <i>et al.</i> ¹⁵ | 1987 | 216–1 023 | 0–300 | Schmidt and Wagner ⁴ | 32 | $p\rho T, p_s \rho' \rho'', c_v, c_\sigma$ |
| Pitzer and Schreiber ¹⁶ | 1988 | 230–1 030 | 0–100 | Extended polynomial | 53 | $p\rho T, p_s \rho' \rho'', c_v$ |
| Ely <i>et al.</i> ¹⁷ | 1989 | 216–1 023 | 0–316 | Jacobsen and Stewart ¹⁸ | 32 | $p\rho T, p_s \rho' \rho'', c_v, c_\sigma$ |
| Pitzer and Sterner ^{18a} | 1994 | 220–2 000 | 0–10 000 | Fractional form | 28 | $p\rho T, p_s \rho' \rho'', B, f^e$ |

^aBenedict–Webb–Rubin.^bNo information published.^cTerms developed by Ewers and Wagner¹³ for the description of the critical region were also used.^dBesides some experimental data, mainly data from the IUPAC tables³ were used as input data.^eBesides some experimental data, mainly data calculated from the equation of Ely *et al.*¹⁷ were used as input data.

et al.^{15,17} These equations take into account almost all of the published experimental results. However, some of the most important state-of-the-art experiments on carbon dioxide were not yet available at that time. A detailed comparison²¹ shows that the equation given in Refs. 14 and 15 using the form developed by Schmidt and Wagner⁴ is superior to the equation given in Ref. 17 which uses the form developed by Jacobsen and Stewart.¹⁸

Tests of these correlations have yielded that all of the existing equations of state, independent of their different quality, show the following limitations:

- State-of-the-art data for the $p\rho T$ relation are not represented to within their experimental uncertainty.
- State-of-the-art data describing the liquid-vapor phase equilibrium are not represented to within their experimental uncertainty.
- Within the critical region, the calculation of caloric properties yields unreasonable results.
- Unreasonable behavior can be observed in regions with a poor data situation.

- Extrapolation to temperatures and pressures outside the range of validity yields unreasonable results.
- The temperature values used do not correspond to the current International Temperature Scale of 1990 (ITS-90).

The equation of Pitzer and Sterner^{18a} can mainly be considered to be an example for an empirical equation of state with reasonable extrapolation behavior; the authors do not claim that this equation improves the description of thermodynamic properties in the region where accurate data exist.

The problems related to the description of properties within the critical region can essentially be solved by using scaled equations of state; Table 2 shows selected correlations with such scaling approaches for the description of the critical region of carbon dioxide. However, the relatively small range of validity and the mathematically complex structure of these equations limit their use.

An exception with regard to the range of validity is the empirical equation of Erickson *et al.*²⁶ This equation uses an improved form of the transformation procedure, originally developed by Fox,²⁹ to achieve a reasonable but not an as-

TABLE 2. Selected scaled equations of state for carbon dioxide

| Authors | Year | Temperature ^a range (K) | Density ^b range (kg/m ³) | Scaling technique used | Number of fitted coefficients |
|---|------|------------------------------------|---|------------------------|-------------------------------|
| Schofield ¹⁹ | 1969 | ... ^c | ... ^c | Simple scaling | 5 |
| Vicenti-Missoni <i>et al.</i> ²² | 1969 | 301–313 | 327–608 | Simple scaling | 6 |
| Murphy <i>et al.</i> ²³ | 1973 | 304–314 | 336–598 | Simple scaling | 5 |
| Albright <i>et al.</i> ²⁴ | 1987 | 301–323 | 290–595 | Revised and extended | 13 |
| Albright <i>et al.</i> ²⁵ | 1987 | 298–322 | 245–600 | Crossover | 12 |
| Erickson <i>et al.</i> ²⁶ | 1987 | ... ^d | ... ^d | Transformation | 32+7 |
| Chen <i>et al.</i> ²⁷ | 1990 | 291–373 | 193–712 | Crossover | 19 |
| Kiselev <i>et al.</i> ²⁸ | 1991 | 298–395 | 280–655 | Crossover | 12 |

^aRange of validity for $\rho = \rho_c$.^bRange of validity for $T = T_c$.^cNo information published.^dScaled wide-range equation, valid for pressures up to 300 MPa at temperatures from 212 K to 1000 K.

ymptotically correct description of the caloric properties in the critical region. Like other parametric approaches, this equation still requires complicated iteration procedures, but it is valid in a range which is sufficiently wide for engineering applications. Tests carried out by Erickson *et al.*²⁶ showed that outside the critical region the transformed equation based on the form developed by Jacobsen and Stewart¹⁸ is inferior to Ely's equation.^{14,15}

The purpose of this article is to present a new equation of state for carbon dioxide explicit in the Helmholtz energy, which is designed to overcome the disadvantages of the existing correlations. The consistent use of sophisticated fitting³⁰ and optimization⁶ procedures allows the representation of even the most accurate data within their experimental uncertainty. Extensive investigations of the data set prevent the equation from unreasonable behavior within the fitting region, and new procedures are introduced to guarantee a reasonable extrapolation behavior of the new equation. The representation of caloric properties in the critical region has been improved by an empirical approach which yields reasonable results even in the immediate vicinity of the critical point.

All the correlation equations given in this article correspond to the ITS-90 temperature scale.

1.3 Organization of the Article

In Sec. 2 we give a brief review of the application of empirical equations of state explicit in the Helmholtz energy as a function of density and temperature; this combination of variables is one form of a fundamental equation. The techniques used for the development of the new equation (multi-property fitting, optimization procedure) are described briefly. Section 3 deals with the liquid-vapor, solid-vapor, and solid-liquid phase equilibria of carbon dioxide. The available data are discussed. In addition to the equation of state, short supplementary equations have been developed for the temperature dependence of the melting pressure p_m , the sublimation pressure p_{sub} , the vapor pressure p_s , the saturated liquid density ρ' , and the saturated vapor density ρ'' . The experimental information available for the single phase region of carbon dioxide is discussed in Sec. 4. In Sec. 5 a detailed description of the new approach for representing the critical region is given. Possibilities and limitations of the use of nonanalytic terms in empirical wide-range equations of state are outlined. The new correlation equations for both the ideal and the residual part of the Helmholtz free energy are presented in Sec. 6. The final data set and the bank of terms used for the development of the new equation are given. Comparisons of properties calculated from the new equation of state for carbon dioxide with selected experimental data and those values calculated from prior correlations are presented in Sec. 7. A discussion of the extrapolation behavior of the new fundamental equation is included in this section. Finally, the uncertainties of the new formulation are estimated and tables of the thermodynamic properties of carbon dioxide are listed in the Appendix.

2. Basic Elements of the Development of Equations of State in Form of a Fundamental Equation

The new equation of state, developed for the representation of the thermodynamic properties of carbon dioxide, is an empirical representation of the fundamental equation explicit in the Helmholtz energy. Since the application of optimization procedures and the technique of multi-property fitting were extensively discussed by Setzmann and Wagner^{6,30} and Saul and Wagner,⁵ this section is restricted to some basic facts giving a rough understanding of the procedures used for the development of the new equation. However, those facts which have not previously been published are outlined in more detail.

2.1 Helmholtz Function

The fundamental equation given in this article is expressed in form of the Helmholtz energy A with the two independent variables density ρ and temperature T . The dimensionless Helmholtz energy $\phi = A/(RT)$ is commonly split into a part depending on the ideal-gas behavior ϕ^0 and a part which takes into account the residual fluid behavior ϕ^r , namely

$$\phi(\delta, \tau) = \phi^0(\delta, \tau) + \phi^r(\delta, \tau), \quad (2.1)$$

where $\delta = \rho/\rho_c$ is the reduced density and $\tau = T_c/T$ is the inverse reduced temperature. Both the density ρ and the temperature T are reduced with their critical values, ρ_c and T_c , respectively.

Since the Helmholtz energy as a function of density and temperature is one form of a fundamental equation, all the thermodynamic properties of a pure substance can be obtained by combining derivatives of Eq. (2.1). Table 3 gives the relations between Eq. (2.1) and the properties considered in this article. The vapor pressure and the densities of saturated liquid and saturated vapor can be determined from an equation explicit in ϕ by simultaneous solution of the equations

$$\frac{p_s}{RT\rho'} = 1 + \delta' \phi_r'(\delta', \tau), \quad (2.2a)$$

$$\frac{p_s}{RT\rho''} = 1 + \delta'' \phi_r''(\delta'', \tau), \quad (2.2b)$$

$$\frac{p_s}{RT} \left(\frac{1}{\rho''} - \frac{1}{\rho'} \right) - \ln \left(\frac{\rho'}{\rho''} \right) = \phi^r(\delta', \tau) - \phi^r(\delta'', \tau), \quad (2.2c)$$

which correspond to the equality of pressure, temperature, and specific Gibbs energy (Maxwell criterion) in the coexisting phases.

2.2 Helmholtz Energy of the Ideal Gas

The Helmholtz energy of the ideal gas is given by

$$A^0(\rho, T) = h^0(T) - RT - Ts^0(\rho, T). \quad (2.3)$$

TABLE 3. Relations of thermodynamic properties to the dimensionless Helmholtz function ϕ consisting of ϕ^0 and ϕ^r ; see Eq. (2.1)

| Property and common thermodynamic definition | Relation to the reduced Helmholtz energy ϕ and its derivatives ^a |
|--|---|
| Pressure: | $\frac{p(\delta, \tau)}{\rho RT} = 1 + \delta\phi_\delta^r$ |
| $p(T, \rho) = -(\partial A / \partial v)_T$ | $\frac{s(\delta, \tau)}{R} = \tau(\phi_\tau^0 + \phi_\tau^r) - \phi^0 - \phi^r$ |
| Entropy: | $\frac{u(\delta, \tau)}{RT} = \tau(\phi_\tau^0 + \phi_\tau^r)$ |
| $s(T, \rho) = -(\partial A / \partial T)_v$ | $\frac{c_v(\delta, \tau)}{R} = -\tau^2(\phi_{\tau\tau}^0 + \phi_{\tau\tau}^r)$ |
| Internal energy: | $\frac{h(\delta, \tau)}{RT} = 1 + \tau(\phi_\tau^0 + \phi_\tau^r) + \delta\phi_\delta^r$ |
| $u(T, \rho) = A - T(\partial A / \partial T)_v$ | $\frac{c_p(\delta, \tau)}{R} = -\tau^2(\phi_{\tau\tau}^0 + \phi_{\tau\tau}^r) + \frac{(1 + \delta\phi_\delta^r - \delta\tau\phi_{\delta\tau}^r)^2}{1 + 2\delta\phi_\delta^r + \delta^2\phi_{\delta\delta}^r}$ |
| Isochoric heat capacity: | $\frac{c_p(\tau)}{R} = -\tau^2(\phi_{\tau\tau}^0 + \phi_{\tau\tau}^r) + \frac{1 + \delta\phi_\delta^r - \delta\tau\phi_{\delta\tau}^r}{1 + 2\delta\phi_\delta^r + \delta^2\phi_{\delta\delta}^r}$ |
| $c_v(T, \rho) = (\partial u / \partial T)_v$ | $\cdot [1 + \delta\phi_\delta^r - \delta\tau\phi_{\delta\tau}^r] - \frac{\rho_c}{R\delta} \frac{dp_s}{dT}$ |
| Enthalpy: | $\frac{w^2(\delta, \tau)}{RT} = 1 + 2\delta\phi_\delta^r + \delta^2\phi_{\delta\delta}^r - \frac{(1 + \delta\phi_\delta^r - \delta\tau\phi_{\delta\tau}^r)^2}{\tau^2(\phi_{\tau\tau}^0 + \phi_{\tau\tau}^r)}$ |
| $h(T, p) = A - T(\partial A / \partial T)_v - v(\partial A / \partial v)_T$ | $\mu R \rho = \frac{-(\delta\phi_\delta^r + \delta^2\phi_{\delta\delta}^r + \delta\tau\phi_{\delta\tau}^r)}{(1 + \delta\phi_\delta^r - \delta\tau\phi_{\delta\tau}^r)^2 - \tau^2(\phi_{\tau\tau}^0 + \phi_{\tau\tau}^r)(1 + 2\delta\phi_\delta^r + \delta^2\phi_{\delta\delta}^r)}$ |
| Isobaric heat capacity: | $\ln \phi(\delta, \tau) = \phi^r + \delta\phi_\delta^r - \ln(1 + \delta\phi_\delta^r)$ |
| $c_p(T, p) = (\partial h / \partial T)_p$ | $B(\tau)\rho_c = \lim_{\delta \rightarrow 0} \phi_\delta^r(\delta, \tau)$ |
| Saturated liquid heat capacity: | $C(\tau)\rho_c^2 = \lim_{\delta \rightarrow 0} \phi_{\delta\delta}^r(\delta, \tau)$ |
| $c_a(T) = (\partial h / \partial T)_p + T(\partial p / \partial T)_v$ | $\cdot \phi_\delta^r = \left[\frac{\partial \phi}{\partial \delta} \right]_\tau, \quad \delta_{\delta\delta}^r = \left[\frac{\partial^2 \phi}{\partial \delta^2} \right]_\tau, \quad \phi_\tau^r = \left[\frac{\partial \phi}{\partial \tau} \right]_\delta, \quad \phi_{\tau\tau}^r = \left[\frac{\partial^2 \phi}{\partial \tau^2} \right]_\delta, \quad \text{and} \quad \phi_{\delta\tau}^r = \left[\frac{\partial^2 \phi}{\partial \delta \partial \tau} \right]$ |
| Speed of sound: | |
| $w(T, p) = \sqrt{(\partial p / \partial \rho)_s}$ | |
| Joule-Thomson coefficient: | |
| $\mu(T, p) = (\partial T / \partial p)_h$ | |
| Fugacity: | |
| $\ln(\phi(T, p)) = \int_0^p \left[\frac{v(T, p)}{RT} - \frac{1}{p} \right] dp_T$ | |
| Second virial coefficient: | |
| $B(T) = \lim_{\rho \rightarrow 0} (\partial(p / (\rho RT)) / \partial \rho)_T$ | |
| Third virial coefficient: | |
| $C(T) = \frac{1}{2} \lim_{\rho \rightarrow 0} \{\partial^2[p / (\rho RT)] / \partial \rho^2\}_T$ | |
| ^a $\phi_\delta^r = \left[\frac{\partial \phi}{\partial \delta} \right]_\tau, \quad \delta_{\delta\delta}^r = \left[\frac{\partial^2 \phi}{\partial \delta^2} \right]_\tau, \quad \phi_\tau^r = \left[\frac{\partial \phi}{\partial \tau} \right]_\delta, \quad \phi_{\tau\tau}^r = \left[\frac{\partial^2 \phi}{\partial \tau^2} \right]_\delta, \quad \text{and} \quad \phi_{\delta\tau}^r = \left[\frac{\partial^2 \phi}{\partial \delta \partial \tau} \right]$ | |

The enthalpy h^0 of the ideal gas is a function of temperature only, and the entropy s^0 of the ideal gas depends on temperature and density. Both properties can be derived from an equation for the ideal-gas heat capacity c_p^0 . When c_p^0 is inserted into the expression for $h^0(T)$ and $s^0(\rho, T)$ in Eq. (2.3) one obtains

$$A^0 = \int_{T_0}^T c_p^0 dT + h_0^0 - RT - T \int_{T_0}^T \frac{c_p^0 - R}{T} dT - RT[\ln(\rho/\rho_0)] - Ts_0^0, \quad (2.4)$$

where $\rho_0 = p_0/(RT_0)$ is the density, h_0^0 the enthalpy, and s_0^0 the entropy of the ideal gas in a reference state. The final equation for $\phi^0 = A^0/(RT)$ is given in Sec. 6.1.

2.3 Residual Part of the Helmholtz Energy

In contrast to the Helmholtz energy of the ideal gas, no theoretical approach is known which yields a sufficiently accurate equation for the residual part of the Helmholtz energy and which is valid in the whole fluid region of a pure sub-

stance. Thus, the equation for the residual part has to be determined in an empirical way by optimizing its functional form and fitting its coefficients to experimental results.^b Since the Helmholtz energy is not accessible to direct measurements, a procedure has been developed which allows the establishment of an empirical equation for the residual part of the Helmholtz energy by using data of different properties.

2.3.1 Fitting an Empirical Equation for ϕ^r to Data

An empirical equation for the residual part of the Helmholtz energy can be written as $\phi^r(\delta, \tau, \bar{n})$, where \bar{n} represents the vector of coefficients to be fitted. Ahrendts and Baehr³¹ showed that the determination of an optimum set of coefficients results in the minimization of a sum of squares, defined as the sum of partial sums of squares belonging to the different properties included into the fit:

^bThroughout this article the word "data" is used to characterize such experimental results.

$$\chi^2 = \sum_{j=1}^J \chi_j^2 = \sum_{j=1}^J \sum_{m=1}^{M_j} \left[\frac{[z_{\text{exp}} - z_{\text{calc}}(x_{\text{exp}}, y_{\text{exp}}, \bar{n})]^2}{\sigma_{\text{tot}}^2} \right]_{j,m}, \quad (2.5)$$

where J is the number of properties involved in the fit, M_j the number of data points used for the j th property, z_{exp} the value measured for any property $z(x, y)$, and z_{calc} the value calculated for x_{exp} , y_{exp} from the correlation equation with the parameter vector \bar{n} . The universal variable x usually corresponds to T , but y can correspond to ρ [e.g., $p(T, \rho)$] or to p [e.g., $w(T, p)$] and can even vanish [e.g., $p_s(T)$]. The variance σ_{tot}^2 is explained in Sec. 2.3.3.

The determination of \bar{n} by minimizing χ^2 results in a linear system of normal equations if z depends on T and ρ and if the relations between z and ϕ^r and the derivatives of ϕ^r are linear (see Table 3). If these conditions are not fulfilled, the data have to be linearized by suitable procedures^{32,5} or nonlinear algorithms³³ have to be used. A detailed description of the iterative fitting process resulting from the use of data with nonlinear relation to ϕ^r is given by Setzmann and Wagner.³⁰ In this article, the linear data of the $p\rho T$ relation, of the internal energy u , of the isochoric heat capacity c_v , of the third virial coefficient C , and linearized data of the enthalpy h , of the isobaric heat capacity c_p of the homogeneous region and the saturated liquid, of the speed of sound w of the homogeneous region, the saturated liquid, and the saturated vapor, and of the Maxwell criterion were used in linear fitting algorithms. Within the nonlinear fitting process, data of all these properties and of the Joule-Thomson coefficient μ , which cannot be linearized in a reasonable way, were used directly which means without any linearization.

2.3.2 Optimizing the Mathematical Form

The fitting procedure described above supposes that the mathematical form of a correlation equation is already known and only the coefficients \bar{n} have to be determined. Since a universal form for an equation describing the residual part of the Helmholtz energy is not known, this requirement is not satisfied. Thus, a suitable mathematical structure has first to be established. With the exception of the equation of state developed by Ely and co-workers,^{14,15} the form of the equations existing for carbon dioxide has been determined in a subjective way, based on the experience of the equation maker by trial and error. To improve this procedure, Wagner and co-workers developed different optimization strategies^{34,13,6} by introducing objective criteria for the selection of a mathematical structure. The mathematical structure applied by Ely and co-workers was developed by Schmidt and Wagner⁴ for oxygen by the use of the "evolutionary optimization method," EOM.¹³

In this work, the optimization method developed by Setzmann and Wagner⁶ was used for the determination of a suitable mathematical structure. Minor improvements were introduced, concerning the stochastic part of the optimization procedure. More important, however, are the changes made in the Setzmann-Wagner procedure with regard to the handling of different functional forms from the "bank of terms."

A sophisticated correlation equation for the residual part of the Helmholtz energy consists of an extensive sum of terms. Hence, the mathematical form of a single term can be associated with different functional groups ranging from simple polynomials of the reduced density δ and the inverse reduced temperature τ to complicated exponential expressions (see the bank of terms given in Sec. 6.2). In the known optimization procedures, only the total number of terms of the optimized equation is limited to a preselected value. During this work, additional limitations with respect to the number of terms belonging to special functional groups have turned out to be useful. The actual revision of the optimization procedure allows the definition of such limits to special term forms. The new equation for carbon dioxide has been developed with a limit to four nonanalytic terms to avoid unreasonable behavior in the critical region (cf. Sec. 5.2) and eight polynomial terms to improve the extrapolation behavior (cf. Sec. 7.3 and Span and Wagner³⁵).

As pointed out by Setzmann and Wagner,^{6,30} the optimization procedure only works with linear or linearized data. This restriction leads to the previously described³⁰ cyclic process, consisting of linearizing the data, optimizing the mathematical structure of the correlation equation, and nonlinear fitting of the coefficients; these steps are typical for the development of such fundamental equations of state.

2.3.3 The Procedure of Weighting

When data sets of different properties are used for the development of a correlation equation, it is necessary that the residual ($z_{\text{exp}} - z_{\text{calc}}$) in Eq. (2.5) is reduced with a suitable measure for the uncertainty of the data point. According to the Gaussian error propagation formula, the uncertainty of a measured data point is given by

$$\sigma_{\text{exp}}^2 = \left(\left[\frac{\partial \Delta z}{\partial x} \right]_{y,z}^2 \sigma_x^2 + \left[\frac{\partial \Delta z}{\partial y} \right]_{x,z}^2 \sigma_y^2 + \left[\frac{\partial \Delta z}{\partial z} \right]_{x,y}^2 \sigma_z^2 \right), \quad (2.6)$$

where σ_x , σ_y , and σ_z are the uncertainties with respect to the uncorrelated single variables x , y , and z ; the partial derivatives of z can be calculated from a preliminary equation of state.

In order to have an additional influence on the data set, a weighting factor f_{wt} is introduced. The total variance σ_{tot} of a data point used in Eq. (2.5) is defined as

$$\sigma_{\text{tot}}^2 = \sigma_{\text{exp}}^2 / f_{\text{wt}}^2. \quad (2.7)$$

In this way, weighting factors $f_{\text{wt}} > 1$ enlarge the influence of a data point with respect to the sum of squares and weighting factors $f_{\text{wt}} < 1$ reduce it. Usually f_{wt} is equal to one and σ_{tot}^2 is equal to σ_{exp}^2 ; in some cases, however, different weighting factors are used to compensate for effects caused by the structure of the data set. These effects may be divided into the following groups:

- In a special region there are only a few ($f_{\text{wt}} > 1$) or exceptionally many ($f_{\text{wt}} < 1$) data points.
- An extensive data set with large experimental uncertainties can be transformed into a smaller, but more consistent data

set by suitable data selection ($f_{wt} > 1$).

- After correcting systematic deviations, a data set yields results much better than expected from its original experimental uncertainty ($f_{wt} > 1$).
- In a special region, enlarged, but difficult assignable uncertainties of the selected data are expected ($f_{wt} < 1$).

To achieve as much transparency with regard to the data set as possible, the tables presenting the selected data (see Sec. 4) contain additional information on the uncertainties used in the weighting procedure as well as on the mean value of the weighting factor. Weighting factors deviating significantly from $f_{wt} = 1$ are discussed.

3. Phase Equilibria of Carbon Dioxide

An accurate description of phase equilibria by auxiliary equations is an important precondition for the development of a wide-range equation of state and is also helpful for users who are only interested in phase equilibria. Therefore, all available experimental information on the triple point, the critical point, the melting pressure, the sublimation pressure, the vapor pressure, the densities of saturated liquid and vapor, and on caloric properties on the liquid-vapor phase boundary have been reviewed. With the exception of the caloric properties, simple correlation equations have been developed for the temperature dependency of these quantities.

To condense the description of the data situation, the characteristic information on the single data sets is summarized in tables for the corresponding property. The data sets have been divided into three groups. The assignment considers the critically assessed uncertainty of the data, size of the data set, and covered temperature range. In addition, attention is paid to the data situation for the respective property. Group 1 contains the data sets used for the development of the corresponding correlation equation. Group 2 contains data sets suitable for comparisons. Compared with group 1 data, these data decline at least under one of the three aspects mentioned above. Group 3 contains very small data sets and data sets with rather high uncertainty. Consideration of these data is not reasonable on the level of accuracy aspired to here. Nevertheless this means no devaluation of these data sets — the whole ranking is influenced more by the quality in relation to the best available reference data than by an absolute level of uncertainty; for other purposes even group 3 data sets may be very useful.

Since the new correlation equations and all temperature values in this article correspond to the ITS-90 temperature scale,³⁶ the temperature values of the available data, based on older temperature scales, were converted to ITS-90. The conversion from the IPTS-68 temperature scale to ITS-90 temperatures was carried out based on the internationally agreed procedure of Preston-Thomas *et al.*,³⁷ explained by Rusby.³⁸ The number of digits of the converted values was increased by one digit in order to guarantee numerically consistent reconversion, but not more than four digits to the right

of the decimal point were used. Data corresponding to the IPTS-48 temperature scale were converted to IPTS-68 according to the procedure given by Bedford and Kirby.³⁹ For temperatures between 90 K and 900 K, the temperature scales ITS-27 and IPTS-48 do not deviate from each other and data older than 1927 were not used.

The algorithm used for the conversion from IPTS-68 to the ITS-90 temperature scale³⁸ causes an additional uncertainty of ± 1.5 mK for temperatures below 273.15 K and ± 1 mK for temperatures above 273.15 K. This additional uncertainty is *not* considered in the uncertainties given in the tables of this section, since these uncertainties were mainly used for consistency tests between data of different authors. In this case, the uncertainty in the absolute temperature, which is influenced by the uncertainty of the conversion, is less important. The comparison between two very similar temperature values is not influenced by the uncertainty of the conversion if both temperatures are converted with the same procedure.

3.1 Triple Point

During the last 90 years, the triple-point temperature of carbon dioxide has been determined by numerous authors but the data situation for the triple-point pressure is rather poor. Fortunately, the few measurements available are very consistent with each other. Table 4 shows selected data of the triple point of carbon dioxide. After a comprehensive review of the existing data, we have chosen the following:

$$T_t = (216.592 \pm 0.003) \text{ K}, \quad (3.1)$$

$$p_t = (0.51795 \pm 0.00010) \text{ MPa}. \quad (3.2)$$

Data of the density of the saturated liquid and the saturated vapor at the triple point are not available, but the evaluation of the corresponding correlation equations given in Secs. 3.6 and 3.7 yields

$$\rho_t' = (1178.53 \pm 0.18) \text{ kg/m}^3, \quad (3.3)$$

$$\rho_t'' = (13.7614 \pm 0.0034) \text{ kg/m}^3. \quad (3.4)$$

3.2 Critical Point

Altogether, data of the critical point of carbon dioxide are given in 75 papers. Table 5 shows selected values of the critical temperature, the critical pressure, and the critical density. The values found for the critical density agree well within the expected uncertainties, but the values for the critical temperature show significant differences, far beyond the uncertainties given by some of the authors. Essentially, the differences in the critical pressures can be explained by the variation of the vapor pressure with the assumed critical temperature.

In the course of this work, no new attempt has been made to determine the critical parameters of carbon dioxide, but the evaluation of Duscheck *et al.*⁵⁸ was tested under different aspects. No reason for altering the data became obvious. Thus, we have used

TABLE 4. Selected data for the triple point of carbon dioxide

| Source | Year | T (K) ^a | ΔT (K) ^b | p (MPa) | Δp (MPa) |
|--|------|----------------------|-----------------------------|-----------|------------------|
| Meyers and Van Dusen ⁴⁰ | 1933 | 216.588 5 | ± 0.005 | 0.517 99 | $\pm 0.000\ 06$ |
| Ambrose ⁴¹ | 1957 | 216.588 5 | ± 0.002 | | |
| Lovejoy ⁴² | 1963 | 216.591 5 | ± 0.001 | | |
| Haro <i>et al.</i> ⁴³ | 1979 | 216.594 5 | ± 0.002 | | |
| Staveley <i>et al.</i> ⁴⁴ | 1981 | 216.591 | | 0.517 96 | |
| Blanes-Rex <i>et al.</i> ⁴⁵ | 1982 | 216.594 5 | ± 0.001 | | |
| Pavese and Fern ⁴⁶ | 1982 | 216.591 5 | ± 0.002 | | |
| Bedford <i>et al.</i> ⁴⁷ | 1984 | 216.590 5 | ± 0.001 | | |
| Bonnier <i>et al.</i> ⁴⁸ | 1984 | 216.591 7 | $\pm 0.000\ 2$ | | |
| Duschek ⁴⁹ | 1989 | 216.591 5 | ± 0.003 | 0.517 95 | $\pm 0.000\ 1$ |

^aAll temperatures were converted to ITS-90. Up to an uncertainty of 0.1 mK an additional digit is added to guarantee consistent reconversion to IPTS-68 temperatures.

^bThe uncertainty of the conversion from IPTS-68 to ITS-90 is not considered here.

$$T_c = (304.1282 \pm 0.015) \text{ K}, \quad (3.5)$$

$$p_c = (7.3773 \pm 0.0030) \text{ MPa}, \quad (3.6)$$

$$\rho_c = (467.6 \pm 0.6) \text{ kg/m}^3. \quad (3.7)$$

(The additional digit in T_c is given to guarantee numerical consistency in any reconversion to the IPTS-68 temperature scale.)

3.3 Melting Pressure

There are only two available sets of measurements describing the melting pressure of carbon dioxide. In 1942 Michels *et al.*⁶⁰ measured 25 melting pressures at temperatures between 217 K and 266 K, corresponding to pressures between 0.9 MPa and 284 MPa. In 1960, Clusius *et al.*⁶¹ published 21 data, covering the range from 217 K to 222 K, corresponding to 0.5 MPa to 24 MPa.

Unfortunately, these data sets are inconsistent with each other and with recent data of the triple point pressure. In both experiments, the thermometers were calibrated at the triple-point of carbon dioxide. Since the values of the triple-point

temperature assumed by Michels *et al.*⁶⁰ and Clusius *et al.*⁶¹ deviate from the recent value [cf. Eq. (3.1)], all their temperature values were corrected according to

$$T_{90} = T_{Cl,90} - 0.05 \text{ K}, \quad (3.8)$$

$$T_{90} = T_{Mi,90} - 0.04 \text{ K} \quad (3.9)$$

after their conversion to ITS-90 temperatures.

The corrected data are consistent within the expected uncertainties and were used to establish a simple correlation equation for the melting pressure:

$$\frac{p_m}{p_t} = 1 + a_1 \left(\frac{T}{T_t} - 1 \right) + a_2 \left(\frac{T}{T_t} - 1 \right)^2, \quad (3.10)$$

with $T_t = 216.592$ K, $p_t = 0.51795$ MPa, $a_1 = 1955.5390$, and $a_2 = 2055.4593$. The equation is constrained to the triple-point pressure by its functional form. The representation of both the corrected and uncorrected data is shown in Fig. 1. The uncertainty of Eq. (3.10) is estimated to be $\Delta p_m/p_m \leq \pm 1.5\%$ for $T_t \leq T \leq 225$ K and $\Delta p_m/p_m \leq \pm 0.5\%$ for

TABLE 5. Selected data for the critical point of carbon dioxide

| Source | Year | T_c (K) ^{a,b} | p_c (MPa) | ρ_c (kg/m ³) |
|--|------|--------------------------|--------------------|-------------------------------|
| Leveld Sengers and Chen ⁵⁰ | 1972 | 304.182 | | |
| Moldover ⁵¹ | 1974 | 304.1192 ± 0.004 | 7.3753 | 467.8 ± 2.2 |
| Angus <i>et al.</i> ⁵² | 1976 | 304.202 ± 0.05 | 7.3858 ± 0.005 | 468 ± 5 |
| Lipa <i>et al.</i> ⁵² | 1977 | 303.9170 ± 0.005 | | |
| Moldover <i>et al.</i> ⁵³ | 1979 | 304.122 | 7.375 | 467 |
| Baade ⁵⁴ | 1983 | 304.122 | 7.375 | 467 |
| Edwards ⁵⁵ | 1984 | 304.0984 ± 0.0001 | | |
| Sengers and Leveld Sengers ⁵⁶ | 1986 | 304.122 | 7.372 | 468 |
| Albright <i>et al.</i> ²⁴ | 1987 | 304.0992 | 7.3719 | 467.67 |
| Ely <i>et al.</i> ²¹ | 1987 | 304.1192 | 7.37479 | 466.5 |
| Chen <i>et al.</i> ⁵⁷ | 1990 | 304.0992 | 7.3916 | 467.69 |
| Chen <i>et al.</i> ²⁷ | 1990 | 304.1192 | 7.3753 | 467.83 |
| Duschek <i>et al.</i> ⁵⁸ | 1990 | 304.1282 ± 0.015 | 7.3773 ± 0.003 | 467.6 ± 0.6 |
| Abdulagatov <i>et al.</i> ⁵⁹ | 1991 | 304.1272 ± 0.010 | | 467.5 |

^aAll temperatures were converted to ITS-90. Up to four digits beyond the decimal point an additional digit is added to guarantee consistent reconversion to IPTS-68 temperatures.

^bThe uncertainty of the conversion from IPTS-68 to ITS-90 is not considered here.

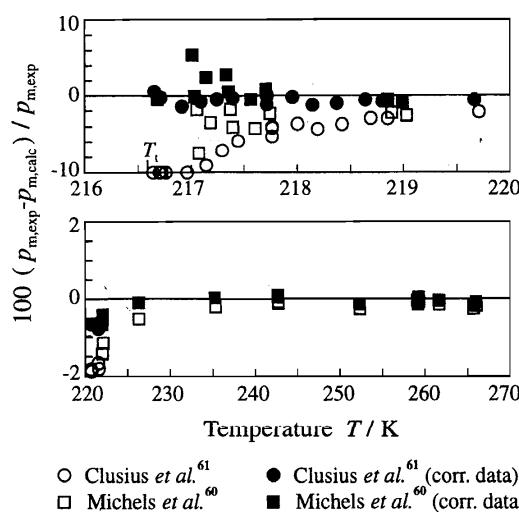


FIG. 1. Relative deviations of experimental melting pressure data from values calculated from the melting pressure equation, Eq. (3.10). In this figure, both the corrected and the uncorrected data are plotted (see Sec. 3.3).

$225 \text{ K} < T \leq 270 \text{ K}$. The simple form of the equation should ensure reasonable extrapolation to higher temperatures.

3.4 Sublimation Pressure

Due to the widespread use of solid carbon dioxide, the data situation for the sublimation pressure is exceptionally good. The available data sets for the sublimation pressure of carbon dioxide are given in Table 6. The data are classified according to the procedure described above. The data set of Bilkadi *et al.*⁷⁴ had to be corrected due to a difference between the recent triple-point temperature and the one used by Bilkadi *et al.* for calibration purposes. The corrected temperature is given by

$$T_{90} = T_{\text{Bi},90} - 0.049 \text{ K}. \quad (3.11)$$

The sublimation pressure can be described by the correlation equation

$$\ln\left(\frac{p_{\text{sub}}}{p_t}\right) = \frac{T_t}{T} \cdot \left\{ a_1 \left(1 - \frac{T}{T_t}\right) + a_2 \left(1 - \frac{T}{T_t}\right)^{1.9} + a_3 \left(1 - \frac{T}{T_t}\right)^{2.9} \right\}, \quad (3.12)$$

with $T_t = 216.592 \text{ K}$, $p_t = 0.51795 \text{ MPa}$, $a_1 = -14.740846$, $a_2 = 2.4327015$, and $a_3 = -5.3061778$. The equation is constrained to the triple-point pressure by its functional form. Figure 2 compares group 1 and group 2 data with values calculated from Eq. (3.12). The uncertainty of the new equation is estimated to be $\Delta p_{\text{sub}} \leq \pm 250 \text{ Pa}$ for $185 \text{ K} \leq T \leq T_t$, $\Delta p_{\text{sub}} \leq \pm 100 \text{ Pa}$ for $170 \text{ K} \leq T \leq 185 \text{ K}$, and $\Delta p_{\text{sub}} \leq \pm 50 \text{ Pa}$ for $T \leq 170 \text{ K}$. Bedford *et al.*⁴⁷ concluded that the most recent value for the sublimation temperature at normal pressure ($p_0 = 0.101325 \text{ MPa}$) is $T = 194.6857 \text{ K} \pm 0.0030 \text{ K}$; iteration with Eq. (3.12) yields $T = 194.6855 \text{ K}$.

Equation (3.12) was fitted to data at temperatures above 154 K. The low temperature data of Bryson *et al.*⁷⁵ are not represented to within the uncertainty given by the authors, but the deviations do not exceed 0.01 Pa for $T > 85 \text{ K}$ and 0.0001 Pa for $T \leq 85 \text{ K}$, respectively.

3.5 Vapor Pressure

Information on the vapor pressure of carbon dioxide is given by 36 data sets; the corresponding information is summarized in Table 7 (repeatedly published data sets were only listed once). The very accurate data set of Duschek *et al.*⁵⁸ describes the vapor pressure from the triple-point temperature up to the critical temperature. Only this data set was selected to develop the new vapor pressure equation. For the data converted to the ITS-90 temperature scale, the optimi-

TABLE 6. Summary of the data sets for the sublimation pressure of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | ΔT (mK) | Δp_{sub} | Group |
|---|------|-------------|----------------------|-----------------|-------------------------|-------|
| Bois and Wills ⁶² | 1899 | 8 | 149–196 | | | 3 |
| Kuennen and Robson ⁶³ | 1902 | 6 | 195–215 | ± 32 | | 3 |
| Onnes and Weber ⁶⁴ | 1913 | 9 | 90–106 | | | 3 |
| Siemens ⁶⁵ | 1913 | 29 | 118–195 | ± 20 | | 3 |
| Wobcr and Onnec ⁶⁶ | 1913 | 15 | 104–138 | | | 3 |
| Henning ⁶⁷ | 1914 | 18 | 192–195 | | $\pm 100 \text{ Pa}$ | 3 |
| Heuse and Otto ⁶⁸ | 1931 | 19 | 193–195 | ± 2 | | 3 |
| Heuse and Otto ⁶⁹ | 1932 | 7 | 195 | ± 1 | | 3 |
| Meyers and Van Dusen ⁴⁰ | 1933 | 28 | 195–217 | | $\pm 0.02\%$ | 3 |
| Giauque and Egan ⁷⁰ | 1936 | 12 | 154–196 | ± 1 | $\pm 3 \text{ Pa}$ | 2 |
| Tickner and Lossing ⁷¹ | 1951 | 13 | 106–154 | ± 300 | | 3 |
| Ambrose ⁷² | 1955 | 16 | 179–198 | ± 1 | $\pm 4 \text{ Pa}$ | 1 |
| Hiza ⁷³ | 1970 | 1 | 216 | ± 10 | | 3 |
| Bilkadi <i>et al.</i> ⁷⁴ | 1974 | 132 | 154–217 | ± 20 | | 1 |
| Bryson <i>et al.</i> ⁷⁵ | 1974 | 62 | 70–103 | | | 2 |
| Bedford <i>et al.</i> ⁴⁷ | 1984 | 1 | 195 | ± 3 | | 1 |
| Fernandez-Fassnacht and del Rio ⁷⁶ | 1984 | 21 | 194–243 | ± 1 | $\pm 100 \text{ Pa}$ | 1 |

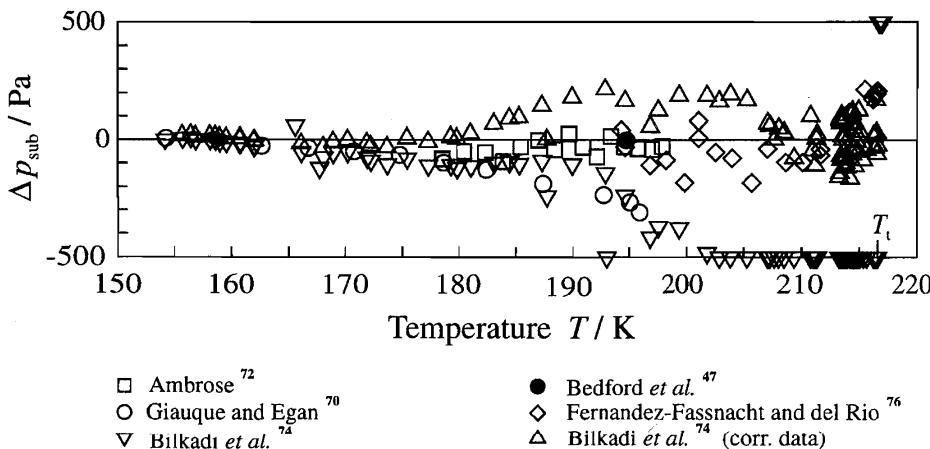


FIG. 2. Absolute deviations $\Delta p_{\text{sub}} = (p_{\text{sub,exp}} - p_{\text{sub,calc}})$ of selected experimental sublimation pressure data from values calculated from the sublimation pressure equation (3.12). In this figure, both the corrected and the uncorrected data of Bilkadi *et al.*⁷⁴ are plotted (see Sec. 3.4).

TABLE 7. Summary of the data sets for the vapor pressure of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | ΔT (mK) | Δp_s | Group |
|---|------|-------------|--------------------|-----------------|---------------------------|-------|
| Kuennen and Robson ⁶³ | 1902 | 13 | 217–273 | ± 32 | | 3 |
| Keesom ⁷⁷ | 1903 | 4 | 298–304 | ± 20 | $\pm 1000 \text{ Pa}$ | 3 |
| Jenkin and Pye ⁷⁸ | 1914 | 23 | 222–296 | ± 10 | $\pm 0.2\%$ | 3 |
| Bridgeman ⁷⁹ | 1927 | 30 | 273 | | $\pm 140 \text{ Pa}$ | 3 |
| Meyers and Van Dusen ⁴⁰ | 1933 | 67 | 217–304 | | $\pm 0.01\%$ | 2 |
| Michels <i>et al.</i> ⁸⁰ | 1936 | 9 | 276–304 | $\leq \pm 10$ | $\leq \pm 100 \text{ Pa}$ | 3 |
| Roebuck <i>et al.</i> ⁸¹ | 1942 | 10 | 223–304 | | | 3 |
| Michels <i>et al.</i> ⁸² | 1950 | 19 | 217–276 | | | 2 |
| Reamer <i>et al.</i> ⁸³ | 1951 | 2 | 279, 294 | ± 14 | $\pm 0.1\%$ | 3 |
| Bierlein and Webster ⁸⁴ | 1953 | 9 | 274–304 | ± 20 | $\pm 0.01\%$ | 2 |
| Cook ⁸⁵ | 1953 | 9 | 293–304 | ± 10 | | 3 |
| Cook ⁸⁶ | 1953 | 6 | 293–303 | ± 10 | $\pm 1000 \text{ Pa}$ | 3 |
| Schmidt and Thomas ⁸⁷ | 1954 | 6 | 274–304 | | $\pm 0.05\%$ | 3 |
| Wentorf ⁸⁸ | 1956 | 8 | 304 | ± 1 | $\pm 132 \text{ Pa}$ | 3 |
| Kletschk ⁸⁹ | 1964 | 2 | 260, 266 | | | 3 |
| Greig and Dadson ⁹⁰ | 1966 | 1 | 273 | | $\pm 0.0034\%$ | 3 |
| Edwards and Johnson ⁹¹ | 1968 | 28 | 273 | | | 3 |
| Vukalovich <i>et al.</i> ⁹² | 1968 | 4 | 301–304 | | | 3 |
| Kirillin <i>et al.</i> ⁹³ | 1969 | 3 | 283–303 | | | 3 |
| Kholodov <i>et al.</i> ⁹⁴ | 1972 | 5 | 243–283 | | | 3 |
| Levett Sengers and Chen ⁵⁰ | 1972 | 37 | 267–304 | ± 2 | $\pm 500 \text{ Pa}$ | 2 |
| Fredenslund and Mollerup ⁹⁵ | 1974 | 5 | 223–293 | ± 20 | $\pm 2000 \text{ Pa}$ | 3 |
| Gugoni <i>et al.</i> ⁹⁶ | 1974 | 3 | 241–269 | | | 3 |
| Besserer and Robinson ⁹⁷ | 1975 | 1 | 274 | ± 60 | $\pm 24000 \text{ Pa}$ | 3 |
| Davalos <i>et al.</i> ⁹⁸ | 1976 | 3 | 230–270 | ± 10 | $\pm 3000 \text{ Pa}$ | 3 |
| Stead and Williams ⁹⁹ | 1980 | 9 | 220–300 | ± 10 | $\leq \pm 0.1\%$ | 3 |
| Kwang-Bae <i>et al.</i> ¹⁰⁰ | 1982 | 5 | 263–298 | ± 30 | $\pm 3500 \text{ Pa}$ | 3 |
| Al-Sahaf <i>et al.</i> ¹⁰¹ | 1983 | 4 | 219–270 | | $\pm 0.14\%$ | 3 |
| Baade ⁵⁴ | 1983 | 227 | 220–304 | ± 3 | $\pm 80 \text{ Pa}$ | 2 |
| Fernandez-Fassnacht and del Rio ⁷⁶ | 1984 | 21 | 217–243 | ± 1 | $\pm 100 \text{ Pa}$ | 2 |
| Kratz ¹⁰² | 1984 | 7 | 289–294 | ± 3 | $\pm 0.005\%$ | 2 |
| Holste <i>et al.</i> ¹⁰³ | 1987 | 12 | 250–303 | ± 10 | | 2 |
| Brown <i>et al.</i> ¹⁰⁴ | 1988 | 4 | 220–270 | ± 20 | $\pm 0.1\%$ | 3 |
| Duschek <i>et al.</i> ⁵⁸ | 1990 | 109 | 217–304 | ± 3 | $\leq \pm 0.005\%$ | 1 |
| Shah <i>et al.</i> ¹⁰⁵ | 1991 | 2 | 276+293 | ± 20 | $\pm 0.5\%$ | 3 |
| Yurttas <i>et al.</i> ^{105a} | 1994 | 9 | 230–280 | ± 3 | $\pm 0.01\%$ | 2 |

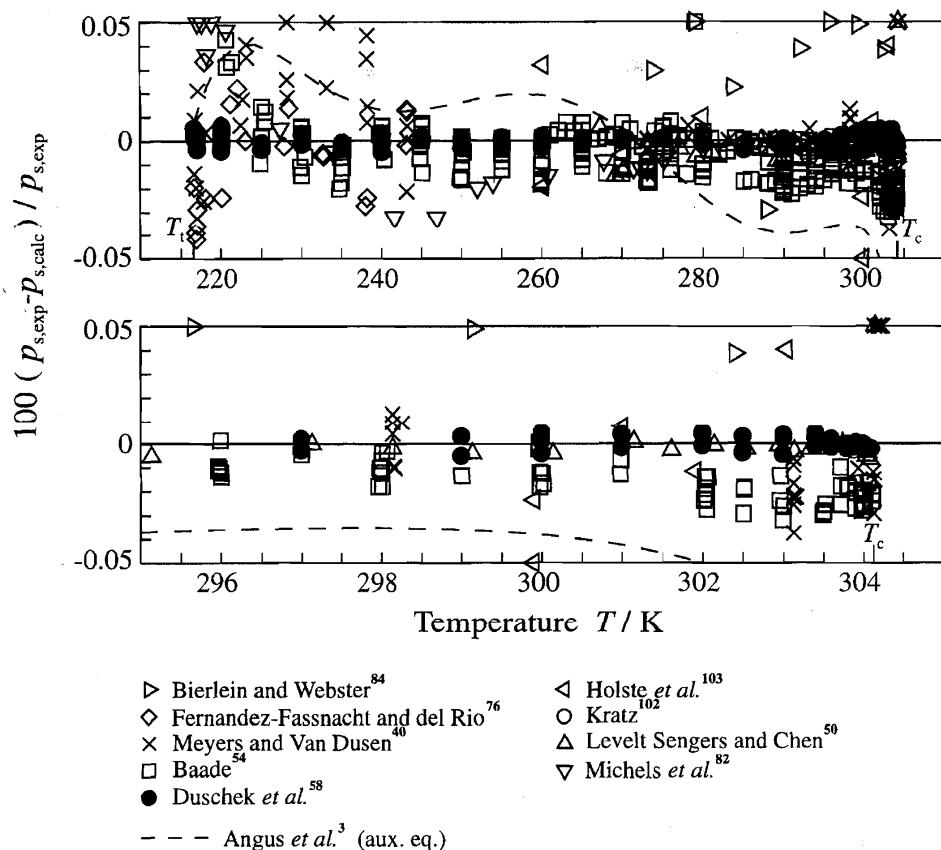


FIG. 3. Relative deviations of selected experimental vapor pressure data from values calculated from the vapor pressure equation, Eq. (3.13). Vapor pressures calculated from the corresponding equation of Angus *et al.*³ are plotted for comparison.

TABLE 8. Summary of the data sets for the saturated liquid density of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | ΔT (mK) | $\Delta \rho'$ (%) | Group |
|--|------|-------------|----------------------|-----------------|--------------------|-------|
| Amagat ¹⁰⁶ | 1892 | 35 | 273–304 | | | 3 |
| Behn ¹⁰⁷ | 1900 | 11 | 215–297 | | | 3 |
| Lowry and Erickson ¹⁰⁸ | 1927 | 8 | 267–296 | | ± 0.1 | 3 |
| Michels <i>et al.</i> ⁸⁰ | 1936 | 9 | 276–304 | $\leq \pm 10$ | | 3 |
| Reamer <i>et al.</i> ⁸³ | 1951 | 2 | 279+294 | ± 20 | ± 0.2 | 3 |
| Bierlein and Webster ⁸⁴ | 1953 | 9 | 274–304 | ± 20 | ± 0.5 | 3 |
| Cook ⁸⁵ | 1953 | 11 | 293–303 | ± 10 | ± 0.5 | 3 |
| Vukalovich <i>et al.</i> ⁹² | 1968 | 4 | 301–304 | | ± 0.5 | 3 |
| Straub ¹⁰⁹ | 1972 | 34 | 294–304 | | | 3 |
| Gugoni <i>et al.</i> ⁹⁶ | 1974 | 3 | 241–269 | | | 3 |
| Besserer and Robinson ⁹⁷ | 1975 | 1 | 274 | ± 60 | | 3 |
| Baade ⁵⁴ | 1983 | 115 | 220–304 | ± 3 | | 3 |
| Haynes ¹¹⁰ | 1985 | 17 | 220–300 | ± 30 | ± 0.1 | 2 |
| Esper ^{111,a} | 1987 | 3 | 266–303 | | ± 0.2 | 2 |
| Holste <i>et al.</i> ^{103,a} | 1987 | 3 | 266–303 | ± 10 | | 2 |
| Duscheck <i>et al.</i> ⁵⁸ | 1990 | 50 | 217–304 | ± 3 | $\pm 0.015^b$ | 1 |
| Abdulagatov <i>et al.</i> ^{59a} | 1994 | 5 | 304 | | | 3 |

^aThe data sets of Esper¹¹¹ and Holste *et al.*¹⁰³ are different evaluations of the same measurements.

^bAt temperatures above 300 K, the uncertainty rises to $\pm 0.2\%$.

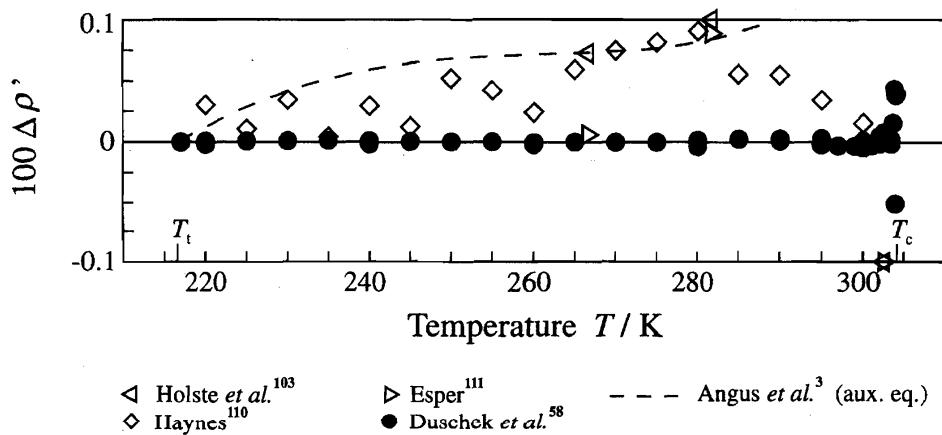


FIG. 4. Relative deviations $100 \Delta\rho' = 100 (\rho'_{\text{exp}} - \rho'_{\text{calc}})/\rho'_{\text{exp}}$ of selected experimental saturated liquid density data from values calculated from Eq. (3.14). Saturated liquid densities calculated from the corresponding equation of Angus *et al.*³ are plotted for comparison.

zation procedure yields the same mathematical form used by Duschek *et al.*⁵⁸ to describe this data set in the IPTS-68 temperature scale; only the coefficients a_i have changed. The vapor pressure equation can be written as

$$\ln\left(\frac{p_s}{p_c}\right) = \frac{T_c}{T} \cdot \left[\sum_{i=1}^4 a_i \left(1 - \frac{T}{T_c}\right)^{t_i} \right], \quad (3.13)$$

with $T_c = 304.1282$ K, $p_c = 7.3773$ MPa, $a_1 = -7.0602087$, $a_2 = 1.9391218$, $a_3 = -1.6463597$, $a_4 = -3.2995634$, $t_1 = 1.0$, $t_2 = 1.5$, $t_3 = 2.0$, and $t_4 = 4.0$.

Figure 3 shows both the good agreement between the data sets marked as group 1 and group 2 data and the representation of the data measured by Duschek *et al.*⁵⁸ Considering

the experimental uncertainty of these data, the uncertainty of Eq. (3.13) is estimated to be $\Delta p_s \leq \pm 0.012\%$ for the whole temperature range.

The dashed line in Fig. 3 corresponds to values calculated from the vapor pressure equation of Angus *et al.*³ after conversion to ITS-90. The results of this correlation are remarkably good but, of course, the most accurate data available today are not represented to within their experimental uncertainty.

3.6 Saturated Liquid Density

Table 8 shows information on the 17 data sets of the saturated liquid density of carbon dioxide. Again, only the data

TABLE 9. Summary of the data sets for the saturated vapor density of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | ΔT (mK) | $\Delta\rho''$ (%) | Group |
|--|------|-------------|--------------------|-----------------|--------------------|-------|
| Amagat ¹⁰⁶ | 1892 | 35 | 273–304 | | | 3 |
| Lowry and Erickson ¹⁰⁸ | 1927 | 8 | 267–296 | | ± 0.7 | 3 |
| Michels <i>et al.</i> ⁸⁰ | 1936 | 9 | 276–304 | $\leq \pm 10$ | | 3 |
| Reamer <i>et al.</i> ⁸³ | 1951 | 2 | 279, 294 | ± 20 | ± 0.2 | 3 |
| Bierlein and Webster ⁸⁴ | 1953 | 9 | 274–304 | ± 20 | ± 0.5 | 3 |
| Cook ⁸⁵ | 1953 | 11 | 293–303 | ± 10 | ± 0.5 | 3 |
| Vukalovich <i>et al.</i> ⁹² | 1968 | 4 | 301–304 | | ± 0.8 | 3 |
| Kholodov <i>et al.</i> ⁹⁴ | 1972 | 5 | 243–283 | | | 3 |
| Straub ¹⁰⁹ | 1972 | 34 | 294–304 | | | 3 |
| Besserer and Robinson ⁹⁷ | 1975 | 1 | 274 | ± 60 | | 3 |
| Baade ⁵⁴ | 1983 | 145 | 220–304 | ± 3 | | 3 |
| Esper ^{111,a} | 1987 | 5 | 245–304 | | ± 0.5 | 3 |
| Holste <i>et al.</i> ^{103a} | 1987 | 5 | 245–304 | ± 10 | | 3 |
| Duschek <i>et al.</i> ⁵⁸ | 1990 | 42 | 217–304 | ± 3 | $\pm 0.025^b$ | 1 |
| Abdulagatov <i>et al.</i> ^{59a} | 1994 | 2 | 304 | | | 3 |

^aThe data sets of Esper¹¹¹ and Holste *et al.*¹⁰³ are different evaluations of the same measurements.

^bAt temperatures above 295 K, the uncertainty rises to $\pm 0.25\%$.

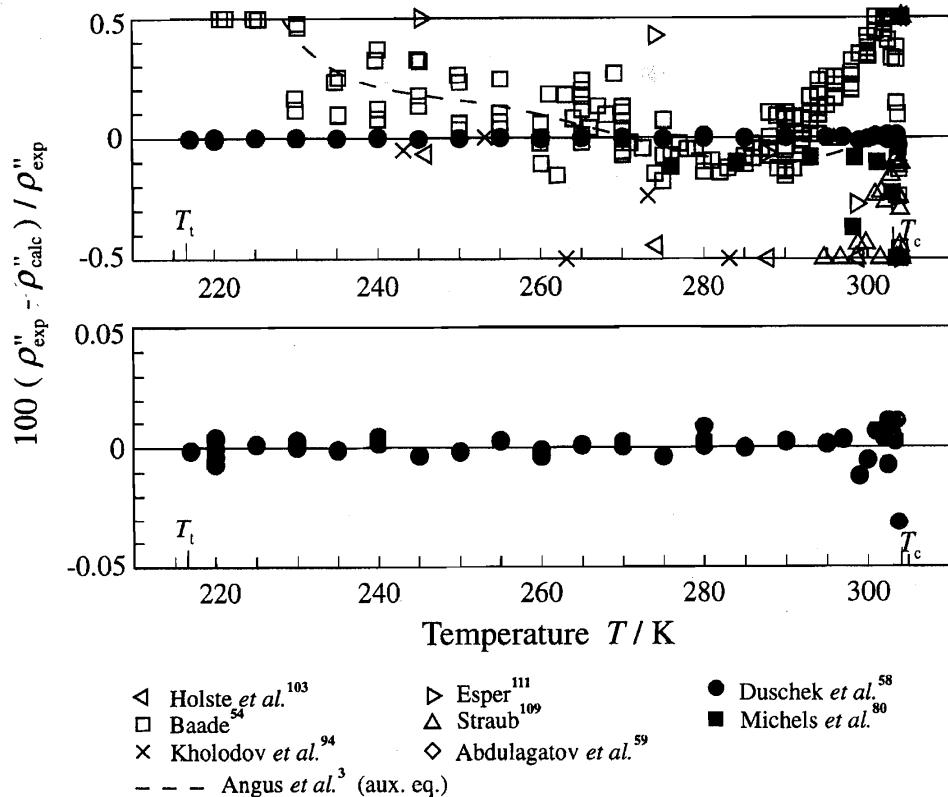


FIG. 5. Relative deviations of selected experimental saturated vapor density data from values calculated from Eq. (3.15). Saturated vapor densities calculated from the corresponding equation of Angus *et al.*³ are plotted for comparison.

set of Duscheck *et al.*⁵⁸ is used to develop a simple saturated liquid density equation. Group 2 is restricted to data sets which deliver uncertainties comparable with common uncertainties in the single phase region, that means $\Delta\rho' \leq \pm 0.2\%$ outside the critical region. Unfortunately, this criterion is only met by the data sets of Haynes,¹¹⁰ Esper,¹¹¹ and Holste *et al.*,¹⁰³ all the other data proved to be less accurate.

For the whole temperature range, the simple correlation

$$\ln\left(\frac{\rho'}{\rho_c}\right) = \sum_{i=1}^4 a_i \left(1 - \frac{T}{T_c}\right)^{t_i} \quad (3.14)$$

with $T_c = 304.1282$ K, $\rho_c = 467.6$ kg/m³, $a_1 = 1.9245108$, $a_2 = -0.62385555$, $a_3 = -0.32731127$, $a_4 = 0.39245142$, $t_1 = 0.34$, $t_2 = \frac{1}{2}$, $t_3 = \frac{10}{6}$, and $t_4 = \frac{11}{6}$ describes the data of Duscheck *et al.*⁵⁸ within their experimental uncertainty. For this equation, both the coefficients and the exponents differ from the formulation given by Duscheck *et al.*,⁵⁸ which is valid for temperatures on IPTS-68. The changed functional form of the correlation resulted in slightly improved results in the critical region. According to the uncertainty of the selected data, the uncertainty of Eq. (3.14) is estimated to be $\Delta\rho' \leq \pm 0.015\%$ for $T_i \leq T \leq 295$ K, $\Delta\rho' \leq \pm 0.04\%$ for $295 \text{ K} < T \leq 303$ K, and $\Delta\rho' \leq \pm 1\%$ for $303 \text{ K} < T \leq T_c$.

Figure 4 shows the poor situation regarding group 1 and group 2 data and the highly accurate representation of the group 1 data. The dashed line corresponds to values calculated from an auxiliary equation given by Angus *et al.*³ for the saturated liquid density.

3.7 Saturated Vapor Density

Data on the saturated vapor density of carbon dioxide are given in 15 sources, which are listed in Table 9. If the same criterion as mentioned in Sec. 3.6 is used to distinguish between group 2 and group 3 data, only the data of Michels *et al.*⁸⁰ can be assigned to group 2. While numerous authors published accurate $p\rho T$ data for the homogeneous gas region, even recent data sets of the saturated vapor density scatter by up to $\pm 0.5\%$ in density.

The new correlation equation for the saturated vapor density,

$$\ln\left(\frac{\rho''}{\rho_c}\right) = \sum_{i=1}^5 a_i \left(1 - \frac{T}{T_c}\right)^{t_i}, \quad (3.15)$$

with $T_c = 304.1282$ K, $\rho_c = 467.6$ kg/m³, $a_1 = -1.7074879$, $a_2 = -0.82274670$, $a_3 = -4.6008549$, $a_4 = -10.111178$, $a_5 = -29.742252$, $t_1 = 0.340$, $t_2 = \frac{1}{2}$, $t_3 = 1$, $t_4 = \frac{7}{3}$, and $t_5 = \frac{14}{3}$,

TABLE 10. Summary of the data sets for calorific properties on the liquid-vapor phase boundary of carbon dioxide

| Source | Year | Property | No. of data | Temp. range, T (K) | Uncertainty | Group |
|--|------|----------------|-------------|--------------------|-----------------------|-------|
| Eucken and Hauck ¹¹² | 1928 | c_σ | 8 | 223–293 | | 3 |
| Novikov and Trelin ¹¹³ | 1960 | w'' | 18 | 293–304 | | 1 |
| Amirkhanov <i>et al.</i> ¹¹⁴ | 1972 | c'_v^a | 11 | 304 | | 3 |
| Peccau and Van Daej ¹¹⁵ | 1972 | w' | 23 | 217–293 | $\Delta w' = \pm 1\%$ | 1 |
| Magee and Ely ¹¹⁶ | 1986 | c_σ | 77 | 220–303 | | 1 |
| Abdulagatov <i>et al.</i> ^{59a} | 1994 | c'_v/c''_v^a | 8 | 304 | | 3 |

^aThe specific isochoric heat capacity on the phase boundary cannot be measured directly; such data can only be determined by extrapolation from the homogeneous regions.

describes the group 1 data of Duschek *et al.*⁵⁸ within their experimental uncertainty. Compared with the corresponding equation of Duschek *et al.*,⁵⁸ both the coefficients and the exponents of the correlation have been revised in order to achieve a slightly improved representation of the data set which has been converted to the ITS-90 temperature scale. Again, the estimation of uncertainty can be guided by the experimental uncertainties. We expect the uncertainty of Eq. (3.15) to be $\Delta \rho'' \leq \pm 0.025\%$ for $T_l \leq T \leq 295$ K, $\Delta \rho'' \leq \pm 0.08\%$ for $295 \text{ K} < T \leq 303$ K, and $\Delta \rho'' \leq \pm 1\%$ for $303 \text{ K} < T \leq T_c$.

Figure 5 shows the inexplicably poor data situation, although only measurements published since 1970 and the older data of Michels *et al.*³⁰ are plotted. The data set of Duschek *et al.*⁵⁸ is the only one which enabled the development of an accurate correlation for the saturated vapor density. The correlation equation of Angus *et al.*³ yields reliable results at temperatures above 275 K, where it mainly depends on the data set of Michels *et al.*³⁰

3.8 Calorific Data on the Liquid-Vapor Phase Boundary

Table 10 lists information on the data sets which contain measurements of different calorific properties on the liquid-vapor phase boundary of carbon dioxide. No auxiliary equations have been developed for the description of these data. Instead, group 1 data have been taken into account in the development of the new equation of state, namely in the linearized form during the optimization and in the direct form during the nonlinear fit. More detailed information on these data is given in Sec. 4.9 together with the selected data describing the Maxwell criterion.

The only data which have not been taken into account by direct nonlinear fitting are the data for the specific heat capacity c_σ along the saturated liquid line. Table 3 shows that the relation between the dimensionless Helmholtz energy and c_σ contains the first derivative of the vapor pressure. Therefore, the inclusion of this property into the nonlinear fit in a direct way would involve an interlocked relation to the Maxwell criterion according to Eq. (2.2). To avoid numerical problems, the specific heat capacity along the saturated liquid line has been transformed to the specific isobaric heat capacity at saturated liquid density according to the relation

$$c_p'(T) = c_\sigma(T) - \frac{T}{(\rho')^2} \frac{\left(\frac{\partial p}{\partial T} \right)_v \frac{dp_e}{dT}}{\left(\frac{\partial \rho}{\partial p} \right)_T}. \quad (3.16)$$

Up to temperatures of 295 K, the fraction in Eq. (3.16) remains smaller than 20% of c_σ and can be determined from a preliminary equation of state with an estimated uncertainty of less than 0.5%. Thus, the uncertainty caused by the transformation is less than 0.1% in c_p' and is therefore negligible compared with the experimental uncertainty of the c_σ data measured by Magee and Ely.¹¹⁶ At temperatures above 295 K, the influence of the fractional term increases rapidly and likewise the uncertainty of the derivative $(\partial p/\partial \rho)_T$. Therefore, converted c_σ data at temperatures above 295 K were used only for comparison; see Fig. 20.

4. Experimental Basis of the New Equation of State

In this section, the data sets which describe the thermodynamic properties in the single-phase region of carbon dioxide are presented. For each property considered in this work, both general information on all available data sets and more detailed information on the selected data sets is given in corresponding tables. Again, the data sets are classified into three groups as explained in Sec. 3. Since the data situation in the homogeneous region is less unequivocal than the situation of the different properties on the phase boundaries, numerous data sets are associated with more than one group. Usually these data sets are selected in regions with a poor data situation, but they are used only for comparison in regions in which more reliable data exist.

The information given for the selected data sets comprises the uncertainties estimated by the authors, the uncertainties estimated by ourselves, and the mean square value of the weighting factor f_{wt} , defined by Eq. (2.7). Particularly for some data sets which are more than 20 years old, the uncertainties estimated by the authors and by ourselves differ considerably. The reason for this different assessment might be based on the difference between the scatter and the uncertainty of data, which was not considered by many of the

authors in the past. The uncertainties which we reviewed resulted from extensive comparisons and should be at least a reasonable estimation. These values were used in the weighting procedure.

Section 4.9 contains the corresponding information on all data used for the description of the liquid-vapor equilibrium.

4.1 Thermal Properties

Since 1903, the temperature and pressure dependence of the density of carbon dioxide has been investigated in 59 papers, covering the single-phase region with a total of 5508 data points. Table 11 presents information on the available data sets including their classification.

For temperatures of up to 360 K and pressures of up to 13 MPa, the description of the $p\rho T$ relation is based mainly on the data sets of Duschek *et al.*¹⁵⁴ and Gilgen *et al.*¹⁵⁹. These data sets are supported by the p_s , ρ' , ρ'' data measured by Duschek *et al.*,⁵⁸ by $p\rho T$ data of the gas phase supplied by Guo *et al.*¹⁵⁷ and by $p\rho T$ data on the 313 K isotherm measured by Nowak *et al.*^{160d}. All these measurements were performed using the "two-sinker" buoyancy method,¹⁶¹ which probably provides the most accurate $p\rho T$ data available today. The data from the different two-sinker apparatuses are consistent with each other far within their estimated

uncertainties. Nevertheless, in the region of overlapping (mainly at pressures between 8 MPa and 9 MPa) the data sets of Duschek *et al.*¹⁵⁴ and Gilgen *et al.*¹⁵⁹ show small systematic deviations of up to about $\pm 0.01\%$ in density.

On seven isotherms between 233 K and 523 K the two-sinker measurements are supplemented by recent measurements^{160,160b} with a new "single-sinker" apparatus^{160,160e} which allows measurements up to pressures of 30 MPa. On principle, for densities above 100 kg/m³, the accuracy of this apparatus is comparable with the accuracy of the two-sinker apparatus, but since the measurements for carbon dioxide were partly made in the test phase of the new apparatus, slightly enlarged uncertainties had to be assumed.

At pressures above 13 MPa, the adjusted data sets of Lau,¹⁴⁹ Kirillin *et al.*^{93,137,140} and Michels *et al.*¹²³ (see Sec. 4.9.2) yield a smooth continuation of the course given by the data of Gilgen *et al.*¹⁵⁹. Up to 30 MPa the adjusted data are generally consistent with the new single-sinker data within $\pm 0.05\%$ in density, but the adjusted data reach up to significantly higher pressures. Due to their high quality, these adjusted data sets are used with substantially increased weighting factors; details are given in Table 12. For temperatures between 523 K and 698 K and pressures up to 34 MPa, the recent data of Fenghour *et al.*^{160a} improve the data situ-

TABLE 11. Summary of the data sets available for the $p\rho T$ relation of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | Pressure range, p (MPa) | Group |
|---|------|-------------|----------------------|---------------------------|-------|
| Keesom ⁷⁷ | 1903 | 151 | 298–333 | 6.0–14.2 | 3 |
| Jenkin ¹¹⁷ | 1920 | 82 | 236–303 | 1.4–9.7 | 3 |
| Maas and Mennie ¹¹⁸ | 1926 | 16 | 203–373 | 0–0.1 | 3 |
| Cooper and Maas ¹¹⁹ | 1930 | 30 | 273–297 | 0–0.1 | 3 |
| Cooper and Maas ¹²⁰ | 1931 | 47 | 242–350 | 0–0.1 | 3 |
| Cawood and Patterson ¹²¹ | 1933 | 8 | 273 | 0–0.4 | 3 |
| Michels and Michels ¹²² | 1935 | 190 | 273–423 | 1.6–25.3 | 1–2 |
| Michels <i>et al.</i> ¹²³ | 1935 | 140 | 298–423 | 7.5–315.8 | 1–2 |
| Michels <i>et al.</i> ⁸⁰ | 1936 | 179 | 276–413 | 3.6–9.9 | 2 |
| Reamer <i>et al.</i> ¹²⁴ | 1944 | 147 | 344–510 | 0–70.0 | 3 |
| Bottomley <i>et al.</i> ¹²⁵ | 1950 | 1 | 295 | 0.1 | 3 |
| Batuecas and Losa ¹²⁶ | 1954 | 32 | 280–282 | 0–0.1 | 3 |
| Kennedy ^{127,a} | 1954 | | 273–1273 | 2.5–140.0 | 3 |
| Wentorf ^{88,b} | 1956 | 106 | 304 | 7.4 | 1–2 |
| Vukalovich and Altunin ¹²⁸ | 1959 | 120 | 348–773 | 2.7–32.7 | 1–2 |
| Vukalovich and Altunin ¹²⁹ | 1962 | 205 | 473–1023 | 1.1–60.0 | 1–2 |
| Vukalovich <i>et al.</i> ¹³⁰ | 1963 | 22 | 923–1076 | 2.1–15.0 | 1 |
| Vukalovich <i>et al.</i> ¹³¹ | 1963 | 124 | 313–423 | 2.1–60.0 | 1–2 |
| Juza <i>et al.</i> ^{132,c} | 1965 | 82 | 323–748 | 70.0–400.0 | 1 |
| Ku and Dodge ¹³³ | 1967 | 13 | 373 | 0.6–25.1 | 3 |
| Sass <i>et al.</i> ¹³⁴ | 1967 | 47 | 348–398 | 0.8–25.3 | 3 |
| Vukalovich <i>et al.</i> ¹³⁵ | 1968 | 168 | 273–308 | 0.8–30.0 | 2 |
| Golovskii and Tsymarnyi ¹³⁶ | 1969 | 129 | 217–303 | 13.0–60.0 | 1–2 |
| Kirillin <i>et al.</i> ¹³⁷ | 1969 | 21 | 433–473 | 2.0–69.0 | 1–2 |
| Kirillin <i>et al.</i> ⁹³ | 1969 | 39 | 283–308 | 1.6–49.2 | 1–2 |
| Kirillin <i>et al.</i> ^{138,d} | 1969 | 99 | 223–473 | 1.6–54.0 | 1–2 |
| Tsiklis <i>et al.</i> ¹³⁹ | 1969 | 50 | 323–673 | 200.0–700.0 | 1 |
| Kirillin <i>et al.</i> ¹⁴⁰ | 1970 | 24 | 223–273 | 2.0–56.0 | 1 |
| Popov and Sayapov ¹⁴¹ | 1970 | 117 | 223–303 | 0.7–30.0 | 1–2 |
| Vukalovich <i>et al.</i> ¹⁴² | 1970 | 95 | 238–268 | 0.7–19.0 | 1–2 |
| Schönmann ^{143,e} | 1971 | 85 | 373–573 | 0.4–5.9 | 3 |
| Kholodov <i>et al.</i> ¹⁴⁴ | 1972 | 141 | 293–363 | 0.5–4.8 | 3 |

TABLE 11. Summary of the data sets available for the $p\mu T$ relation of carbon dioxide—Continued

| Source | Year | No. of data | Temp. range, T (K) | Pressure range p (MPa) | Group |
|--|------|-------------|----------------------|--------------------------|-------|
| Kholodov <i>et al.</i> ⁹⁴ | 1972 | 85 | 243–283 | 0.5–4.4 | 3 |
| Levelet Sengers and Chen ⁵⁰ | 1972 | 22 | 304–319 | 7.4–10.0 | 2 |
| Straub ¹⁰⁹ | 1972 | 24 | 304 | 7.4 | 2 |
| Besserer and Robinson ¹⁴⁶ | 1973 | 76 | 310–394 | 0.7–11.0 | 3 |
| Rasskazov <i>et al.</i> ¹⁴⁷ | 1974 | 148 | 248–303 | 0.5–5.6 | 2 |
| Shmonov and Shmulovich ¹⁴⁸ | 1974 | 64 | 681–980 | 50.0–800.0 | 1 |
| Lau ¹⁴⁹ | 1986 | 69 | 240–350 | 1.6–70.0 | 1–2 |
| Esper ^{111,f} | 1987 | 73 | 246–320 | 0.1–47.7 | 1–2 |
| Holste <i>et al.</i> ^{103,f} | 1987 | 236 | 215–448 | 0.1–50.0 | 1–2 |
| Jaeschke ¹⁵⁰ | 1987 | 245 | 260–360 | 0.2–28.5 | 1 |
| Jaeschke ¹⁵¹ | 1987 | 27 | 273–353 | 0.2–30.0 | 1 |
| Magee and Ely ¹⁵² | 1988 | 10 | 250–330 | 5.8–27.1 | 1–2 |
| Ely <i>et al.</i> ¹⁷ | 1989 | 61 | 250–330 | 2.2–35.4 | 1–2 |
| Hoinkis ¹⁴⁵ | 1989 | 186 | 298–423 | 0.2–58.0 | 1–2 |
| McElroy <i>et al.</i> ¹⁵³ | 1989 | 44 | 303–333 | 0.8–6.0 | 3 |
| Duschek <i>et al.</i> ¹⁵⁴ | 1990 | 362 | 217–340 | 0.3–9.0 | 1 |
| Duschek <i>et al.</i> ^{58,g} | 1990 | 87 | 295–304 | 6.0–7.4 | 1 |
| Jaeschke <i>et al.</i> ¹⁵⁵ | 1990 | 270 | 270–320 | 0.2–12.0 | 1 |
| Nebendahl ¹⁵⁶ | 1990 | 21 | 337–413 | 1.9–4.4 | 3 |
| Guo <i>et al.</i> ¹⁵⁷ | 1992 | 40 | 273–293 | 1.0–3.3 | 1 |
| Weber ¹⁵⁸ | 1992 | 12 | 320 | 0.1–6.0 | 2 |
| Gilgen <i>et al.</i> ¹⁵⁹ | 1993 | 264 | 220–360 | 0.3–13.0 | 1 |
| Brachthäuser ¹⁶⁰ | 1993 | 29 | 233–523 | 0.8–30.1 | 1 |
| Fenghour <i>et al.</i> ^{160a} | 1995 | 120 | 330–698 | 3.0–34.2 | 1 |
| Klimeck <i>et al.</i> ^{160b} | 1995 | 60 | 300–430 | 0.5–30.1 | 1 |
| Gokmenoglu <i>et al.</i> ^{160c} | 1996 | 142 | 297–425 | 6.1–66.6 | 3 |
| Nowak <i>et al.</i> ^{160d} | 1997 | 21 | 313 | 8.4–12.1 | 1 |

^aProperty tables derived from measurements.^bData partly within the two-phase region.^cWe used the smoothed data originally published; the unsmoothed data published by Angus *et al.*³ cannot be used because of very large scatterings.^dThis paper also contains all data given in Refs. 137, 91 and 140.^eThe data of Schönmann¹⁴³ were reevaluated by Hoinkis;¹⁴⁵ the reevaluated data were considered in this work.^fThe data published by Esper¹¹¹ are reevaluations of the measurements published by Holste *et al.*¹⁰³ as experiment III.^gDuschek *et al.*⁵⁸ published $p\mu T$ data in the vicinity of the phase boundary which were used to determine saturated liquid- and vapor-densities in the near critical region.

ation significantly. The data set of Straub¹⁰⁹ was not included in the data set used for the development of the final equation, but it was used as a sensitive test for the description of the critical region.

4.2 Specific Isobaric Heat Capacity

As regards the specific isobaric heat capacity, the description of the data situation has to be split up into data sets which describe the caloric behavior of the ideal gas and data sets which in addition contain the residual behavior. While the data situation for the caloric properties of the ideal gas is dominated by theoretical approaches, the description of the real gas behavior, where both the ideal and the residual part of the heat capacity are considered, is virtually restricted to experimental investigations. In order to account for these different situations, this section is divided into two subsections.

4.2.1 Experimental Results for the Specific Isobaric Heat Capacity

Today, calorimetric measurements performed with flow apparatuses provide accurate data of the specific isobaric heat capacity over wide ranges of temperature and pressure. In the low density region, these results are usually more accurate than isochoric heat capacity measurements.

Since state-of-the-art data on the speed of sound for carbon dioxide are available only within a very limited temperature range and only up to pressures of 0.9 MPa, the data sets given in Table 13 and especially the selected data sets shown in Table 14 represent the most important source of information on the caloric behavior of carbon dioxide. While the data set of Bender *et al.*¹⁷⁷ provides an accurate description of the low density region, the data of Ernst and Hochberg¹⁷⁸ and Ernst *et al.*¹⁷⁹ allow a precise description of caloric properties up to 90 MPa. At least for subcritical pressures, the accuracy of these data sets is improved by suitable corrections; see Sec. 4.9.3.

TABLE 12. Summary of selected $p\rho T$ data for carbon dioxide; detailed information is given on the uncertainty values estimated by the authors and those estimated by ourselves and used in the weighting procedure

| Source | No. of data Mean f_{wt}^2 | Uncertainty estimated by the authors | | Source | No. of data Mean f_{wt}^2 | Uncertainty estimated by the authors | |
|---|---------------------------------------|---|---------------------------------------|--|---------------------------------------|---|---------------------------------------|
| | | Uncertainty estimated by ourselves | Uncertainty estimated by ourselves | | | Uncertainty estimated by ourselves | Uncertainty estimated by ourselves |
| Michels and Michels ¹²² | 9 | N.R.E. ^a | | Lau ^{149,c} | 42 | $\Delta\rho=0.1\%$ | |
| | 4.00 | $\Delta p=1000 \text{ Pa}$, $\Delta\rho=0.2\%$ | | | | | |
| Michels <i>et al.</i> ^{123,c} | 75 | $\Delta\rho=0.05\%$ | | Esper ¹¹¹ | 3.71 | $\Delta T=10 \text{ mK}$, $\Delta p=0.02\%$, $\Delta\rho=0.1\%$ | |
| | 1.00 | $\Delta p=0.02\%$, $\Delta\rho=0.1\%$ | | | | $\Delta\rho=0.03-0.11\%$ | |
| Wentorf ^{88,c} | 87 | $\Delta T=1 \text{ mK}$, $\Delta p=132 \text{ Pa}$, $\Delta\rho=0.02\%$ | | | 1.00 | $\Delta T=10 \text{ mK}$, $\Delta p=0.015\%$, $\Delta\rho=0.05\%$ | |
| | 0.09 | $\Delta T=2 \text{ mK}$, $\Delta p=500 \text{ Pa}$, $\Delta\rho=0.09\%$ | | Holste <i>et al.</i> ¹⁰³ | 80 | $\Delta T=10 \text{ mK}$, $\Delta p=0.015\%$, | |
| Vukalovich and Altunin ¹²⁸ | 44 | $\Delta\rho=0.15-0.35\%$ | | | 0.80 | $\Delta T=10 \text{ mK}$, $\Delta p=0.015\%$, $\Delta\rho=0.05\%$ | |
| | 1.07 | $\Delta\rho=0.4\%$ | | Jaeschke ¹⁵⁰ | 245 | N.R.E. | |
| Vukalovich and Altunin ¹²⁹ | 134 | N.R.E. | | | 0.69 | $\Delta T=5 \text{ mK}$, $\Delta p=0.1\%$, $\Delta\rho=0.1\%$ | |
| | 1.00 | $\Delta\rho=0.2\%$ | | Jaeschke ¹⁵¹ | 27 | N.R.E. | |
| Vukalovich <i>et al.</i> ¹³⁰ | 22 | N.R.E. | | | 1.14 | $\Delta T=5 \text{ mK}$, $\Delta p=0.05\%$, $\Delta\rho=0.05\%$ | |
| | 1.00 | $\Delta\rho=0.2\%$ | | Magee and Ely ¹⁵² | 9 | $\Delta T=30 \text{ mK}$, $\Delta p=0.01\%$, $\Delta\rho=0.1\%$ | |
| Vukalovich <i>et al.</i> ¹³¹ | 36 | N.R.E. | | Ely <i>et al.</i> ¹⁷ | 0.16 | $\Delta T=30 \text{ mK}$, $\Delta p=0.01\%$, $\Delta\rho=0.1\%$ | |
| | 0.64 | $\Delta\rho=0.1\%$ | | | 52 | $\Delta T=30 \text{ mK}$, $\Delta p=0.01\%$, $\Delta\rho=0.1-0.15\%$ | |
| Juza <i>et al.</i> ¹³² | 82 | $\Delta p=2 \text{ MPa}$, $\Delta\rho=0.3\%$ | | Hoinkis ¹⁴⁵ | 1.00 | $\Delta T=30 \text{ mK}$, $\Delta p=0.01\%$, $\Delta\rho=0.1-0.15\%$ | |
| | 1.00 | $\Delta T=0.2 \text{ K}$, $\Delta p=2 \text{ MPa}$, $\Delta\rho=0.4\%$ | | | 72 | $\Delta T=10 \text{ mK}$, $\Delta p=0.01\%$, $\Delta\rho=0.16\%$ | |
| Golovskii and Tsymarnyi ¹³⁶ | 108 | $\Delta T=80 \text{ mK}$, $\Delta p=0.08\%$, $\Delta\rho=0.15\%$ | | | 1.83 | $\Delta T=10 \text{ mK}$, $\Delta p=0.01\%$, $\Delta\rho=0.16\%$ | |
| Kirillin <i>et al.</i> ^{137,c} | 2.25 | $\Delta T=80 \text{ mK}$, $\Delta p=0.08\%$, $\Delta\rho=0.15\%$ | | Duschek <i>et al.</i> ¹⁵⁴ | 362 | $\Delta T=3 \text{ mK}$, $\Delta p=0.006\%$, $\Delta\rho=0.015\%$ | |
| | 17 | $\Delta\rho=0.1\%$ | | | 1.88 | $\Delta T=3 \text{ mK}$, $\Delta p=0.006\%$, $\Delta\rho=0.015\%$ | |
| Kirillin <i>et al.</i> ^{93,c} | 9.65 | $\Delta p=0.05\%$, $\Delta\rho=0.2\%$ | | Duschek <i>et al.</i> ⁵⁸ | 87 | $\Delta\rho=0.03-0.25\%$ ^d | |
| | 29 | N.R.E. | | | 2.25 | $\Delta\rho=0.03-0.25\%$ | |
| | 4.00 | $\Delta p=0.05\%$, $\Delta\rho=0.2\%$ | | Jaeschke <i>et al.</i> ¹⁵⁵ | 268 | N.R.E. | |
| Kirillin <i>et al.</i> ¹³⁸ | 66 | $\Delta\rho=0.15-0.2\%$ | | | 0.75 | $\Delta T=5 \text{ mK}$, $\Delta p=0.05-0.1\%$, | |
| | 1.00 | $\Delta p=0.05\%$, $\Delta\rho=0.2\%$ | | Guo <i>et al.</i> ¹⁵⁷ | 40 | $\Delta\rho=0.05-0.01\%$ | |
| Tsiklis <i>et al.</i> ¹³⁹ | 49 | $\Delta\rho=0.3\%$ | | | 2.25 | $\Delta T=3 \text{ mK}$, $\Delta p=0.005\%$, $\Delta\rho=0.01\%$ | |
| | 1.00 | $\Delta T=0.5 \text{ K}$, $\Delta p=1 \text{ MPa}$, $\Delta\rho=1.0\%$ | | Gilgen <i>et al.</i> ¹⁵⁹ | 264 | $\Delta T=3 \text{ mK}$, $\Delta p=0.005\%$, $\Delta\rho=0.01\%$ | |
| Kirillin <i>et al.</i> ^{140,c} | 24 | $\Delta\rho=0.1\%$ | | | 2.18 | $\Delta T=1.5 \text{ mK}$, $\Delta p=0.006\%$, $\Delta\rho=0.015\%$ | |
| | 4.00 | $\Delta p=0.05\%$, $\Delta\rho=0.1\%$ | | Brachthäuser ¹⁶⁰ | 29 | $\Delta T=1.5 \text{ mK}$, $\Delta p=0.006\%$, $\Delta\rho=0.015\%$ | |
| Popov and Sayapov ¹⁴¹ | 73 | N.R.E. | | | 1.00 | $\Delta\rho=0.016-0.051\%$ | |
| | 1.00 | $\Delta T=30 \text{ mK}$, $\Delta p=0.05\%$, $\Delta\rho=0.15\%$ | | Fenghour <i>et al.</i> ^{160a} | 120 | $\Delta\rho=0.016-0.051\%$ | |
| Vukalovich <i>et al.</i> ¹⁴² | 86 | $\Delta\rho=0.08-0.15\%$ | | | 1.00 | $\Delta\rho=0.05-0.10\%$ | |
| | 1.00 | $\Delta T=15 \text{ mK}$, $\Delta p=0.005\%$, $\Delta\rho=0.08-0.15\%$ | | Klimeck <i>et al.</i> ^{160b} | 60 | $\Delta\rho=0.10\%$ | |
| Shmonov and Shmulovich ¹⁴⁸ | 60 | $\Delta\rho=0.25-0.5\%$ | | | 1.00 | $\Delta T=6 \text{ mK}$, $\Delta p=0.006\%$, $\Delta\rho=0.02-0.04\%$ | |
| | 1.44 | $\Delta T=0.4 \text{ K}$, $\Delta p=0.2\%$, $\Delta\rho=1.0\%$ | | Nowak <i>et al.</i> ^{160d} | 21 | $\Delta T=6 \text{ mK}$, $\Delta p=0.006\%$, $\Delta\rho=0.02-0.04\%$ | |
| | | | | | 1.00 | $\Delta T=1.5 \text{ mK}$, $\Delta p=0.006\%$, $\Delta\rho=0.015\%$ | |
| | | | | | | $\Delta T=1.5 \text{ mK}$, $\Delta p=0.006\%$, $\Delta\rho=0.015\%$ | |

^aN.R.E.: No reasonable estimation given by the authors.

^bConsistency is given instead of uncertainty.

^cAdjusted values were used in the final data sets, see Sec. 4.10.

^dUncertainties given for the corresponding saturated liquid and saturated vapor densities.

The data sets of Rivkin and Gukov^{171,174} describe the supercritical region of carbon dioxide. Since empirical equations of state may produce misleading results regarding calorific properties within this region, these data sets were considered to be of great interest for the development of the new fundamental equation. Unfortunately, the data proved to be inconsistent with each other and with state-of-the-art $p\rho T$ data. Since the data given in Ref. 174 were deduced from measurements of a mixture with high carbon dioxide content,

this data set was classified in group 3. The data set given in Ref. 171 was used only with a reduced weighting factor.

4.2.2 Results for the Specific Isobaric Heat Capacity in the Ideal-Gas State

According to Eq. (2.4), knowledge of the specific isobaric heat capacity in the ideal-gas state forms the basis for the

TABLE 13. Summary of the data sets available for the specific isobaric heat capacity of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | Pressure range, p (MPa) | Group |
|---|------|-------------|--------------------|-------------------------|-------|
| Keyes and Collins ¹⁶² | 1932 | 1 | 300 | 0.2 | 3 |
| Kistiakowsky and Rice ^{163,a} | 1939 | 3 | 300–367 | 0.1 | 1 |
| de Groot and Michels ^{164,a,b} | 1948 | 92 | 298–423 | 0.1–206.5 | 3 |
| Masi and Perkof ^{165,a} | 1952 | 12 | 243–363 | 0.05–0.15 | 1 |
| Schrock ¹⁶⁶ | 1952 | 26 | 311–783 | 0.1–7.0 | 2–3 |
| Koppel and Smith ¹⁶⁷ | 1960 | 102 | 291–322 | 7.2–8.3 | 3 |
| Vukalovich <i>et al.</i> ¹⁶⁸ | 1964 | 23 | 295–355 | 0.4–8.2 | 2–3 |
| Vukalovich and Gureev ¹⁶⁹ | 1964 | 8 | 313–333 | 0.8–8.0 | 2–3 |
| Vukalovich <i>et al.</i> ¹⁷⁰ | 1965 | 86 | 293–493 | 1.0–22.2 | 2–3 |
| Rivkin and Gukov ¹⁷¹ | 1968 | 221 | 283–403 | 8.8–24.5 | 1 |
| Altunin and Kuznetsov ¹⁷² | 1969 | 36 | 293–333 | 1.0–5.0 | 2–3 |
| Altunin and Kuznetsov ¹⁷³ | 1970 | 54 | 283–373 | 1.0–6.0 | 2–3 |
| Rivkin and Gukov ^{174,c} | 1971 | 46 | 306–332 | 8.8–11.8 | 3 |
| Altunin and Kuznetsov ¹⁷⁵ | 1972 | 30 | 253–323 | 0.9–6.0 | 2–3 |
| Saegeus <i>et al.</i> ¹⁷⁶ | 1980 | 35 | 245–346 | 0.3–3.7 | 3 |
| Bender <i>et al.</i> ^{177,a} | 1981 | 60 | 233–473 | 0.1–1.5 | 1 |
| Ernst and Hochberg ^{178,a} | 1989 | 9 | 303 | 0.3–52.2 | 1 |
| Ernst <i>et al.</i> ^{179,a} | 1989 | 55 | 333–393 | 0.2–90.0 | 1 |
| Dordain <i>et al.</i> ^{179a} | 1994 | 40 | 327–416 | 5.1–25.1 | 3 |

^aThe paper also contains extrapolated values for the specific isobaric heat capacity of carbon dioxide in the ideal gas state.

^bData calculated from measurements of the $p\rho T$ relation.

^cMeasurements of a mixture with high carbon dioxide content; the results considered here were extrapolated from the mixture experiments to pure carbon dioxide.

description of the ideal-gas part of the Helmholtz energy, $A^0(\rho, T)$. Results for c_p^0 obtained by the extrapolation of c_p measurements to zero pressure (cf. Table 13) are neither accurate enough for this application nor do they cover a sufficiently wide range of temperature. Therefore, theoretical approaches which describe the caloric behavior of carbon dioxide in the ideal-gas state were reviewed.

Information on the fundamental frequencies of the carbon dioxide molecule can be found in various compilations, but

only a few papers contain reliable data on c_p^0 , where corrections to the simple rigid rotator, harmonic-oscillator model were taken into account in order to achieve high accuracy. Table 15 summarizes these data sets, of which the data set of Chao¹⁸⁴ is the most recent one. Chao considers first order corrections to the rigid rotator, harmonic-oscillator model, which were developed by Pennington and Kobe;¹⁸⁵ he estimates that the uncertainty of his results is less than $\pm 0.02\%$.

TABLE 14. Summary of selected data for the specific isobaric heat capacity of carbon dioxide; detailed information is given on the uncertainty values estimated by the authors and those estimated by ourselves and used in the weighting procedure

| Source | No. of data Mean f_{wt}^2 | Uncertainty estimated by the authors | | Uncertainty estimated by ourselves |
|---|---------------------------------------|--|------------|---------------------------------------|
| | | Δc_p | ΔT | |
| Kistiakowsky and Rice ¹⁶³ | 3 | $\Delta c_p=0.3\%$ | | |
| | 1.00 | $\Delta T=30 \text{ mK}$, $\Delta c_p=0.3\%$ | | |
| Masi and Perkof ¹⁶⁵ | 12 | $\Delta T=30 \text{ mK}$, $\Delta c_p=0.1\%$ | | |
| | 1.00 | $\Delta T=30 \text{ mK}$, $\Delta c_p=0.1\%$ | | |
| Rivkin and Gukov ¹⁷¹ | 220 | $\Delta T=10 \text{ mK}$, $\Delta p=0.05\%$, $\Delta c_p=2\%$ | | |
| | 0.17 | $\Delta T=25 \text{ mK}$, $\Delta p=0.05\%$, $\Delta c_p=2\%$ | | |
| Bender <i>et al.</i> ^{177,b} | 60 | $\Delta c_p=0.1\%–0.15\%$ | | |
| | 1.00 | $\Delta T=10 \text{ mK}$, $\Delta p=0.01\%$, $\Delta c_p=0.12\%$ | | |
| Ernst and Hochberg ^{178,b} | 9 | $\Delta c_p=0.2\%–0.9\%$ | | |
| | 2.25 | $\Delta T=20 \text{ mK}$, $\Delta p=0.1\%$, $\Delta c_p=0.2\%–0.9\%$ | | |
| Ernst <i>et al.</i> ^{179,b} | 55 | $\Delta c_p=0.2\%–0.9\%$ | | |
| | 1.92 | $\Delta T=20 \text{ mK}$, $\Delta p=0.1\%$, $\Delta c_p=0.2\%–0.9\%$ | | |

^aThe consistency is given instead of the uncertainty.

^bCorrected values were used in the final data set, see Sec. 4.10.

4.3 Specific Isochoric Heat Capacity

Seven data sets are available for the isochoric heat capacity of carbon dioxide. The information on these data sets is summarized in Table 16. More detailed information on the

TABLE 15. Data sets for the isobaric heat capacity in the ideal-gas state of carbon dioxide calculated by theoretical approaches

| Source | Year | Temp. range, T (K) |
|------------------------------------|------|--------------------|
| Wooley ¹⁸⁰ | 1954 | 50–5 000 |
| Baehr <i>et al.</i> ¹⁸¹ | 1968 | 10–6 000 |
| Gurvich ¹⁸² | 1979 | 10–10 000 |
| Chao ¹⁸³ | 1983 | 50–5 000 |
| Chao ¹⁸⁴ | 1986 | 10–1 500 |

TABLE 16. Summary of the data sets available for the specific isochoric heat capacity of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | Density range, ρ (kg/m ³) | Group |
|--|------|------------------|--------------------|--|-------|
| Eucken and Hauck ¹¹² | 1928 | 8 | 223–293 | | 3 |
| Michels and Strijland ^{186,a} | 1952 | 50 | 297–313 | 274–839 | 3 |
| Amirkhanov <i>et al.</i> ¹⁸⁷ | 1970 | 214 ^b | 280–393 | 500–831 | 2 |
| Amirkhanov and Polikhronidi ¹⁸⁸ | 1971 | 733 ^b | 276–403 | 512–903 | 1–2 |
| Edwards ⁵⁵ | 1984 | 221 ^c | 301–312 | 434–467 | 1 |
| Magee and Ely ¹¹⁶ | 1986 | 113 | 223–330 | 88–1140 | 1–2 |
| Abdulagatov <i>et al.</i> ⁵⁹ | 1991 | 331 | 304–357 | 460–510 | 1–2 |
| Abdulagatov <i>et al.</i> ^{59,a} | 1994 | 88 ^d | 304–357 | 460–510 | 1 |
| Abdulagatov <i>et al.</i> ^{59,b} | 1994 | 230 ^e | 280–357 | 460–519 | 1–2 |

^aEvaluation of the data is hindered by unclear temperature assignment.^bSome of the data are in the two-phase region.^cPreselected numerical values provided by Sengers;¹⁸⁹ 97 measurements describe states within the two-phase region.^dThese data are selected from the data given in Abdulagatov *et al.*⁵⁹^e132 data are in the two-phase region; 88 of the 98 data in the single-phase region are already known from Abdulagatov *et al.*^{59,59a}

selected data is given in Table 17. For carbon dioxide, measurements of the isochoric heat capacity are of great importance in the two regions discussed below.

The data set of Magee and Ely¹¹⁶ yields the only comprehensive description of calorific properties within the high density region. At liquid densities, this data set is limited to pressures above the critical pressure, leaving a gap between the available calorific data in the homogeneous region and on the saturated liquid curve (see Sec. 7.2.2). At densities below 600 kg/m³, these data can only be represented with systematic deviations clearly outside the uncertainty estimated by the authors. On the other hand, in this region several accurate equations of state^{3,15–17} agree with each other and with the new equation of state within about 2% for the isochoric heat capacity, and data of the isobaric heat capacity are met

within less than 0.5% by the new equation of state. Based on these facts, we concluded that deviations up to 8% in the isochoric heat capacity were probably due to shortcomings in the data set. Thus, the weighting factors were strongly reduced for the low density measurements.

Within the extended critical region, the data sets of Edwards⁵⁵ and of Abdulagatov *et al.*^{59,59a,59b} had great influence on the development of the new equation of state. (Edwards's thesis⁵⁵ only contains graphical illustrations of the results. The data used here were provided by Sengers.¹⁸⁹) The reduced weighting factors given in Table 17 were chosen because of the large number of data points within a small and very sensitive region. The use of these data sets with $f_{wt}=1$ would have resulted in an overemphasis of the critical region; details are given in Sec. 5.

The recent data of Abdulagatov *et al.*⁵⁹ were first presented in the *Proceedings of the 11th Symposium on Thermophysical Properties* in Boulder in 1991. When the corresponding paper^{59a} was published three years later, it contained only 88 data points selected from the 331 data points given in the proceedings. In the same year, another paper^{59b} was published which contains the 88 points published before, 10 additional points on one isochore in the homogeneous phase, and 132 additional points in the two

TABLE 17. Summary of selected data for the specific isochoric heat capacity of carbon dioxide; detailed information is given on the uncertainty values estimated by the authors and those estimated by ourselves and used in the weighting procedure

| Source | No. of data Mean f_{wt}^2 | Uncertainty estimated by the authors | | Uncertainty estimated by ourselves |
|--|--------------------------------|--|---|---------------------------------------|
| | | | | |
| Amirkhanov and Polikhronidi ¹⁸⁸ | 18 | $\Delta T=5$ mK, $\Delta c_v=2\text{--}4\%$ | | |
| Edwards ^{55,a} | 1.00 | $\Delta T=50$ mK, $\Delta \rho=0.05\%$, $\Delta c_v=2.5\%$ | | |
| | 124 | | $\Delta c_v=0.75\%$ ^b | |
| | 0.16 | $\Delta T=1$ mK, $\Delta \rho=0.05\%$, $\Delta c_v=2\%$ | | |
| Magee and Ely ¹¹⁶ | 80 | $\Delta T=10$ mK, $\Delta \rho=0.1\%$, $\Delta c_v=0.5\text{--}2\%$ | | |
| | 0.37 | | $\Delta T=10$ mK, $\Delta \rho=0.1\%$, $\Delta c_v=0.5\text{--}2\%$ | |
| Abdulagatov <i>et al.</i> ⁵⁹ | 233 | $\Delta \rho=0.023\%$, $\Delta c_v=2\text{--}3.5\%$ | | |
| | 0.25 | $\Delta T=10$ mK, $\Delta \rho=0.05\%$, $\Delta c_v=5\%$ | | |
| Abdulagatov <i>et al.</i> ^{59a} | 88 | $\Delta \rho=0.023\%$, $\Delta c_v=2\text{--}3.5\%$ | | |
| | 0.25 | $\Delta T=10$ mK, $\Delta \rho=0.05\%$, $\Delta c_v=5\%$ | | |
| Abdulagatov <i>et al.</i> ^{59b} | 10 | $\Delta \rho=0.023\%$, $\Delta c_v=2\text{--}3.5\%$ | | |
| | 0.25 | $\Delta T=10$ mK, $\Delta \rho=0.05\%$, $\Delta c_v=5\%$ | | |

^aAdjusted values were used in the final data set; see Sec. 4.10.^bThe precision is given instead of the uncertainty.

TABLE 18. Summary of the data sets available for the speed of sound of carbon dioxide

| Source | Year | No. of data | Temp. | Pressure | Group |
|--|------|-------------|--------------|------------------|-------|
| | | | range, T (K) | range, p (MPa) | |
| Herget ¹⁹¹ | 1940 | 195 | 301–311 | 7.0–10.3 | 2 |
| Novikov and Trelin ¹⁹² | 1962 | 236 | 288–373 | 3.0–10.0 | 1 |
| Pitayevskaya and Bilevich ^{193,a} | 1973 | 176 | 298–473 | 50.0–450.0 | 1–2 |
| Lemming ¹⁹⁴ | 1989 | 50 | 240–360 | 0.4–0.9 | 1 |

^aSmoothed data.

TABLE 19. Summary of selected data for the speeds of sound of carbon dioxide; detailed information is given on the uncertainty values estimated by the authors and those estimated by ourselves and used in the weighting procedure

| Source | No. of data Mean f_{wt}^2 | Uncertainty estimated by the authors | | Uncertainty estimated by ourselves |
|--|--------------------------------|--|---------------------|---------------------------------------|
| | | | | |
| Novikov and Trelin ¹⁹² | 234 | | N.R.E. ^a | |
| | 0.77 | $\Delta T=0.1$ K, $\Delta p=0.1\%$, $\Delta w=0.5\%$ | | |
| Pitaevskaya and Bilevich ¹⁹³ | 144 | | N.R.E. ^a | |
| | 2.25 | $\Delta T=0.1$ K, $\Delta p=0.2\%$, $\Delta w=2\%$ | | |
| Lemming ¹⁹⁴ | 44 | $\Delta T=8$ mK, $\Delta p=4.2$ mbar, $\Delta w=0.015\%$ | | |
| | 0.06 | $\Delta T=8$ mK, $\Delta p=4.2$ mbar, $\Delta w=0.015\%$ | | |

^aN.R.E.: No reasonable estimation given by the author.

phase region. The uncertainty of the data of Abdulagatov *et al.* was estimated to be at least as big as the scatter visible in the original data set.⁵⁹

The papers of Lipa *et al.*,^{190,52} which are often cited in literature on carbon dioxide, do not contain numerical results. Since the data of Edwards⁵⁵ cover the same region, were measured with the same equipment, and are less influenced by impurities,⁵⁵ the data of Lipa *et al.* were not considered in this work.

4.4 Speed of Sound

Three of the four data sets available for the speed of sound of carbon dioxide were used for the development of the new equation of state. Table 18 contains the available data sets and Table 19 gives additional information on the selected data. The data sets of Novikov and Trelin¹⁹² and of Pitaevskaya and Bilevich¹⁹³ provide important information on the extended critical region and the high pressure region, respectively. Though the quality of the data published by Lemming¹⁹⁴ is superior to the other data sets, these data were used only with reduced weighting factors. In the gas region, the residual part of the speed of sound is less than 2% of the total speed of sound at pressures below 1 MPa. Since the uncertainty of measurements is related to the total value of the speed of sound and not only to the residual part, the contribution of these data for the development of an empirical correlation describing the residual fluid behavior is very limited.

TABLE 20. Summary of the data sets available for enthalpy differences of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | | Pressure range, p (MPa) | Group |
|---------------------------------------|------|-------------|----------------------|---------|---------------------------|-------|
| | | | | | | |
| Maas and Barnes ²⁰⁰ | 1926 | 4 | 212–298 | 0.1 | 3 | |
| Koppel and Smith ¹⁶⁷ | 1960 | 102 | 291–322 | 7.2–8.3 | 3 | |
| Vukalovich and Masalov ²⁰¹ | 1964 | 54 | 423–523 | 2.5–9.8 | 2 | |
| Vukalovich and Masalov ²⁰² | 1964 | 68 | 573–773 | 2.5–9.8 | 2 | |
| Möller <i>et al.</i> ²⁰³ | 1993 | 10 | 233–358 | 15.5 | 1 | |

TABLE 21. Summary of the data sets for differences of the internal energy of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | Density range, ρ (kg/m ³) | Group |
|-----------------------|------|------------------|----------------------|--|-------|
| Krüger ²⁰⁴ | 1964 | 454 ^a | 274–325 | 190–870 | 1–2 |
| Baehr ²⁰⁵ | 1968 | 47 | 291–316 | 466 | 3 |

^aSome of the measured temperature intervals partly reach into the two-phase region.

Besides the data presented in Table 18, five papers^{195–199} are available which deal with the speed of sound in the immediate vicinity of the critical point. None of these papers, which were published between 1951 and 1970, contains numerical results. We did not try to evaluate the graphical representations given in these papers since the special problems connected with experimental work in the critical region were not adequately considered at that time.

4.5 Enthalpy

The literature sources which deal with enthalpy measurements are summarized in Table 20. The data of Vukalovich and Masalov^{201,202} and of Möller *et al.*²⁰³ were considered in this work, but only the data of Möller *et al.* were used with the uncertainties given by the authors (10 data selected, mean value of $f_{wt}^2=2.78$, $\Delta h=0.7\%$ or $\Delta h=0.6$ kJ/kg, whichever is greater). These data provide important information at high densities where the data situation for caloric properties is poor. The data of Vukalovich and Masalov^{201,202} were used to test the quality of the new equation with regard to caloric properties at high temperatures.

4.6 Internal Energy

Table 21 lists the general information on the two data sets which are available for differences of internal energy. The data measured on the critical isochore by Baehr²⁰⁵ were not used since the temperature displacement of the $(\partial u/\partial T)_v$ maximum observed by Baehr could not be explained. The 150 selected data of Krüger,²⁰⁴ which do not reach into the two-phase region, were used with estimated uncertainties of $\Delta T=40$ mK, $\Delta p=0.2\%$, $\Delta u=2\%-4\%$, and a mean weighting factor of $f_{wt}^2=0.88$. The uncertainties given by the author ($\Delta T=10$ mK, $\Delta p=0.03\%$, $\Delta u=1.4\%-3\%$) are too small to explain the scatter of the data.

4.7 Joule-Thomson Coefficient

Since data of the Joule-Thomson coefficient can only be used in the nonlinear fitting procedure and not in the linear algorithms of the optimization procedure, their influence on the development of an empirical fundamental equation is fairly small. The data of Bender *et al.*¹⁷⁷ are the only ones which were included in the data set used for the nonlinear fit

TABLE 22. Summary of the data sets available for the Joule-Thomson coefficient of carbon dioxide

| Source | Year | No. of data | Temp. range, T (K) | Pressure range, p (MPa) | Group |
|---|------|-------------|--------------------|-------------------------|-------|
| Burnett ²⁰⁷ | 1923 | 127 | 273–393 | 2.0–7.7 | 3 |
| Roebrick <i>et al.</i> ⁸¹ | 1942 | 151 | 198–573 | 0.1–20.7 | 3 |
| de Groot and Michels ^{164,a} | 1948 | 92 | 298–423 | 0.1–206.5 | 3 |
| Vukalovich <i>et al.</i> ^{206,b} | 1970 | 131 | 253–343 | 0.6–5.9 | 2 |
| Altunin and Gureev ²⁰⁸ | 1972 | 92 | 293–500 | 1.5–22.0 | 2–3 |
| Bender <i>et al.</i> ¹⁷⁷ | 1981 | 35 | 233–473 | 0.1–1.5 | 1 |
| Cusco <i>et al.</i> ^{208a,b} | 1995 | 33 | 350–500 | 1.0–4.6 | 3 |

^aJoule-Thomson coefficients calculated from measured $p\rho T$ data.^bIsothermal Joule-Thomson coefficients, $\delta_T = c_p\mu$.

(34 data were selected with $\Delta T=10$ mK, $\Delta p=0.01\%$, $\Delta \mu=0.4\%$, and $f_{wt}^2=0.36$). The data of Vukalovich *et al.*²⁰⁶ proved to be a sensitive test for the consistent description of the gas region. Table 22 gives a survey of the data sets dealing with the Joule-Thomson coefficient.

4.8 Virial Coefficients

The literature on carbon dioxide contains many papers in which information on the second and third virial coefficient is given. Table 23 summarizes the corresponding sources.

TABLE 23. Summary of the data sets available for the second and third virial coefficient of carbon dioxide. For reasons explained in the text, no data were assigned to Group 1

| Source | Year | No. of data B/C | Temp. range, T (K) | Group |
|---|------|--------------------|-----------------------|-------|
| Michels and Michels ¹²² | 1935 | 13/13 | 273–423 | 3/3 |
| Schäfer ²⁰⁹ | 1937 | 16/... | 203–273 | 3/... |
| MacCormack and Schneider ²¹⁰ | 1950 | 9/9 | 273–873 | 3/3 |
| Cottrel and Hamilton ²¹¹ | 1955 | 7/... | 303–333 | 3/... |
| Pfefferle <i>et al.</i> ²¹² | 1955 | 2/2 | 303 | 3/3 |
| Cottrell <i>et al.</i> ²¹³ | 1956 | 3/... | 303–363 | 3/... |
| Cook ²¹⁴ | 1957 | 6/... | 213–303 | 3/... |
| Masia and Pena ²¹⁵ | 1958 | 6/... | 298–423 | 3/... |
| Butcher and Dadson ²¹⁶ | 1963 | 13/13 | 263–473 | 3/3 |
| Huff and Reed ²¹⁷ | 1963 | 10/... | 298–510 | 3/... |
| Vukalovich and Masalov ²¹⁸ | 1966 | 18/18 | 423–773 | 2/3 |
| Dadson <i>et al.</i> ²¹⁹ | 1967 | 9/... | 263–398 | 3/... |
| Ku and Dodge ¹³³ | 1967 | 1/1 | 373 | 3/3 |
| Sass <i>et al.</i> ^{134,a} | 1967 | 3/... | 348–398 | 3/... |
| Timoshenko <i>et al.</i> ²²⁰ | 1970 | 9/... | 224–313 | 3/... |
| Vukalovich <i>et al.</i> ¹⁴² | 1970 | 10/10 | 253–343 | 3/3 |
| Vukalovich <i>et al.</i> ²⁰⁶ | 1970 | 14/... | 238–308 | 3/... |
| Waxman <i>et al.</i> ²²¹ | 1973 | 6/... | 273–423 | 2/... |
| Bender <i>et al.</i> ¹⁷⁷ | 1981 | 4/... | 233–263 | 3/... |
| Ohgaki <i>et al.</i> ²²² | 1984 | 2/... | 423–473 | 3/... |
| Holste <i>et al.</i> ¹³³ | 1987 | 18/16 | 217–448 | 2/2 |
| Mallu <i>et al.</i> ²²³ | 1987 | 3/... | 323–423 | 3/... |
| Hoinkis ¹⁴⁵ | 1989 | 4/4 | 298–423 | 2/2 |
| Mallu <i>et al.</i> ^{224,b} | 1989 | .../3 | 323–423 | .../3 |
| Mc Elroy <i>et al.</i> ¹⁵³ | 1989 | 4/4 | 303–333 | 3/3 |
| Duschek <i>et al.</i> ¹⁵⁴ | 1990 | 7/4 | 220–340 | 2/2 |

^aVirial expansion developed in pressure.^bThis paper additionally includes the values already published²²³ in 1987.

Recently, Span²²⁵ pointed out that it was not very useful to include experimental second and third virial coefficients into the data set used for the development of a wide-range equation. Most of the data sets descend from $p\rho T$ measurements which have been evaluated in order to determine virial coefficients. Thus, the use of the original measurements yields much better access to the desired experimental information. Furthermore, fitting an equation of state to virial coefficients is only useful if the terms of the equation corresponding to the virial coefficients are independent of each other, as is the case in a simple virial expansion. However, if an equation of state contains exponential functions, this condition is no longer met. Thus, in this article, the available values for virial coefficients were only used for comparison; none of the data sets was assigned to group 1.

At temperatures below 220 K, however, the whole contribution of the third virial coefficient [$p/(\rho RT) = \dots + C\rho^2 + \dots$] is smaller than the uncertainty of the most recent $p\rho T$ data¹⁵⁴ throughout the gas region. Therefore, at low temperatures a physically unreasonable representation of the third virial coefficient calculated from an equation of state may occur if the equation was fitted only to $p\rho T$ data. Since reliable values of the third virial coefficient cannot be established by an evaluation of experimental $p\rho T$ data in this temperature range, 13 values of the third virial coefficient were calculated from a simple polynomial equation which describes all the selected data of the different thermodynamic properties in the gas region within their experimental uncertainty and yields a reasonable plot of the third virial coefficient at low temperatures. These "artificial" data of the third virial coefficient were then used during the development of the new equation of state.

4.9 Liquid-Vapor Equilibrium

During the procedure of optimizing the structure of the new equation of state, the liquid-vapor equilibrium was used in a linearized way.^{32,30} The data set used for this purpose consists of values of $p_s(T)$, $\rho'(T)$, and $\rho''(T)$ at 205 temperatures which were calculated from Eqs. (3.13) to (3.15). These data cover the whole liquid-vapor phase boundary with temperature intervals which decrease when approaching the

TABLE 24. Summary of selected data describing the liquid-vapor phase equilibrium of carbon dioxide; detailed information is given on the uncertainty values estimated by the authors and those estimated by ourselves and used in the weighting procedure

| Source | Property | No. of data Mean f_{wt}^2 | Uncertainty estimated by the authors | Uncertainty estimated by ourselves |
|-------------------------------------|------------|--------------------------------|--|---------------------------------------|
| | | | | |
| Novikov and Trelin ^{113,b} | w'' | 18 | N.R.E. ^a | |
| | | 1.00 | $\Delta T = 10 \text{ mK}, \Delta w'' = 0.5\%$ | |
| Pecceu and Van Dael ¹¹⁵ | w' | 23 | $\Delta w' = 1\%$ | |
| | | 1.23 | $\Delta T = 0.1 \text{ K}, \Delta w' = 0.5\%$ | |
| Magee and Ely ¹¹⁶ | c_σ | 73 ^c | N.R.E. ^a | |
| | | 2.04 | $\Delta T = 10 \text{ mK}, \Delta c_\sigma = 1\%$ | |
| Duschek <i>et al.</i> ⁵⁸ | p_s | 109 | $\Delta T = 3 \text{ mK}, \Delta p_s = 0.005\%$ | |
| | | 1.00 | $\Delta T = 3 \text{ mK}, \Delta p_s = 0.005\%$ | |
| Duschek <i>et al.</i> ⁵⁸ | ρ' | 50 | $\Delta T = 3 \text{ mK}, \Delta \rho' = 0.015\%$ | |
| | | 1.00 | $\Delta T = 3 \text{ mK}, \Delta \rho' = 0.015\%$ | |
| Duschek <i>et al.</i> ⁵⁸ | ρ'' | 42 | $\Delta T = 3 \text{ mK}, \Delta \rho'' = 0.025\%$ | |
| | | 1.00 | $\Delta T = 3 \text{ mK}, \Delta \rho'' = 0.025\%$ | |

^aN.R.E.: No reasonable estimation given by the authors.

^bIn the final data set adjusted values were used; see Sec. 4.10.

^cOnly data at $T < 295 \text{ K}$ were considered; see Sec. 3.8.

critical temperature. Additionally, the group 1 calorific data already presented in Table 10 were used to fit the new equation of state.

The final equation was nonlinearly fitted directly to the phase equilibrium data of Duschek *et al.*⁵⁸ and to the calorific data. Table 24 gives detailed information on the experimental calorific and thermal data used for the description of the liquid-vapor equilibrium.

4.10 Adjustment of Data

In order to achieve a final data set which is as consistent as possible, some of the selected data had to be adjusted. As a result, three groups of data can be distinguished which were corrected for different reasons. These three groups are explained in the following subsections.

4.10.1 Adjustment of Data Sets Describing the Critical Region

For the description of the thermodynamic surface in the immediate vicinity of the critical point, the difference between the measured temperature and the critical temperature is more important than the absolute temperature, and this temperature difference is probably also less influenced by systematic deviations or by impurities of the sample. If the corresponding critical temperature is given, the absolute temperature can be corrected by the difference between this value and the value used in this work [cf. Eq. (3.5)]. This technique was used for two important sets of calorific data:

$$\text{Edwards}^{55}: \quad T_{68} = T_{\text{Ed.}} + 29.8 \text{ mK}, \quad (4.1)$$

$$\text{Novikov and Trelin}^{113}: \quad T_{48} = T_{\text{No.}} - 44 \text{ mK}. \quad (4.2)$$

Wentorf⁸⁸ did not give any information on the critical temperature corresponding to his $p\rho T$ data, but a similar correc-

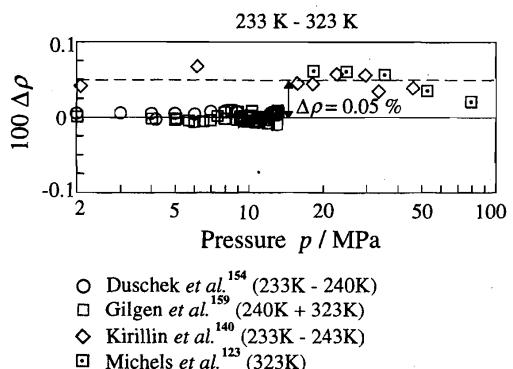


FIG. 6. Relative deviations $100 \Delta\rho = 100 (\rho_{\text{exp}} - \rho_{\text{calc}})/\rho_{\text{exp}}$ of experimental $p\rho T$ data from values calculated from Eq. (6.1). This figure illustrates the reason for adjusting the data of Kirillin *et al.*¹⁴⁰ and Michels *et al.*¹²³ (see Sec. 4.10.2).

tion can be established based on the pressure on the critical isochore. In reasonable accordance with earlier suggestions,^{154,24,17,50} we used

$$\text{Wentorf}^{88}: \quad T_{48} = T_{\text{We.}} - 27 \text{ mK}. \quad (4.3)$$

4.10.2 Adjustment of $p\rho T$ Data

Reasonable adjustments can be applied to $p\rho T$ measurements if systematic deviations occur in a region where a data set and a set of reference data overlap. In this way, accurate information on the $p\rho T$ relation can be obtained up to pressures of approximately 100 MPa, whereas the two-sinker data of Duschek *et al.*¹⁵⁴ and Gilgen *et al.*¹⁵⁹ are limited to 9 MPa and 13 MPa, respectively and the single-sinker data of Brachthäuser¹⁶⁴ and Klimeck *et al.*^{160b} are limited to 30 MPa.

Such simple corrections were used for the data sets of the following:

$$\text{Kirillin et al.}^{137,93,140}: \quad \rho = \rho_{\text{Kl.}} 0.9995, \quad (4.4)$$

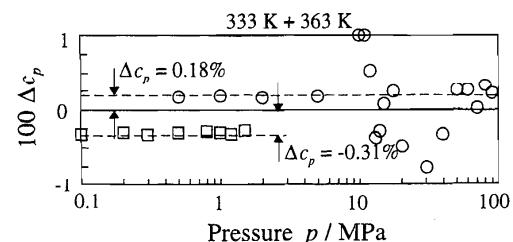


FIG. 7. Relative deviations $100 \Delta c_p = 100 (c_{p,\text{exp}} - c_{p,\text{calc}})/c_{p,\text{exp}}$ of experimental c_p data from specific isobaric heat capacities calculated from Eq. (6.1). This figure illustrates the reason for correcting the data of Ernst *et al.*¹⁷⁹ and Bender *et al.*¹⁷⁷ (see Sec. 4.10.3).

TABLE 25. Temperature dependent corrections of isobaric heat capacity data

| Temperature, <i>T</i> (K) | $\frac{c_{p,\text{cor.}} - c_{p,\text{exp.}}}{c_{p,\text{exp.}}}$ |
|-------------------------------------|---|
| Bender <i>et al.</i> ¹⁷⁷ | |
| 233 | +0.40% |
| 243 | +0.25% |
| 273 | +0.13% |
| 323 | +0.05% |
| 363 | +0.31% |
| 393 | +0.14% |
| 423 | +0.10% |
| 473 | -0.17% |
| Ernst and Hochberg ¹⁷⁸ | |
| 303 | +0.36% |
| Ernst <i>et al.</i> ¹⁷⁹ | |
| 333 | 0.18% |
| 363 | $\pm 0.00\%$ |
| 393 | -0.37% |

$$\text{Michels } \textit{et al.}^{123}: \quad \rho = \rho_{\text{Mi.}} \cdot 0.9995, \quad (4.5)$$

$$\text{Lau}^{149}: \quad \rho = \rho_{\text{La.}} \cdot 0.9993. \quad (4.6)$$

Figure 6 shows an example for the justification of these adjustments by combining two very different isotherms in a single deviation plot. The 99 measurements published by Kirillin *et al.* only in Ref. 138 cannot be adjusted according to Eq. (4.4). The corrected data of Michels *et al.*¹²³ were used only at pressures above 18 MPa. In regions where the temperature and pressure dependence of the density is strong, the data adjusted according to Eq. (4.5) also yield unsatisfactory results.

During the last 20 years, different authors^{50,21,24,27} have suggested corrections for the temperature scale used by Michels *et al.*^{80,123} and Michels and Michels.¹²² Possible corrections were tested in this work, but no reasonable temperature shift between the ITS-27 temperature scale and the temperature scale used at the Van der Waals laboratory at that time could be established. If the systematic deviation of these data is due to errors in the temperature scale, different scales have to be assumed for the measurements published in different papers of Michels. Since the data situation in the gas and extended critical region has improved significantly, it was decided not to use Michels' data within these regions.

4.10.3 Correction of Isobaric Heat Capacities

Since the low pressure limit of the isobaric heat capacity, c_p^0 , is known very well for carbon dioxide (see Sec. 6.1), temperature dependent errors of measured isobaric heat capacities can be determined easily. Figure 7 shows systematic deviations of data measured by Bender *et al.*¹⁷⁷ and by Ernst *et al.*¹⁷⁹ Again, two different isotherms are combined in a single deviation plot. A systematic error of the new equation for the residual part of the Helmholtz energy, Eq. (6.5), would result in deviations which increase with pressure since the residual contribution to the isobaric heat capacity increases.

To compensate for these temperature-dependent deviations, the data sets of Bender *et al.*,¹⁷⁷ Ernst and Hochberg,¹⁷⁸ and Ernst *et al.*¹⁷⁹ were corrected according to the values given in Table 25.

5. Description of Thermodynamic Properties in the Critical Region

It is well known^{56,226} that thermodynamic properties can be described by so called "power laws" along certain paths throughout the critical region of a pure fluid. This kind of description, which was originally introduced in 1896 by Verschaffelt²²⁷ as an empirical attempt, has been supported by recent theoretical results. In particular, the renormalization group approach introduced by Wilson²²⁸ extended knowledge on the behavior of pure fluids in the critical region and resulted in "universal" values for the critical exponents. These values are defined as power-law exponents in the limit of vanishing distance to the critical point. Table 26 shows some of the most important power laws and gives different values for the corresponding critical exponents, which were established by evaluation of the renormalization group theory,⁵⁶ by expansion of a classical equation with a so-called three-point contact at the critical point, and by expansion of a classical equation with a so-called five-point contact at the critical point. None of the classical equations is able to reproduce the values predicted by the renormalization group theory.

TABLE 26. Examples for power laws describing thermodynamic properties along certain paths throughout the critical region

| Property | Power law | Described path | Critical exponent | Values determined by evaluation of | | |
|----------------------------|---|----------------|-------------------|------------------------------------|--------------------------|--------------------------|
| | | | | RG theory ^a | 3-point eq. ^b | 5-point eq. ^c |
| Densities at saturation | $(\rho' - \rho'') \sim (T_c - T)^{\beta}$ | phase boundary | β | 0.326 ± 0.002 | 0.5 | 0.25 |
| Isothermal compressibility | $K_T \sim T - T_c ^{-\gamma}$ | crit. isochore | γ | 1.239 ± 0.002 | 1 | 1 |
| Pressure | $ p - p_c \sim \rho - \rho_c ^{\delta}$ | crit. isotherm | δ | 4.80 ± 0.02 | 3 | 5 |
| Isochoric heat capacity | $c_v \sim T - T_c ^{-\alpha}$ | crit. isochore | α | 0.110 ± 0.003 | 0 | 0 |

^aAccording to Sengers and Levelt Sengers.⁵⁶

^bSuch an equation of state is constrained at the critical point by the conditions $(\partial p / \partial \rho)_T = 0$ and $(\partial^2 p / \partial \rho^2)_T = 0$, where $(\partial^3 p / \partial \rho^3)_T > 0$.

^cIn addition to the conditions given in footnote b this equation yields $(\partial^3 p / \partial \rho^3)_T = 0$ and $(\partial^4 p / \partial \rho^4)_T = 0$, where $(\partial^5 p / \partial \rho^5)_T > 0$.

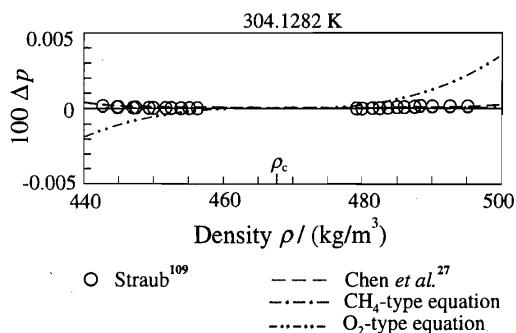


FIG. 8. Relative deviations $100 \Delta p = 100 (p_{\text{exp}} - p_{\text{calc}})/p_{\text{exp}}$ of experimental $p\rho T$ data on the critical isotherm from values calculated from Eq. (6.1). Values calculated from the crossover equation of Chen *et al.*²⁷ and from refitted equations using the CH_4 - and O_2 -form (see Sec. 5.1) are plotted for comparison.

5.1 Limitations of Analytical Equations of State

Usually it is concluded that analytic equations of state cannot represent the properties of pure fluids within the critical region because they do not yield correct critical exponents. For most of the properties considered in this article, this conclusion is incorrect if state-of-the-art equations are considered.

In this section, the results obtained within the critical region from two wide-range equations are compared with experimental results and with values which were calculated from a nonanalytic equation especially designed for the description of the extended critical region. For this purpose, we chose the crossover equation of Chen *et al.*²⁷ The critical parameters of the crossover equation were changed to the values used in this work because otherwise the comparison of equations with different critical parameters would produce misleading results in the immediate vicinity of the critical point. To give an example, which is typical for a modern wide-range equation, we fitted the equation published by Schmidt and Wagner⁴ for oxygen to the data set used in this work; this equation is referred to as O_2 -type equation. The equations of Ely¹⁴ and Ely *et al.*¹⁵ use the same functional form but these equations are constrained to different critical parameters. To illustrate the limits of an analytic equation of state, we refitted the formulation published by Setzmann and Wagner³⁰ for methane which is referred to as a CH_4 -type equation. As far as the description of the critical region is concerned, this equation is probably the most efficient analytic equation available today.

Figure 8 shows the relative deviation between pressures calculated from the new equation of state for carbon dioxide [Eq. (6.1)], from the refitted CH_4 - and O_2 -type equations, and from the crossover equation of Chen *et al.*,²⁷ compared with the very consistent data measured by Straub,¹⁰⁹ directly on the critical isotherm of carbon dioxide. (None of the wide-range equations was fitted to the data of Straub; these data only served as a consistency check for the critical region; cf. Sec. 4.1.) In the resolution chosen in Fig. 8, only the

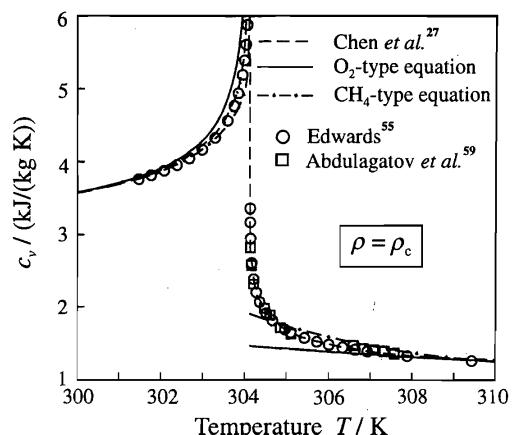


FIG. 9. Representation of representative isochoric heat capacity data in the critical region. The plotted curves correspond to values calculated from the crossover equation of Chen *et al.*²⁷ and from refitted equations using the CH_4 - and O_2 -form (see Sec. 5.1).

O_2 -type equation shows the too steep course of the critical isotherm which is to be expected from an analytic equation of state. The analytic CH_4 -type equation and the new equation of state yield almost identical results and represent the data as accurately as the crossover equation, even though they do not result in the limit for the corresponding critical exponent δ which is predicted by the renormalization group theory.

Along the critical isotherm, $p\rho T$ data can be very accurately described with a wide-range equation because the corresponding power law describes pressure differences which vanish when approaching the critical point (cf. Table 26). Thus, different values for the critical exponent δ , which is defined as limit $|\rho - \rho_c| \rightarrow 0$, hardly effect the representation of the $p\rho T$ surface. Most of the properties considered in this article show a similar behavior when approaching the critical point.

However, there are two properties which behave in a completely different way: the specific isochoric heat capacity, c_v , and the speed of sound, w . The evaluation of analytic equations yields a critical exponent $\alpha=0$, which results in a finite value of c_v at the critical point, whereas the renormalization group theory predicts $\alpha=0.110$, resulting in a slow divergence of the specific isochoric heat capacity at the critical point.

Figure 9 shows measured specific isochoric heat capacities on the critical isochore of carbon dioxide and the corresponding values calculated from the O_2 -type equation, the CH_4 -type equation, and the crossover equation. When approaching the critical temperature, only the crossover equation is able to follow the steep course of the data. The CH_4 -type equation fails within an interval of approximately ± 0.5 K around the critical temperature and the O_2 -type equation fails within an interval of approximately ± 2 K.

Similar results can be obtained for the speed of sound since it is related to the reciprocal value of the isochoric heat

capacity. From a theoretical point of view, the speed of sound is expected to vanish at the critical point, whereas analytic equations yield only a finite minimum. Again, the temperature interval, where the analytic equations fail, extends over approximately ± 0.5 K and ± 2 K, respectively, around the critical temperature.

5.2 Use of Nonanalytic Terms as an Integral Component in an Empirical Wide-Range Equation of State

The performance of a sophisticated analytic equation of state, such as the CH₄-type equation, is completely sufficient for any technical application within the critical region. However, because of the scientific importance of the critical region of carbon dioxide, an improved description of caloric properties was regarded as desirable at least as long as the numerical expense for the evaluation of the resulting correlation remains justifiable. Therefore, we rejected models which employ an iterative procedure for the relation between the physical variables T and ρ and the mathematical variables used, like switching^{3,229} and transformation²⁶ approaches.

In the context where the fundamental equation presented in this article is clearly empirical, an asymptotic behavior corresponding to the predictions of the renormalization group theory was considered to be of minor importance; mixing up theoretical and empirical approaches may even produce misleading results. Therefore, the attempt was made to extend the qualitatively correct behavior of an empirical wide-range equation to the immediate vicinity of the critical point by introducing special nonanalytic terms.

The development of such formulations started with an examination of the relations between the reduced Helmholtz energy and caloric properties. The specific isobaric heat capacity can be expressed as

$$\frac{c_p}{R} = \underbrace{\frac{c_v}{R}}_{\sim \left(\frac{\partial p}{\partial \rho}\right)_T} + \underbrace{\frac{(1 + \delta\phi_r^r - \delta\tau\phi_{\delta\tau}^r)^2}{1 + 2\delta\phi_r^r + \delta^2\phi_{\delta\delta}^r}}_{\sim \left(\frac{\partial p}{\partial T}\right)_\rho}. \quad (5.1)$$

where R corresponds to the specific gas constant, ϕ to the ideal (superscript o) and residual (superscript r) part of the reduced Helmholtz energy, τ to the inverse reduced temperature, and δ to the reduced density. The quantities τ and δ used as subscripts indicate the corresponding derivative of ϕ ; see the footnote of Table 3. Since $(\partial p / \partial \rho)_T^{-1}$ grows much faster when approaching the critical point than c_v , in Eq. (5.1) the specific isobaric heat capacity is dominated by the fraction, which is closely related to the representation of $p\rho T$ data. Thus, an equation which yields an accurate de-

scription of the $p\rho T$ surface within the critical region should also yield reliable values of the specific isobaric heat capacity.

The situation is different for the isochoric specific heat capacity which is given by

$$\frac{c_v}{R} = -\tau^2(\phi_{\tau\tau}^o + \phi_{\tau\tau}^r). \quad (5.2)$$

If the second derivative of the residual part of the Helmholtz energy with respect to τ is finite at the critical point, the value of the specific isochoric heat capacity is also finite. Only an equation with a nonanalytic behavior in $\phi_{\tau\tau}^r$ can reproduce the expected divergence in c_v . At the same time, such a formulation would result in vanishing values of the speed of sound since w corresponds to

$$\frac{w^2}{RT} = \underbrace{1 + 2\delta\phi_r^r + \delta^2\phi_{\delta\delta}^r}_{\sim \left(\frac{\partial p}{\partial \rho}\right)_T} - \underbrace{\frac{(1 + \delta\phi_r^r - \delta\tau\phi_{\delta\tau}^r)^2}{\tau^2(\phi_{\tau\tau}^o + \phi_{\tau\tau}^r)}}_{-\frac{c_v}{R}}. \quad (5.3)$$

At the critical point, the expression $(\partial p / \partial \rho)_T$ becomes zero and $(\partial p / \partial T)_\rho$ is a finite value. Thus, if c_v becomes infinite, the speed of sound becomes zero.

Consequently, a formulation has been developed which can be included into an empirical wide-range equation of state as a regular contribution to the usual sum of terms and which yields the intended nonanalytic behavior of $\phi_{\tau\tau}^r$. Such a formulation has to fulfill three additional conditions:

- The values resulting for $\phi_{\tau\tau}^r$ have to be finite everywhere except at the critical point.
- Singular behavior of the other second derivatives and all derivatives with respect to δ has to be avoided everywhere. However, there are no further restrictions for the behavior of these derivatives—the *complete* equation of state has to be designed to behave in a special way and not only a single term in the equation.
- Within the δ, τ surface of the critical region, the maximum of $\phi_{\tau\tau}^r$ has to follow the course of the saturated vapor and saturated liquid line in order to avoid unreasonable c_v maxima in the single-phase region.

These conditions can be fulfilled if a formulation of the following mathematical form is introduced as the i th term in an equation for the residual part of the Helmholtz energy, namely

$$\phi_i^r = n_i \Delta^{b_i} \delta \exp[-C_i(\delta - 1)^2 - D_i(\tau - 1)^2] \quad (5.4)$$

with

$$\Delta = \{(1 - \tau) + A_i[(\delta - 1)^2]^{1/(2\beta_i)}\}^2 + B_i[(\delta - 1)^2]^{a_i}.$$

The exponential function damps the influence of this expression outside the critical region. The distance function Δ^{b_i} introduces the nonanalytic behavior and ensures that the

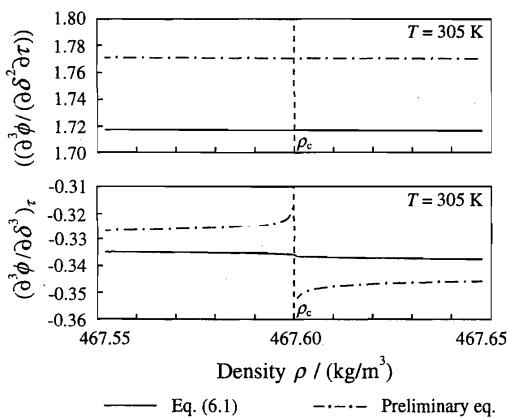


FIG. 10. While preliminary equations of state showed a discontinuous plot of the third density derivative of the reduced Helmholtz energy, the new equation of state, Eq. (6.1), yields continuous plots for the third derivatives.

maximum in c_v follows the phase boundary. Finally, the reduced density in the product of ϕ_i^r guarantees a physically correct behavior in the low-density limit.

Besides the coefficients n_i , Eq. (5.4) introduces seven “internal” parameters (A_i , B_i , C_i , D_i , a_i , b_i , β_i) for each of the terms i ; in principle, these parameters can be included into a nonlinear fit of the entire equation. However, because of the highly correlated influence of these parameters, a simultaneous nonlinear fit turned out to be very difficult. Therefore, we decided to determine reasonable starting values for B_i , C_i , a_i , and b_i with our optimization strategy. The subsequent nonlinear fit of b_i , C_i , and D_i resulted only in minor improvements of the equation. B_i and a_i were not refitted in the current project. On principle, A_i and β_i correspond to the proportionality factor and to the critical exponent of the power law describing the densities of saturated liquid and saturated vapor (see Table 26) and can be independently determined. In the final bank of terms (see Table 30) a value for β_i was used which is slightly smaller than the value expected for the corresponding critical exponent in order to fulfill the conditions

$$b_i > 0.5 + \beta_i \quad (5.5)$$

and

$$\beta_i < \frac{1}{2a_i(1-b_i)+2}. \quad (5.6)$$

Equations (5.5) and (5.6) result from the condition that singular behavior has to be avoided everywhere except for derivatives of at least second degree with respect to temperature at the critical point. Unpublished preliminary equations did not fulfill these conditions and resulted in a discontinuous plot of the third density derivative of the reduced Helmholtz energy, $(\partial^3\phi/\partial\delta^3)_T$, at the critical isochore. Figure 10 shows an example for this possible misbehavior and shows that the final equation, Eq. (6.1), results in a continuous plot of the crucial third derivatives.

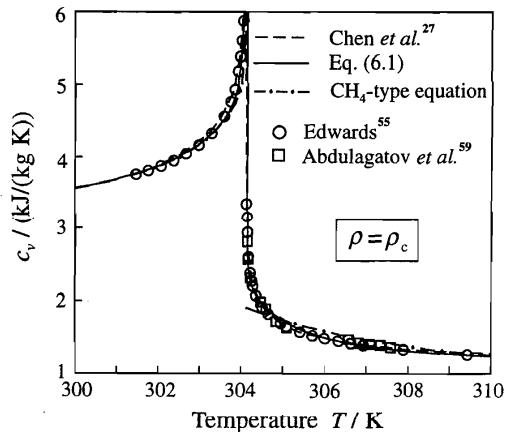


FIG. 11. Representation of representative isochoric heat capacity data in the critical region. The plotted curves correspond to values calculated from Eq. (6.1), the crossover equation of Chen *et al.*,²⁷ and a refitted equation using the CH₄-form (see Sec. 5.1).

The smallest exponent b_i occurring in the equation of state is related to the critical exponent α , which describes the divergence of the specific isochoric heat capacity, by the expression

$$b_i = 1 - \frac{\alpha}{2}. \quad (5.7)$$

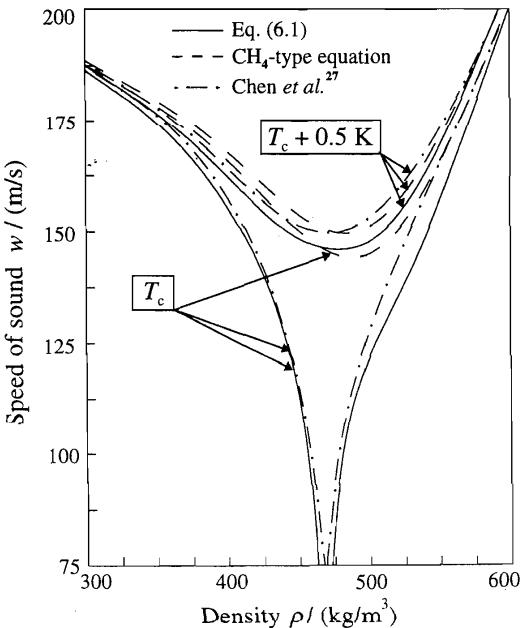


FIG. 12. Representation of the speed of sound on isotherms in the critical region. The plotted curves correspond to values calculated from Eq. (6.1), the crossover equation of Chen *et al.*,²⁷ and a refitted equation using CH₄-form (see Sec. 5.1).

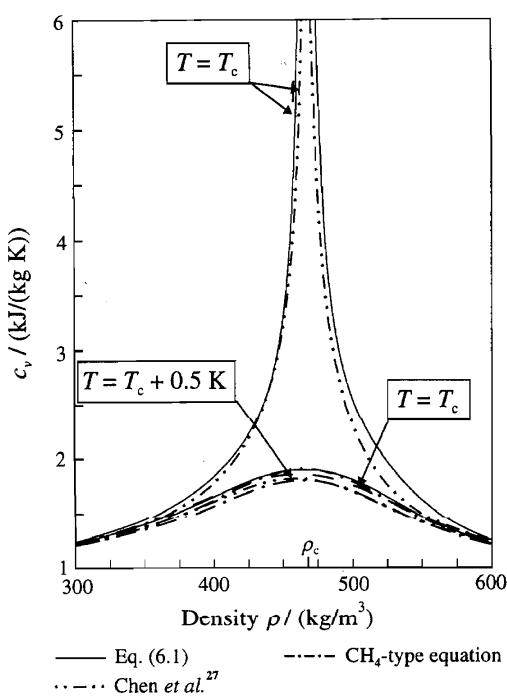


FIG. 13. Representation of the isochoric heat capacity on isotherms in the critical region. The plotted curves correspond to values calculated from Eq. (6.1), the crossover equation of Chen *et al.*,²⁷ and a refitted equation using the CH₄-form (see Sec. 5.1).

However, in combination with the sum of all terms of the entire equation of state, the asymptotically expected leading value of $b_1=0.945$ yielded unsatisfactory results. This discrepancy is discussed later in this section.

The final equation of state for carbon dioxide, which is presented in detail in Sec. 6, has been developed by the use of nonanalytic terms corresponding to Eq. (5.4). The procedure optimizing the structure of the equation of state was restricted to a maximum of four nonanalytic terms within a total number of 42 terms. Preliminary correlations with more than four nonanalytic terms tended to have an unreasonable behavior concerning the dependence of c_v and w on density in the critical region; moreover, when using more than four of such complex terms, the numerical expense would have been increased without a significant improvement in the quality of the equation. Anticipating Sec. 6 with regard to the critical region, Eq. (6.1) will be discussed in this section to avoid repeating a discussion of the representation of caloric properties in the critical region later in this paper.

Figure 11 shows the plot of c_v on the critical isochore; for analytic equations of state this plot was already shown in Fig. 9. In this figure, however, the solid line corresponds to Eq. (6.1). In contrast to the analytic CH₄-type equation, the new formulation is able to follow the strong curvature of the c_v plot in the immediate vicinity of the critical temperature and yields an infinite value for the specific isochoric heat capacity at the critical point. Accordingly, the evaluation of

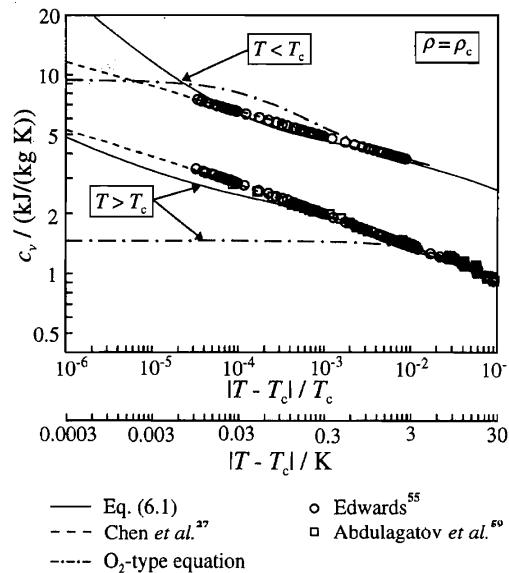


FIG. 14. Representation of experimental isochoric heat capacity data in the single phase ($T > T_c$) and two phase ($T < T_c$) region in a double logarithmic diagram. The plotted curves correspond to data on the critical isochore calculated from Eq. (6.1), the crossover equation of Chen *et al.*,²⁷ and a refitted equation using the O₂-form (see Sec. 5.1).

Eq. (6.1) yields a vanishing speed of sound at the critical point. Figure 12 shows the curve of the speed of sound, plotted on two isotherms as function of density. At the isotherm $T_c+0.5$ K, the analytic CH₄-type equation, the crossover equation of Chen *et al.*,²⁷ and Eq. (6.1) result in very

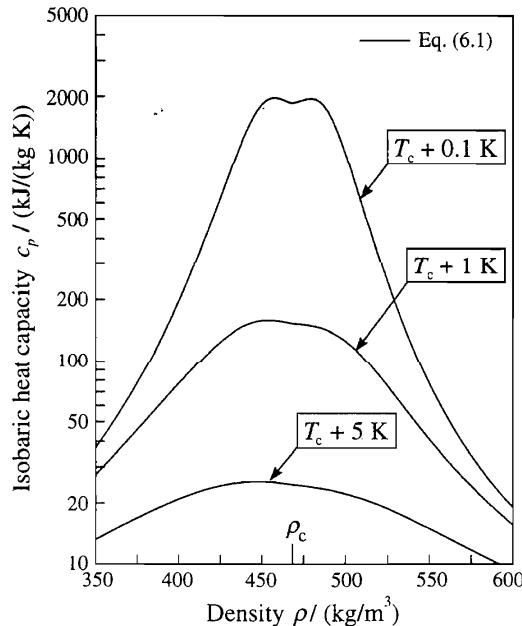


FIG. 15. For temperatures between T_c and T_c+1 K Eq. (6.1) results in an oscillating plot for the isobaric heat capacity around the critical density.

TABLE 27. Coefficients of the correlation equations, Eq. (6.2) and Eq. (6.3), for c_p^0 and ϕ^0 , respectively

| i | a_i^0 | θ_i^0 | i | a_i^0 | θ_i^0 |
|-----|---------------|--------------|-----|--------------|--------------|
| 1 | 8.373 044 56 | | 5 | 0.621 052 48 | 6.111 90 |
| 2 | -3.704 543 04 | | 6 | 0.411 952 93 | 6.777 08 |
| 3 | 2.500 000 00 | | 7 | 1.040 289 22 | 11.323 84 |
| 4 | 1.994 270 42 | 3.151 63 | 8 | 0.083 276 78 | 27.087 92 |

similar values for the speed of sound. However, on approaching the critical temperature, both the crossover equation and the nonanalytic wide-range equation, Eq. (6.1), develop a sharp minimum in the speed of sound, whereas the speed of sound calculated from the analytic equation does not change significantly when approaching the critical temperature. Within the same density range, Fig. 13 shows the corresponding plots of the specific isochoric heat capacity calculated from the same set of equations.

Thus, Eq. (6.1) is the first wide-range equation which yields a nonanalytic behavior of the isochoric heat capacity and the speed of sound in the immediate vicinity of the criti-

cal point and which is still explicit in the physical variables T and ρ . In Sec. 7 it will be shown that this nonanalytic behavior does not affect the quality of the equation with respect to the representation of other properties anywhere outside the critical region.

Nevertheless, empirical equations of state containing nonanalytic terms have certain limits if an exact fulfillment of the asymptotic power laws is required. The nonanalytic terms in Eq. (6.1) do not replace the contribution of the analytic terms in the surrounding of the critical point but they fill the increasing gap between the analytic and nonanalytic behavior. Therefore, efficient values of the exponent b_i are smaller than theoretically expected and result in a critical exponent α which is too large from an asymptotic point of view [see Eq. (5.5)].

Figure 14 shows that Eq. (6.1) represents the measured and theoretically predicted values of c_v without significant deviations for temperatures in the region $|T - T_c| > 0.2$ K and within about $\pm 10\%$ for $0.2 \text{ K} \geq (T - T_c) \geq 0.3 \text{ mK}$ in the homogeneous phase and for $-0.2 \text{ K} \leq (T - T_c) \leq -10 \text{ mK}$ in the two-phase region. The plotted c_v courses correspond to the critical isochore in the one- ($T > T_c$) and two-phase ($T < T_c$)

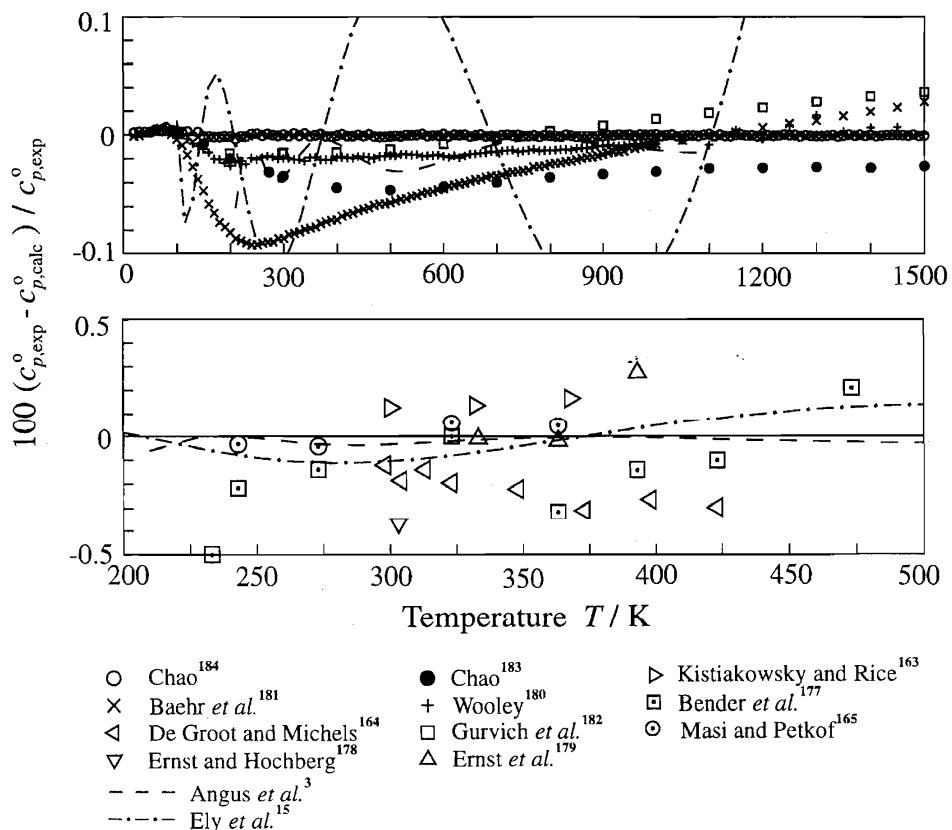


FIG. 16. Relative deviations of c_p^0 data from values calculated from Eq. (6.2). The upper diagram shows data calculated from statistical thermodynamics (see Table 15) and the lower diagram shows data extrapolated from experimental results (see Table 13). Values of c_p^0 calculated from the corresponding equations of Angus *et al.*³ and Ely *et al.*¹⁵ are plotted for comparison.

TABLE 28. The ideal-gas part of the dimensionless Helmholtz function ϕ^o and its derivatives^a

| | | | | | | | | | | |
|-------------------------|---|---------------|---|---------|---|--------------|---|-------------------|---|--|
| ϕ^o | = | $\ln \delta$ | + | a_1^o | + | $a_2^o \tau$ | + | $a_3^o \ln(\tau)$ | + | $\sum_{i=4}^8 a_i^o \ln(1 - e^{-\theta_i^o \tau})$ |
| ϕ_δ^o | = | $1/\delta$ | + | 0 | + | 0 | + | 0 | + | 0 |
| $\phi_{\delta\delta}^o$ | = | $-1/\delta^2$ | + | 0 | + | 0 | + | 0 | + | 0 |
| $\phi_{\delta\tau}^o$ | = | 0 | + | 0 | + | 0 | + | 0 | + | 0 |
| ϕ_τ^o | = | 0 | + | 0 | + | a_2^o | + | a_3^o/τ | + | $\sum_{i=4}^8 a_i^o \theta_i^o [(1 - e^{-\theta_i^o \tau})^{-1} - 1]$ |
| $\phi_{\tau\tau}^o$ | = | 0 | + | 0 | + | 0 | - | a_3^o/τ^2 | - | $\sum_{i=4}^8 a_i^o (\theta_i^o)^2 e^{-\theta_i^o \tau} (1 - e^{-\theta_i^o \tau})^{-2}$ |

^a $\phi_\delta^o = [\partial \phi^o / \partial \delta]_\tau$, $\phi_{\delta\delta}^o = [\partial^2 \phi^o / \partial \delta^2]_\tau$, $\phi_\tau^o = [\partial \phi^o / \partial \tau]_\delta$, $\phi_{\tau\tau}^o = [\partial^2 \phi^o / \partial \tau^2]_\delta$, and $\phi_{\delta\tau}^o = [\partial^2 \phi^o / \partial \delta \partial \tau]$.

region. However, within a region of about +0.1 mK (outside the temperature range shown in Fig. 14) and -10 mK around the critical temperature, Eq. (6.1) yields specific isochoric heat capacities which are significantly larger than the values predicted by the crossover equation of state.

Figure 15 shows a problem which is related to a small oscillation in the derivative $(\partial p / \partial \rho)_T$ close to the critical point. Since the numerical value of this derivative is small close to the critical point, even a very small oscillation in this derivative results in a significant oscillation of properties related to its reciprocal value like the isobaric heat capacity [see Eq. (5.1)] or the isothermal compressibility. Derivatives of these properties [e.g., $(\partial c_p / \partial \rho)_T$] should not be used in the range $440 \text{ kg/m}^3 \leq \rho \leq 500 \text{ kg/m}^3$ and $(T - T_c) \leq 2 \text{ K}$. Oscillations are also observed in the derivative $(\partial c_v / \partial T)_\rho$ for approximately $420 \text{ kg/m}^3 \leq \rho \leq 550 \text{ kg/m}^3$ and $(T - T_c) \leq 15 \text{ K}$.

The quality of Eq. (6.1) should be sufficient for any application which requires numerical values of thermodynamic properties in the critical region. Equation (6.1), however, is not suitable to investigate the asymptotic behavior^c of thermodynamic properties and the derivatives mentioned above should not be used in the regions indicated.

6. The New Equation of State

As discussed in Sec. 2.1 the new equation of state for carbon dioxide is a fundamental equation expressed in form of the Helmholtz energy as

$$A(\rho, T)/(RT) = \phi(\delta, \tau) = \phi^o(\delta, \tau) + \phi^r(\delta, \tau), \quad (6.1)$$

^cThe recent experimental results of Wagner *et al.*²³⁰ for the "thermal" critical exponents β , γ , and δ , derived from $p\rho T$ measurements in the immediate vicinity of the critical point show clear differences from the corresponding values predicted by the renormalization group theory. These surprising results might be caused by an extended validity range of the so-called explicit influence of gravity (the implicit influence of gravity, e.g., the averaging errors based on density stratifications, was taken into account when evaluating the experimental $p\rho T$ data). Thus, we think that the "true" asymptotic behavior at the gas-liquid critical point of a pure fluid is not yet finally clarified.

where $\delta = \rho/\rho_c$ and $\tau = T_c/T$ with $\rho_c = 467.6 \text{ kg/m}^3$ and $T_c = 304.1282 \text{ K}$.

The formulations which describe the ideal-gas part of the Helmholtz energy, Eq. (6.3), and the residual part of the Helmholtz energy, Eq. (6.5), are introduced in this section.

6.1 Ideal-Gas Part of the Helmholtz Energy

According to Eq. (2.4), the ideal-gas part of the Helmholtz energy can be easily obtained if the function $c_p^o(T)$ is known. A correlation equation for $c_p^o(T)$ has been established by means of a nonlinear fitting routine using the 150 c_p^o data of Chao¹⁸⁴ as input values (cf. Sec. 4.2.2). With the coefficients given in Table 27, the obtained equation

TABLE 29. Summary of selected data used for the linear optimization procedure and for the nonlinear fit

| Property | Details of the data set are given in | Number of data | |
|-----------------------------|--------------------------------------|---------------------|---------------|
| | | Linear optimization | Nonlinear fit |
| $p(T, \rho)$ | Table 12 | 2824 | 2824 |
| $c_v(T, \rho)$ | Table 14 | 553 | 553 |
| $c_p(T, \rho)$ | Table 17 | 359 ^a | 359 |
| $c'_p(T)$ | Table 24 | 73 ^a | 73 |
| $w(T, \rho)$ | Table 19 | 422 ^a | 422 |
| $w'(T)$ | Table 24 | 23 ^a | 23 |
| $w''(T)$ | Table 24 | 18 ^a | 18 |
| $\Delta h(T, \rho)$ | Sec. 4.5 | 10 ^a | 10 |
| $\Delta u(T, \rho)$ | Sec. 4.6 | 150 | 150 |
| $\mu(T, \rho)$ | Sec. 4.7 | 34 | |
| $p(T, \rho')$ | | 205 ^b | |
| $p(T, \rho'')$ | | 205 ^b | |
| Maxw.-crit. | | 205 ^b | |
| $p_s(T)$ | Table 7 | 109 | |
| $\rho'(T)$ | Table 8 | 50 | |
| $\rho''(T)$ | Table 9 | 42 | |
| Total number of data points | | 5047 | 4667 |

^aLinearized data used in the optimization procedure; see Setzmann and Wagner.³⁰

^bLinearized solution of the Maxwell criterion when using data calculated from the auxiliary Eqs. (3.13) to (3.15); see Wagner.³²

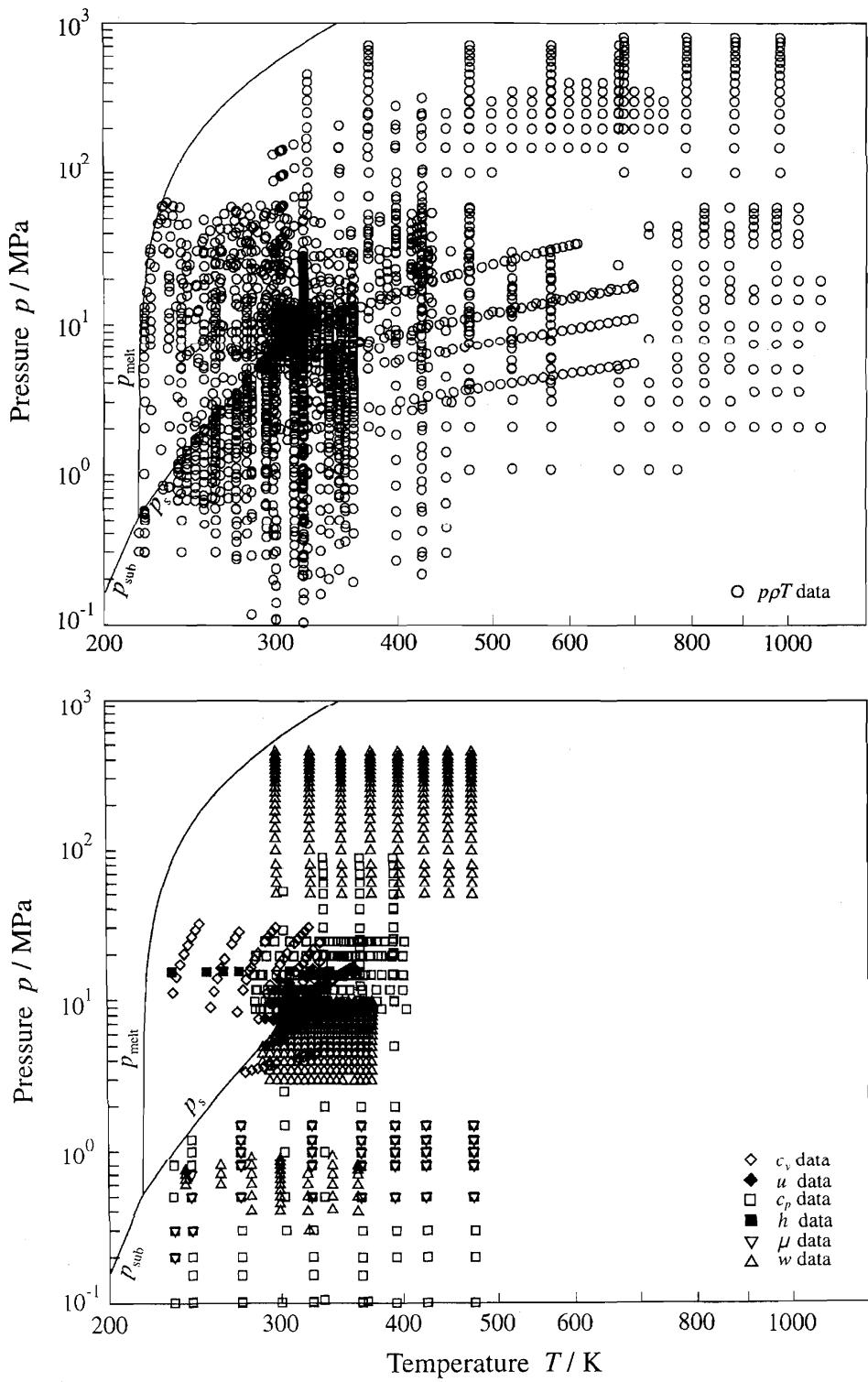


FIG. 17. Distribution of the experimental data used for the establishment of the residual part of the new fundamental equation, Eq. (6.5), in a pT diagram.

$$\frac{c_p^0(T)}{R} = 1 + a_3^0 + \sum_{i=4}^8 a_i^0 (\theta_i^0 \tau)^2 \frac{\exp(\theta_i^0 \tau)}{[\exp(\theta_i^0 \tau) - 1]^2} \quad (6.2)$$

represents Chao's data with deviations less than $\pm 0.005\%$ for $10 \text{ K} \leq T \leq 210 \text{ K}$ and less than $\pm 0.002\%$ for $210 \text{ K} \leq T \leq 1500 \text{ K}$. This means that the uncertainty of Eq. (6.2) is almost equal to the uncertainty of the data which was estimated by Chao to be less than $\pm 0.02\%$. Extrapolation of Eq. (6.2) yields results which are reliable to $\pm 1\%$ for $T \leq 4000 \text{ K}$ and to $\pm 2\%$ for $4000 \text{ K} < T \leq 5000 \text{ K}$. Figure 16 shows deviations between values calculated from the c_p^0 correlations given by Angus *et al.*³ and by Ely *et al.*,¹⁵ data obtained by theoretical approaches and by extrapolation of experimental results, and values calculated from Eq. (6.2), which correspond to the zero line.

The expression for $\phi^0(\delta, \tau)$, which has been derived from Eq. (6.2) by integration, is

$$\begin{aligned} \phi^0(\delta, \tau) = & \ln(\delta) + a_1^0 + a_2^0 \tau + a_3^0 \ln(\tau) \\ & + \sum_{i=4}^8 a_i^0 \ln[1 - \exp(-\tau \theta_i^0)]. \end{aligned} \quad (6.3)$$

The coefficients a_i^0 and θ_i^0 are given in Table 27. The coefficients a_1^0 and a_2^0 were adjusted to give zero for the ideal gas enthalpy at $T_0 = 298.15 \text{ K}$ and the ideal gas entropy at $T_0 = 298.15 \text{ K}$ and $p_0 = 0.101325 \text{ MPa}$. In Table 28, all derivatives of the ideal-gas part ϕ^0 required for the calculation of thermodynamic properties are explicitly given.

6.2 Residual Part of the Helmholtz Energy

The formulation for the residual part of the Helmholtz energy has been developed with the help of the procedure

discussed in Sec. 2.3. The selected data which form the experimental basis of the new equation of state for carbon dioxide have been presented in Sec. 4. Table 29 gives a brief summary of the data used and refers to the corresponding tables, where detailed information is given. Figure 17 shows the distribution of the experimental data used. In addition, data have been calculated from auxiliary equations and from preliminary equations of state in order to guarantee reasonable behavior in regions where the existing measurements yield insufficient information. In detail, these are

- 13 values of the third virial coefficient, which have been calculated from an auxiliary equation (see Sec. 4.8),
- 23 values of the specific isochoric heat capacity, which have been calculated from the crossover equation of Chen *et al.*²⁷ in order to guarantee a reasonable dependence of c_v on density in the critical region,
- 27 $T\rho$ points describing the course of the Joule curve, which have been determined by graphical extrapolation (see Sec. 7.3.2),
- and 70 $p\rho T$ data, which have been calculated from a preliminary equation of state with an exceptionally good extrapolation behavior in order to preserve this progress (see Sec. 7.3.1).

All these "artificial" data are neither considered in Table 29 nor in Fig. 17. The consequences of the absence of caloric data within the liquid region and at temperatures above 500 K are discussed in Sec. 7.2.2.

The bank of terms which was used in the optimization of the final equation of state (see Sec. 2.3.2) contained a total of 860 terms. As far as parameter ranges are predetermined by this general form, these ranges have been established in extensive tests. This bank of terms can be written as

$$\begin{aligned} \phi^r = & \sum_{i=1}^4 \sum_{j=0}^{20} n_{i,j} \delta^i \tau^{j/4} + \sum_{i=1}^6 \sum_{j=0}^{10} n_{i,j} \delta^i \tau^{j/2} e^{-\delta} + \sum_{i=1}^8 \sum_{j=0}^8 n_{i,j} \delta^i \tau^j e^{-\delta^2} + \sum_{i=1}^8 \sum_{j=0}^{16} n_{i,j} \delta^i \tau^j e^{-\delta^3} + \sum_{i=1}^{10} \sum_{j=0}^{12} n_{i,j} \delta^i \tau^{2j} e^{-\delta^4} \\ & + \sum_{i=1}^{10} \sum_{j=5}^{16} n_{i,j} \delta^i \tau^{2j} e^{-\delta^5} + \sum_{i=8}^{15} \sum_{j=5}^{16} n_{i,j} \delta^i \tau^{2j} e^{-\delta^6} + \sum_{i=1}^{48} n_i \delta^{d_i} \tau^i e^{-\alpha_i(\delta - \epsilon_i)^2 - \beta_i(\tau - \gamma_i)^2} \\ & + \sum_{i=1}^3 \sum_{j=1}^2 \sum_{k=1}^2 \sum_{l=1}^3 \sum_{m=1}^3 n_{i,j,k,l} \Delta^{b_j} \delta^{C_l} e^{-C_l(\delta - 1)^2 - D_m(\tau - 1)^2} \end{aligned} \quad (6.4)$$

with $\Delta = \{(1 - \tau) + A[(\delta - 1)^2]\}^{1/(2\beta)}$ and $B_k[(\delta - 1)^2]^{a_i}$.

TABLE 30. Parameters of the nonanalytic terms in the bank of terms

| i, j, k, l, m | a_i | b_j | B_k | C_l | D_m | A^a | β^a |
|-----------------|-------|-------|-------|-------|-------|-------|-----------|
| 1 | 3.00 | 0.875 | 0.30 | 10.00 | 225.0 | 0.700 | 0.300 |
| 2 | 3.50 | 0.925 | 1.00 | 12.50 | 250.0 | | |
| 3 | 4.00 | | | 15.00 | 275.0 | | |

^aPredetermined from a simultaneous fit to saturated liquid and vapor densities in the critical region.

The parameters of the modified Gaussian terms originally introduced by Setzmann and Wagner³⁰ have been slightly changed for carbon dioxide; 48 of these expressions were used in the bank of terms covering the following parameter ranges: $1 \leq d_i \leq 3$, $0 \leq t_i \leq 3$, $15 \leq \alpha_i \leq 25$, $275 \leq \beta_i \leq 325$, and $1.16 \leq \gamma_i \leq 1.25$ with $\epsilon_i = 1$. The values which have been used for the parameters of the 108 nonanalytic terms in Eq. (6.1) are given in Table 30. The values used for b_j , C_l , and D_m resulted from a nonlinear fit of a preliminary formulation.

Proceeding from the bank of terms defined by Eq. (6.4),

TABLE 31. Coefficients and exponents of Eq. (6.5)^a

| <i>i</i> | <i>n_i</i> | <i>d_i</i> | <i>t_i</i> | | | | | |
|----------|--|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|
| 1 | 0.388 568 232 031 61×10 ⁰ | 1 | 0.00 | | | | | |
| 2 | 0.293 854 759 427 40×10 ¹ | 1 | 0.75 | | | | | |
| 3 | -0.558 671 885 349 34×10 ¹ | 1 | 1.00 | | | | | |
| 4 | -0.767 531 995 924 77×10 ⁰ | 1 | 2.00 | | | | | |
| 5 | 0.317 290 055 804 16×10 ⁰ | 2 | 0.75 | | | | | |
| 6 | 0.548 033 158 977 67×10 ⁰ | 2 | 2.00 | | | | | |
| 7 | 0.122 794 112 203 35×10 ⁰ | 3 | 0.75 | | | | | |
| <i>i</i> | <i>n_i</i> | <i>d_i</i> | <i>t_i</i> | <i>c_i</i> | | | | |
| 8 | 0.216 589 615 432 20×10 ¹ | 1 | 1.50 | 1 | | | | |
| 9 | 0.158 417 351 097 24×10 ¹ | 2 | 1.50 | 1 | | | | |
| 10 | -0.231 327 054 055 03×10 ⁰ | 4 | 2.50 | 1 | | | | |
| 11 | 0.581 169 164 314 36×10 ⁻¹ | 5 | 0.00 | 1 | | | | |
| 12 | -0.553 691 372 053 82×10 ⁰ | 5 | 1.50 | 1 | | | | |
| 13 | 0.489 466 159 094 22×10 ⁰ | 5 | 2.00 | 1 | | | | |
| 14 | -0.242 757 398 435 01×10 ⁻¹ | 6 | 0.00 | 1 | | | | |
| 15 | 0.624 947 905 016 78×10 ⁻¹ | 6 | 1.00 | 1 | | | | |
| 16 | -0.121 738 602 252 46×10 ⁰ | 6 | 2.00 | 1 | | | | |
| 17 | -0.370 556 852 700 86×10 ⁰ | 1 | 3.00 | 2 | | | | |
| 18 | -0.167 758 797 004 26×10 ⁻¹ | 1 | 6.00 | 2 | | | | |
| 19 | -0.119 607 366 379 87×10 ⁰ | 4 | 3.00 | 2 | | | | |
| 20 | -0.456 193 625 087 78×10 ⁻¹ | 4 | 6.00 | 2 | | | | |
| 21 | 0.356 127 892 703 46×10 ⁻¹ | 4 | 8.00 | 2 | | | | |
| 22 | -0.744 277 271 320 52×10 ⁻² | 7 | 6.00 | 2 | | | | |
| 23 | -0.173 957 049 024 32×10 ⁻² | 8 | 0.00 | 2 | | | | |
| 24 | -0.218 101 212 895 27×10 ⁻¹ | 2 | 7.00 | 3 | | | | |
| 25 | 0.243 321 665 592 36×10 ⁻¹ | 3 | 12.00 | 3 | | | | |
| 26 | -0.374 401 334 234 63×10 ⁻¹ | 3 | 16.00 | 3 | | | | |
| 27 | 0.143 387 157 568 78×10 ⁰ | 5 | 22.00 | 4 | | | | |
| 28 | -0.134 919 690 832 86×10 ⁰ | 5 | 24.00 | 4 | | | | |
| 29 | -0.231 512 250 534 80×10 ⁻¹ | 6 | 16.00 | 4 | | | | |
| 30 | 0.123 631 254 929 01×10 ⁻¹ | 7 | 24.00 | 4 | | | | |
| 31 | 0.210 583 219 729 40×10 ⁻² | 8 | 8.00 | 4 | | | | |
| 32 | -0.339 585 190 263 68×10 ⁻³ | 10 | 2.00 | 4 | | | | |
| 33 | 0.559 936 517 715 92×10 ⁻² | 4 | 28.00 | 5 | | | | |
| 34 | -0.303 351 180 556 46×10 ⁻³ | 8 | 14.00 | 6 | | | | |
| <i>i</i> | <i>n_i</i> | <i>d_i</i> | <i>t_i</i> | <i>α_i</i> | | | | |
| 35 | -0.213 654 886 883 20×10 ³ | 2 | 1.00 | 25 | | | | |
| 36 | 0.266 415 691 492 72×10 ⁵ | 2 | 0.00 | 25 | | | | |
| 37 | -0.240 272 122 045 57×10 ⁵ | 2 | 1.00 | 25 | | | | |
| 38 | -0.283 416 034 239 99×10 ³ | 3 | 3.00 | 15 | | | | |
| 39 | 0.212 472 844 001 79×10 ³ | 3 | 3.00 | 20 | | | | |
| <i>i</i> | <i>n_i</i> | <i>a_i</i> | <i>b_i</i> | <i>β_i</i> | | | | |
| 40 | -0.666 422 765 407 51×10 ⁰ | 3.500 | 0.875 | 0.300 | | | | |
| 41 | 0.726 086 323 498 97×10 ⁰ | 3.500 | 0.925 | 0.300 | | | | |
| 42 | 0.550 686 686 128 42×10 ⁻¹ | 3.000 | 0.875 | 0.300 | | | | |
| <i>i</i> | <i>n_i</i> | <i>a_i</i> | <i>b_i</i> | <i>β_i</i> | <i>A_i</i> | <i>B_i</i> | <i>C_i</i> | <i>D_i</i> |

^aR = 0.188 924 1 kJ/(kg K); T_c = 304.128 2 K; ρ_c = 467.6 kg/m³.

the modified optimization method (see Sec. 2.3.2) was used to determine the combination of terms which yields the best representation of the linearized data set. The resulting formulation for the residual part of the Helmholtz energy is

$$\phi^r = \sum_{i=1}^7 n_i \delta^{d_i} \tau^i + \sum_{i=8}^{34} n_i \delta^{d_i} \tau^i e^{-\delta^i}$$

$$+ \sum_{i=35}^{39} n_i \delta^{d_i} \tau^i e^{-\alpha_i(\delta - \epsilon_i)^2 - \beta_i(\tau - \gamma_i)^2}$$

$$+ \sum_{i=40}^{42} n_i \Delta^{b_i} \delta e^{-C_i(\delta - 1)^2 - D_i(\tau - 1)^2} \quad (6.5)$$

with $\Delta = \{(1 - \tau) + A_i[(\delta - 1)^2]^{1/(2\beta_i)}\}^2 + B_i[(\delta - 1)^2]^{\alpha_i}$.

After this linear optimization process, the final values of the coefficients *n_i* of Eq. (6.5) have been determined by a direct nonlinear fit to the linear and nonlinear data. These values are given in Table 31 together with the parameters resulting from the optimization process. No further improve-

TABLE 32. The residual part of the dimensionless Helmholtz energy ϕ^r and its derivatives^a

| | | |
|---|--|--|
| $\phi^r = \sum_{i=1}^7 n_i \delta^{d_i} \tau^{t_i} + \sum_{i=8}^{34} n_i \delta^{d_i} \tau^{t_i} e^{-\delta^{c_i}} + \sum_{i=35}^{39} n_i \delta^{d_i} \tau^{t_i} e^{-\alpha_i(\delta-\epsilon_i)^2 - \beta_i(\tau-\gamma_i)^2} + \sum_{i=40}^{42} n_i \Delta^{b_i} \delta \Psi \quad \text{with } \Delta = \theta^2 + B_i[(\delta-1)^2]^{a_i}$ $\theta = (1-\tau) + A_{iL}[(\delta-1)^2]^{1/(2\beta_i)}$ $\Psi = e^{-C_i(\delta-1)^2 - D_i(\tau-1)^2}$ $\phi_\delta^r = \sum_{i=1}^7 n_i d_i \delta^{d_i-1} \tau^{t_i} + \sum_{i=8}^{34} n_i e^{-\delta^{c_i}} [\delta^{d_i-1} \tau^{t_i} (d_i - c_i \delta^{c_i})] + \sum_{i=35}^{39} n_i \delta^{d_i} \tau^{t_i} e^{-\alpha_i(\delta-\epsilon_i)^2 - \beta_i(\tau-\gamma_i)^2} \left[\frac{d_i}{\delta} - 2\alpha_i(\delta-\epsilon_i) \right] + \sum_{i=40}^{42} n_i \left[\Delta^{b_i} \left(\Psi + \delta \frac{\partial \Psi}{\partial \delta} \right) + \frac{\partial \Delta^{b_i}}{\partial \delta} \delta \Psi \right]$ $\phi_{\delta\delta}^r = \sum_{i=1}^7 n_i d_i (d_i - 1) \delta^{d_i-2} \tau^{t_i} + \sum_{i=8}^{34} n_i e^{-\delta^{c_i}} [\delta^{d_i-2} \tau^{t_i} ((d_i - c_i \delta^{c_i}) (d_i - 1 - c_i \delta^{c_i}) - c_i^2 \delta^{c_i})] + \sum_{i=35}^{39} n_i \tau^{t_i} e^{-\alpha_i(\delta-\epsilon_i)^2 - \beta_i(\tau-\gamma_i)^2}$ $\cdot [-2\alpha_i \delta^{d_i} + 4\alpha_i^2 \delta^{d_i} (\delta-\epsilon_i)^2 - 4d_i \alpha_i \delta^{d_i-1} (\delta-\epsilon_i) + d_i (d_i - 1) \delta^{d_i-2}] + \sum_{i=40}^{42} n_i \left[\Delta^{b_i} \left(2 \frac{\partial \Psi}{\partial \delta} + \delta \frac{\partial^2 \Psi}{\partial \delta^2} \right) + 2 \frac{\partial \Delta^{b_i}}{\partial \delta} \left(\Psi + \delta \frac{\partial \Psi}{\partial \delta} \right) + \frac{\partial^2 \Delta^{b_i}}{\partial \delta^2} \delta \Psi \right]$ $\phi_\tau^r = \sum_{i=1}^7 n_i t_i \delta^{d_i} \tau^{t_i-1} + \sum_{i=8}^{34} n_i t_i \delta^{d_i} \tau^{t_i-1} e^{-\delta^{c_i}} + \sum_{i=35}^{39} n_i \delta^{d_i} \tau^{t_i} e^{-\alpha_i(\delta-\epsilon_i)^2 - \beta_i(\tau-\gamma_i)^2} \left[\frac{t_i}{\tau} - 2\beta_i(\tau-\gamma_i) \right] + \sum_{i=40}^{42} n_i \delta \left[\frac{\partial \Delta^{b_i}}{\partial \tau} \Psi + \Delta^{b_i} \frac{\partial \Psi}{\partial \tau} \right]$ $\phi_{\tau\tau}^r = \sum_{i=1}^7 n_i t_i (t_i - 1) \delta^{d_i} \tau^{t_i-2} + \sum_{i=8}^{34} n_i t_i (t_i - 1) \delta^{d_i} \tau^{t_i-2} e^{-\delta^{c_i}} + \sum_{i=35}^{39} n_i \delta^{d_i} \tau^{t_i} e^{-\alpha_i(\delta-\epsilon_i)^2 - \beta_i(\tau-\gamma_i)^2} \left[\left(\frac{t_i}{\tau} - 2\beta_i(\tau-\gamma_i) \right)^2 - \frac{t_i}{\tau^2} - 2\beta_i \right]$ $+ \sum_{i=40}^{42} n_i \left[\frac{\partial^2 \Delta^{b_i}}{\partial \tau^2} \Psi + 2 \frac{\partial \Delta^{b_i}}{\partial \tau} \frac{\partial \Psi}{\partial \tau} + \Delta^{b_i} \frac{\partial^2 \Psi}{\partial \tau^2} \right]$ $\phi_{\delta\tau}^r = \sum_{i=1}^7 n_i d_i t_i \delta^{d_i-1} \tau^{t_i-1} + \sum_{i=8}^{34} n_i e^{-\delta^{c_i}} \delta^{d_i-1} t_i \tau^{t_i-1} (d_i - c_i \delta^{c_i}) + \sum_{i=35}^{39} n_i \delta^{d_i} \tau^{t_i} e^{-\alpha_i(\delta-\epsilon_i)^2 - \beta_i(\tau-\gamma_i)^2} \left[\frac{d_i}{\delta} - 2\alpha_i(\delta-\epsilon_i) \right] \left[\frac{t_i}{\tau} - 2\beta_i(\tau-\gamma_i) \right]$ $+ \sum_{i=40}^{42} n_i \left[\Delta^{b_i} \left(\frac{\partial \Psi}{\partial \tau} + \delta \frac{\partial^2 \Psi}{\partial \delta \partial \tau} \right) + \delta \frac{\partial \Delta^{b_i}}{\partial \delta} \frac{\partial \Psi}{\partial \tau} + \frac{\partial \Delta^{b_i}}{\partial \tau} \left(\Psi + \delta \frac{\partial \Psi}{\partial \delta} \right) + \frac{\partial^2 \Delta^{b_i}}{\partial \delta \partial \tau} \delta \Psi \right]$ | Derivatives of the distance function Δ^{b_i} : $\frac{\partial \Delta^{b_i}}{\partial \delta} = b_i \Delta^{b_i-1} \frac{\partial \Delta}{\partial \delta}$ $\frac{\partial^2 \Delta^{b_i}}{\partial \delta^2} = b_i \left[\Delta^{b_i-1} \frac{\partial^2 \Delta}{\partial \delta^2} + (b_i - 1) \Delta^{b_i-2} \left(\frac{\partial \Delta}{\partial \delta} \right)^2 \right]$ $\frac{\partial \Delta^{b_i}}{\partial \tau} = -2\theta b_i \Delta^{b_i-1}$ $\frac{\partial^2 \Delta^{b_i}}{\partial \tau^2} = 2b_i \Delta^{b_i-1} + 4\theta^2 b_i (b_i - 1) \Delta^{b_i-2}$ $\frac{\partial^2 \Delta^{b_i}}{\partial \delta \partial \tau} = -A_i b_i \frac{2}{\beta_i} \Delta^{b_i-1} (\delta-1) [(\delta-1)^2]^{1/(2\beta_i)-1} - 2\theta b_i (b_i - 1) \Delta^{b_i-2} \frac{\partial \Delta}{\partial \delta}$ $\frac{\partial \Delta}{\partial \delta} = (\delta-1) \left[A_i \theta \frac{2}{\beta_i} [(\delta-1)^2]^{1/(2\beta_i)-1} + 2B_i a_i [(\delta-1)^2]^{a_i-1} \right]$ $\frac{\partial^2 \Delta}{\partial \delta^2} = \frac{1}{(\delta-1)} \frac{\partial \Delta}{\partial \delta} + (\delta-1)^2 \left[4B_i a_i (a_i - 1) [(\delta-1)^2]^{a_i-2} + 2A_i^2 \left(\frac{1}{\beta_i} \right)^2 [(\delta-1)^2]^{1/(2\beta_i)-1} \right]^2 + A_i \theta \frac{4}{\beta_i} \left(\frac{1}{2\beta_i} - 1 \right) [(\delta-1)^2]^{1/(2\beta_i)-2}$ | Derivatives of the exponential function Ψ : $\frac{\partial \Psi}{\partial \delta} = -2C_i(\delta-1)\Psi$ $\frac{\partial^2 \Psi}{\partial \delta^2} = [2C_i(\delta-1)^2 - 1]2C_i\Psi$ $\frac{\partial \Psi}{\partial \tau} = -2D_i(\tau-1)\Psi$ $\frac{\partial^2 \Psi}{\partial \tau^2} = [2D_i(\tau-1)^2 - 1]2D_i\Psi$ $\frac{\partial^2 \Psi}{\partial \delta \partial \tau} = 4C_i D_i (\delta-1)(\tau-1)\Psi$ |
| $\phi_\delta^r = \left(\frac{\partial \phi^r}{\partial \delta} \right)_\tau, \quad \phi_{\delta\delta}^r = \left(\frac{\partial^2 \phi^r}{\partial \delta^2} \right)_\tau, \quad \phi_\tau^r = \left(\frac{\partial \phi^r}{\partial \tau} \right)_\delta, \quad \phi_{\tau\tau}^r = \left(\frac{\partial^2 \phi^r}{\partial \tau^2} \right)_\delta, \quad \text{and} \quad \phi_{\delta\tau}^r = \left(\frac{\partial^2 \phi^r}{\partial \delta \partial \tau} \right)_\delta.$ | | |

ment was achieved by refitting the b_i , C_i , and D_i of the nonanalytic terms.

The new fundamental equation for carbon dioxide, Eq. (6.1), in combination with the formulations according to Eqs. (6.3) and (6.5), is constrained to the critical parameters given in Sec. 3.2. It is valid for the entire fluid region covered by reliable data, namely for

216 K $\leq T \leq$ 1100 K and 0 MPa $\leq p \leq$ 800 MPa.

Estimations for the uncertainty of Eq. (6.1) are given in Sec. 8; the quality of the new equation of state is discussed in Sec. 7. The necessary derivatives of Eq. (6.5) are given in Table 32.

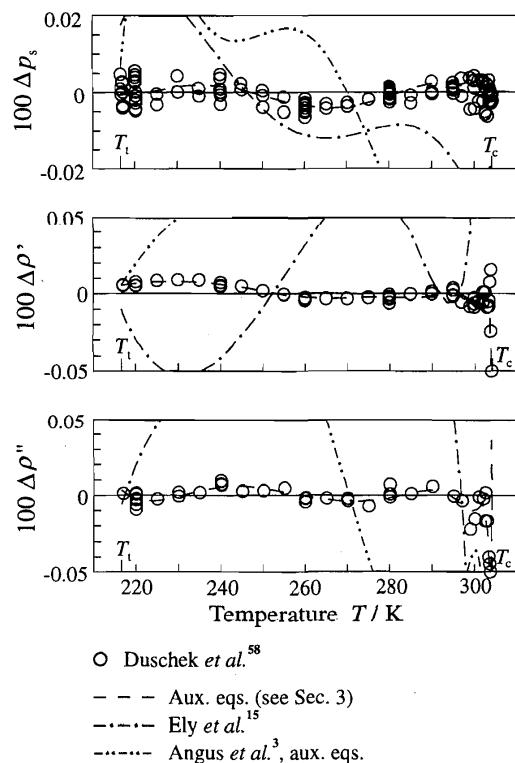


FIG. 18. Relative deviations $100\Delta y = 100(y_{\text{exp}} - y_{\text{calc}})/y_{\text{exp}}$ of the experimental saturation data of Duschek *et al.*⁵⁸ from values calculated from Eq. (6.1). Values calculated from auxiliary equations presented in Sec. 3, the equation of state of Ely *et al.*¹⁵ and the auxiliary equations of Angus *et al.*³ are plotted for comparison.

7. Comparisons of the New Equation of State with Experimental Data and Other Equations of State

In this section, the quality of the new equation of state is discussed based on comparisons with selected experimental data. In addition, most figures also show values calculated from the equation of state published by Angus *et al.*,³ which is commonly accepted as an international standard for carbon dioxide, and by Ely *et al.*,¹⁵ which proved to be the best of the available equations of state for carbon dioxide.

For the extended critical region, comparisons should be performed with the complete IUPAC equation (Angus *et al.*)³ which consists of an analytic wide-range equation, a switching function, and a scaled equation for the description of the critical region (see Sec. 1.2). Since the evaluation of the combined equation causes numerical problems,^d we decided to use the equation of Pitzer and Schreiber¹⁶ for com-

^dThe data published in the IUPAC tables use temperatures according to the IPTS-68 temperature scale, but regarding the equations there seems to be some inconsistency in the temperature scales used. In the critical region, the published isochoric heat capacity data are partly determined graphically, since the evaluation of the combined equation yields unreasonable results.

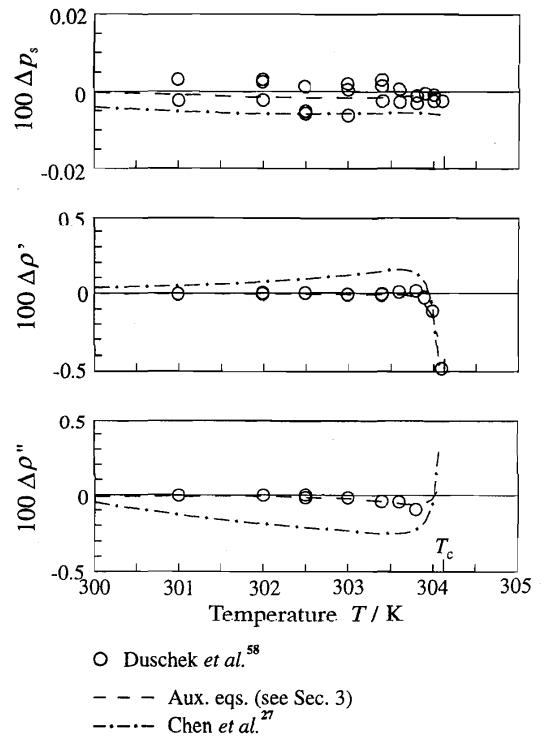


FIG. 19. Relative deviations $100\Delta y = 100(y_{\text{exp}} - y_{\text{calc}})/y_{\text{exp}}$ ($y = p_s, \rho', \rho''$) of the near critical experimental saturation data of Duschek *et al.*⁵⁸ from values calculated from Eq. (6.1). Values calculated from the auxiliary equations presented in Sec. 3 and from the crossover of Chen *et al.*²⁷ are plotted for comparison.

parisons in the extended critical region. This formulation yields very similar results to the IUPAC equation but at clearly less numerical expense. All the figures presenting data in this region also contain values calculated from the crossover equation of Chen *et al.*²⁷ which is the most sophisticated scaled equation of state published for carbon dioxide. The representation of the specific isochoric heat capacity and the speed of sound in the critical region was discussed in detail in Sec. 5.

None of the existing equations of state for carbon dioxide is valid on the ITS-90 temperature scale. Therefore, temperatures were reconverted to the IPTS-68 scale by using the procedure of Preston-Thomas *et al.*,³⁷ before values were calculated from these equations.

7.1 Liquid-Vapor Boundary

7.1.1 Thermal Properties on the Coexistence Curve

As shown in Sec. 3, the discussion of thermal properties on the liquid-vapor boundary can be restricted to the representation of the data of Duschek *et al.*⁵⁸ The deviations between these data and values calculated from Eq. (6.1) by using the phase equilibrium condition [see Eq. (2.2)] is shown in Fig. 18. The additional lines in this deviation plot correspond to values calculated from the auxiliary equations

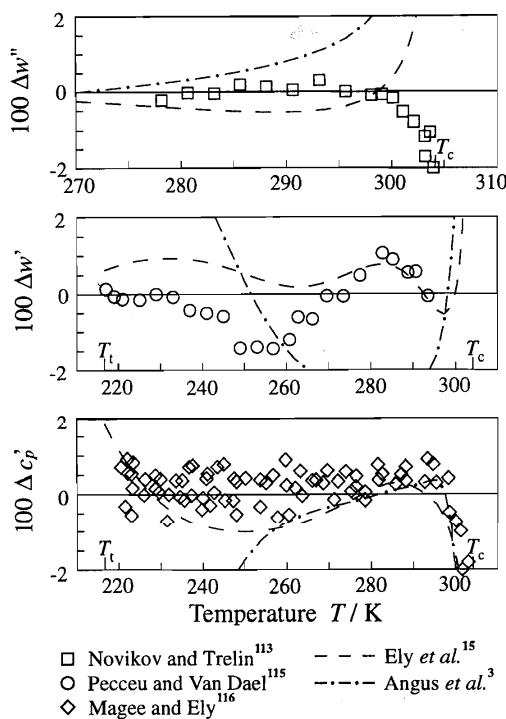


FIG. 20. Relative deviations $100\Delta y = 100(y_{\text{exp}} - y_{\text{calc}})/y_{\text{exp}}$ ($y = w'', w', c'$) of experimental caloric data at saturation from values calculated from Eq. (6.1). Data calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

presented in this work (see Sec. 3), to values calculated from the equation of state of Ely *et al.*¹⁵ by using the phase equilibrium condition and to values calculated from auxiliary equations for the saturation properties established by Angus *et al.*³. Angus *et al.* recommend the use of their auxiliary equations for phase equilibrium calculations since they yield better results than the IUPAC equation of state.

Figure 18 shows that Eq. (6.1) represents the very accurate vapor pressure data of Duscheck *et al.*⁵⁸ to within $\pm 0.006\%$ in pressure. Saturated liquid and vapor densities are represented to within $\pm 0.01\%$ in density up to 303.6 K and 297.0 K, respectively. Approaching the critical point the deviations in density increase, but these deviations are still within the experimental uncertainty of the data; thus, all the data are represented to within their experimental uncertainty. None of the equations hitherto known is able to reproduce the data at least roughly within their uncertainty (the uncertainty values are given in Tables 7–9).

Figure 19 shows the representation of the saturation properties in the critical region where a larger deviation scale is used. The very good representation of the vapor pressure data is practically not affected when approaching the critical temperature and the density deviations increase only slightly, except for the last point measured for the saturated liquid density. Duscheck *et al.*⁵⁸ do not give any estimation for the uncertainty of this point, but only 36 mK below the critical

temperature a deviation of 0.48% in the saturated liquid density can be considered to be within the experimental uncertainty.

The crossover equation of Chen *et al.*²⁷ is able to reproduce the vapor pressure data within their experimental uncertainty but it cannot represent the saturated vapor and liquid densities within the uncertainty of these state-of-the-art measurements. The auxiliary equations presented in Sec. 3 reproduce the experimental data slightly better than Eq. (6.1) does. If one is interested in thermodynamically consistent values for all properties on the phase boundary, the evaluation of Eq. (6.1) in combination with Eq. (2.2) should be used and not the simpler auxiliary equations given in Sec. 3.

7.1.2 Caloric Properties on the Coexistence Curve

Figure 20 shows the representation of group 1 data providing information on the caloric behavior on the phase boundary. The speed of sound data of the saturated vapor state measured by Novikov and Trelin¹¹³ are reproduced within $\pm 0.5\%$ for $T < 301$ K and to $\pm 3\%$ for $T > 301$ K. Only the last point 30 mK below the critical temperature exceeds this limit, but since the temperature scale of Novikov and Trelin is uncertain by more than 30 mK (see Sec. 4.10), we did not rely on this data point. The analytic equations of state of Angus *et al.*³ and Ely *et al.*¹⁵ are not able to follow the decreasing speed of sound when approaching the critical point.

Equation (6.1) represents both the speed of sound and the specific isobaric heat capacity in the saturated liquid state to within $\pm 1\%$; the greater deviations of the w' data of Pecceu and Van Dael¹¹⁵ at temperatures between 249 K and 261 K are due to a systematic offset in the data set. The equation of Ely *et al.*¹⁵ yields results which are at least similar to those calculated from Eq. (6.1), but the formulation of Angus *et al.*³ fails in describing caloric properties in the saturated liquid state (see also the representation of c_v in the homogeneous liquid region, Sec. 7.2.2 and Fig. 31).

The new equation of state was fitted to the c'_p data of Magee and Ely¹¹⁶ up to temperatures of 295 K since the conversion of c_σ to c'_p seems to be uncertain for higher temperatures (see Sec. 3.8). Above 295 K the deviations between the converted data and the new fundamental equation remain within about $\pm 2\%$; keeping in mind that c'_p is strongly diverging when approaching the critical point, this result underlines the consistent description of the critical region by Eq.(6.1).

7.2 Single-Phase Region

7.2.1 Thermal Properties in the Single-Phase Region

For carbon dioxide, the region where $p\rho T$ data in reference quality are available extends up to pressures of 13 MPa at temperatures up to 360 K. Within this region, the data sets of Duscheck *et al.*,^{58,154} Gilgen *et al.*,¹⁵⁹ Nowak *et al.*,^{160d} and Guo *et al.*¹⁵⁷ describe the $p\rho T$ surface with an uncertainty of approximately $\pm 0.02\%$ in density and in the extended criti-

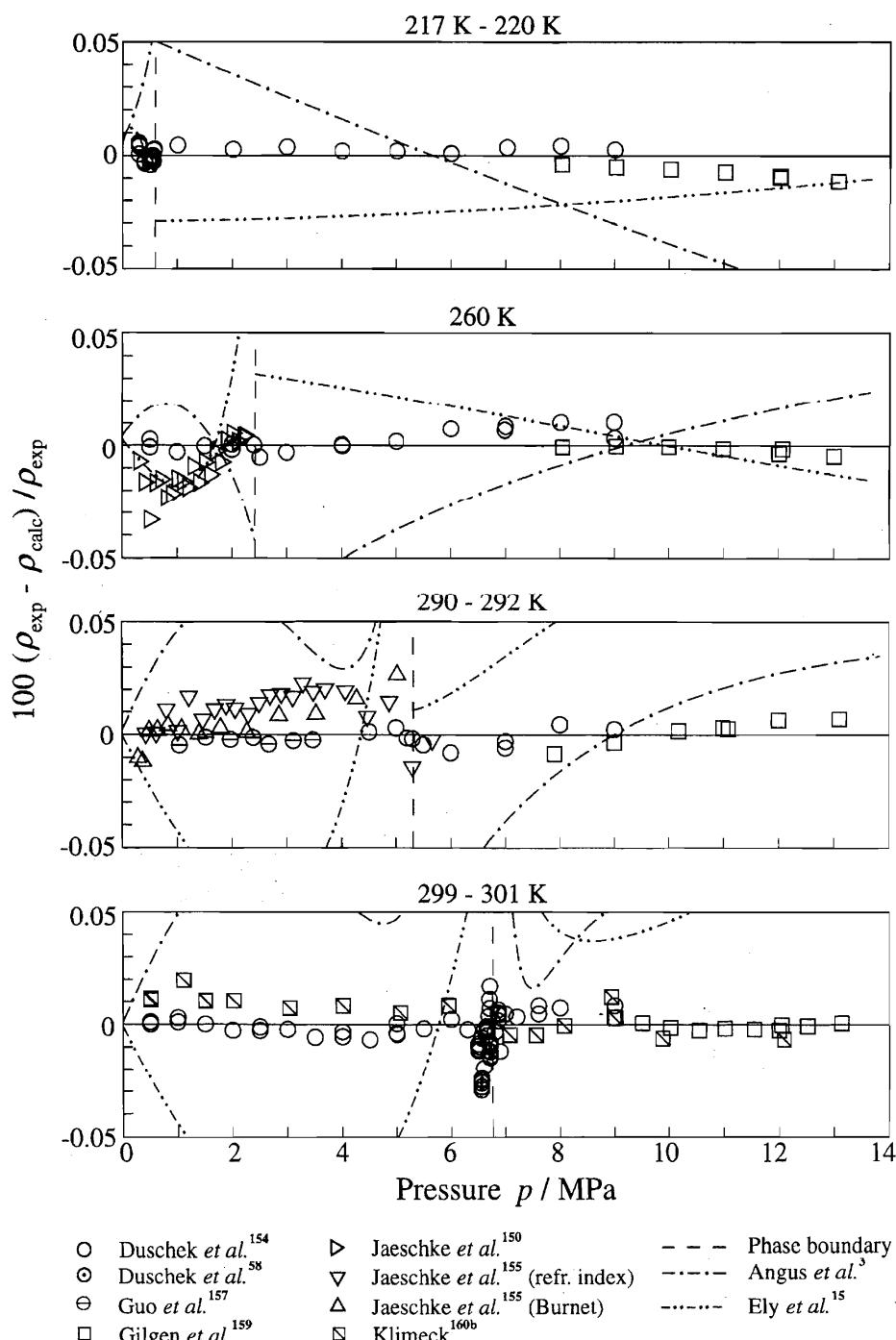


FIG. 21. Relative density deviations of very accurate $p\rho T$ data at subcritical temperatures from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

cal region of $\pm 0.02\%$ in pressure. In an extended region reaching up to pressures of 30 MPa and temperatures of 523 K, the data of Brachthäuser¹⁶⁰ and Klimeck *et al.*^{160b} describe the $p\rho T$ surface with an uncertainty of $\pm 0.02\%$ to

$\pm 0.05\%$ in density. None of the existing equations of state had access to these data sets because the data have been published since 1990. Equation (6.1) is able to reproduce these data within their experimental uncertainty (for the nu-

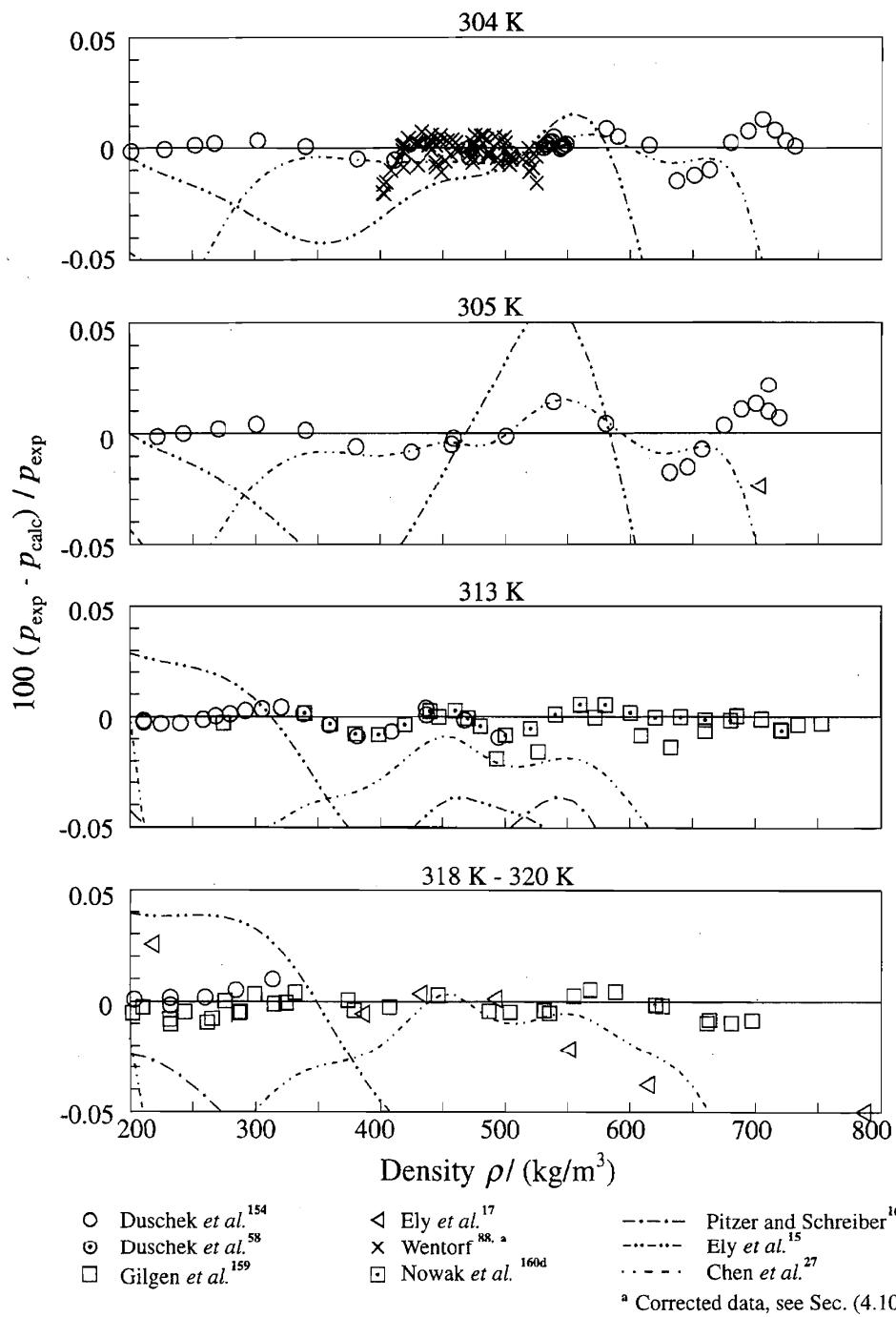


FIG. 22. Relative pressure deviations of very accurate $p\rho T$ data in the extended critical region from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Pitzer and Schreiber¹⁶ and from the crossover equation of Chen *et al.*²⁷ are plotted for comparison.

numerical values of the uncertainty see Table 12). Figures 21 to 23 show the representation of some reference data on typical isotherms in order to illustrate this statement.

Figure 21 additionally contains data of Jaeschke^{150,155} which also give a high-quality description of the $p\rho T$ surface

in the gas and supercritical region. The equation of Ely *et al.*¹⁵ yields a suitable description of the gas region at low temperatures but it has problems for temperatures above about 250 K. The equation of Angus *et al.*³ is not able to reproduce the state-of-the-art data in the gas region. In the

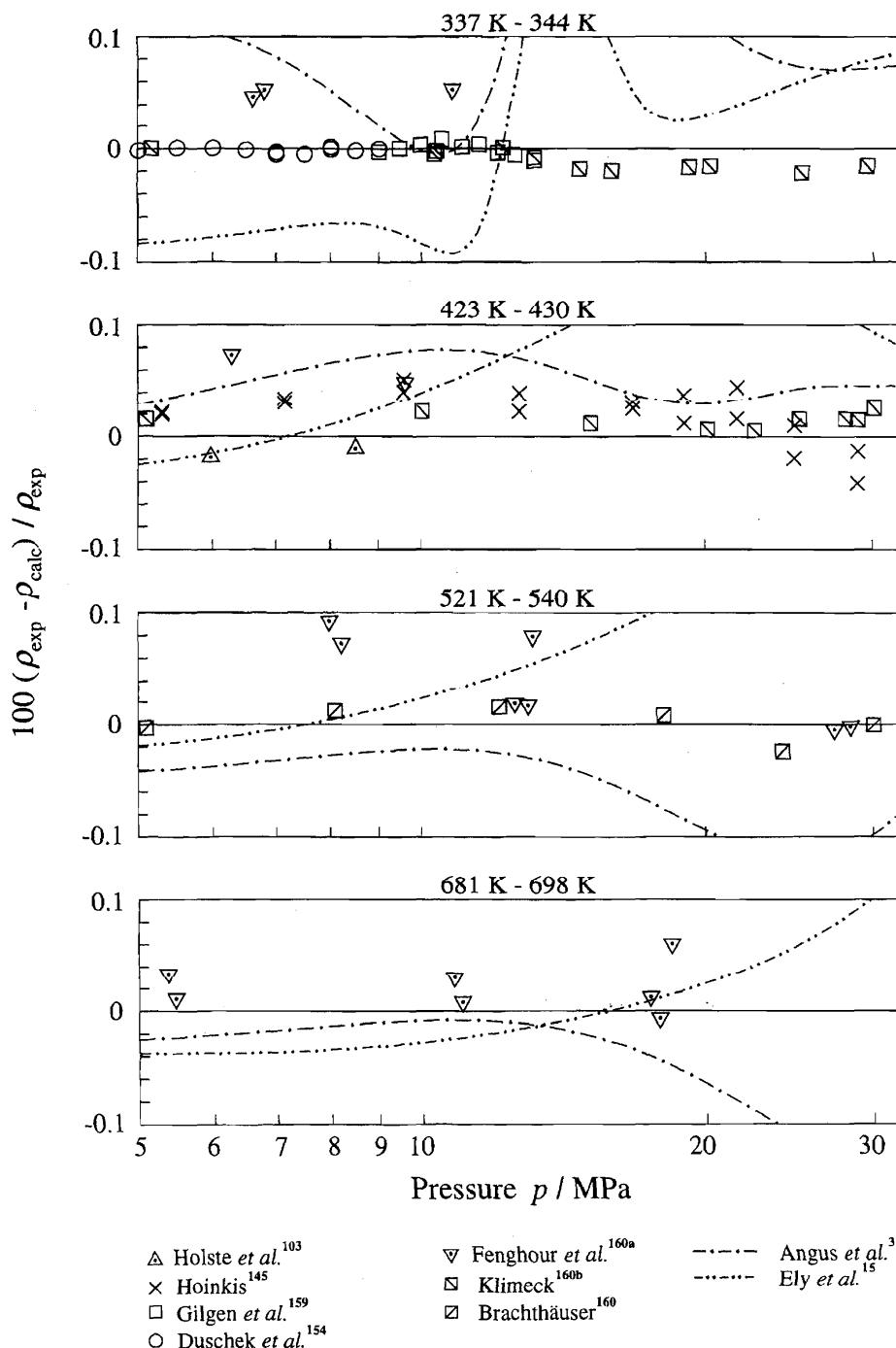


FIG. 23. Relative density deviations of very accurate $p\rho T$ data at supercritical temperatures from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

liquid region, none of the existing equations of state is able to represent the reference data of Duscheck *et al.*¹⁵⁴ and Gilgen *et al.*¹⁵⁹ at least roughly to within their experimental uncertainty.

High-quality $p\rho T$ data in the extended critical region are shown in Fig. 22. The data of Duscheck *et al.*^{58,154} and Gilgen *et al.*¹⁵⁹ are supplemented by the selected data of Wentorf⁸⁸ and by the data of Ely *et al.*¹⁷ which are consistent with the

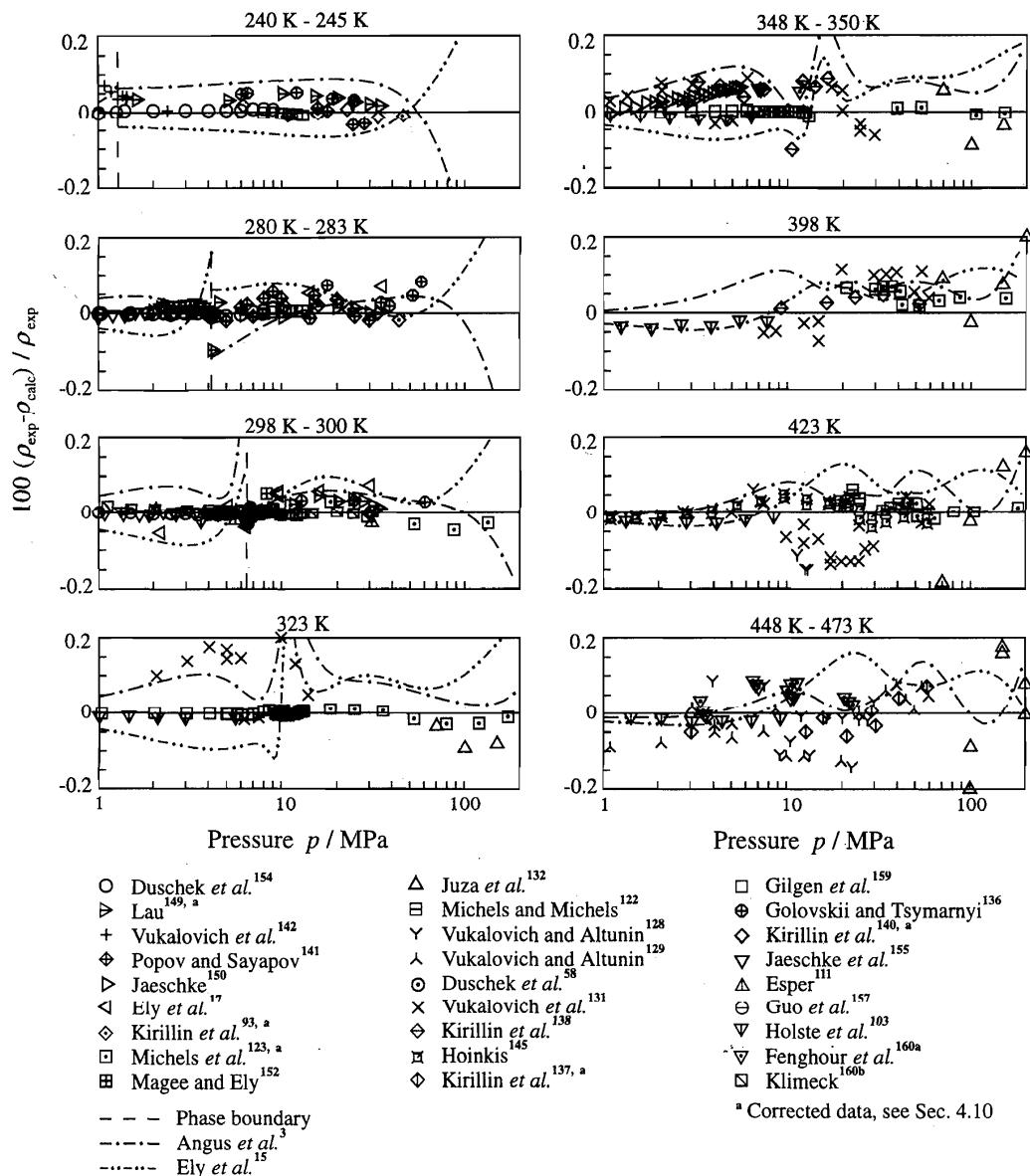


FIG. 24. Relative density deviations of selected $p\rho T$ data from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

reference data by approximately $\pm 0.03\%$ in pressure. Even in this region, Eq. (6.1) represents the reference data to within their experimental uncertainty. The deviations between the data and values calculated from the equation of Ely *et al.*¹⁵ increase up to 0.1% in pressure, which corresponds to five times the uncertainty of the data, while the equation of Pitzer and Schreiber¹⁶ deviates by up to 0.2% . The equation of Chen *et al.*,²⁷ which is especially designed for the description of this region, yields a very suitable rep-

resentation of the $p\rho T$ data in the surrounding of the critical isochore. However, at lower and higher densities, but clearly within the range of its validity, the crossover equation does not reproduce the reference data within their experimental uncertainty.

Figure 23 shows the representation of high-quality data at higher temperatures and pressures. Up to 523 K and 30 MPa, the $p\rho T$ surface is defined by the data of Brachthäuser¹⁶⁰ and Klimeck *et al.*^{160b} with an uncertainty of less than $\pm 0.05\%$.

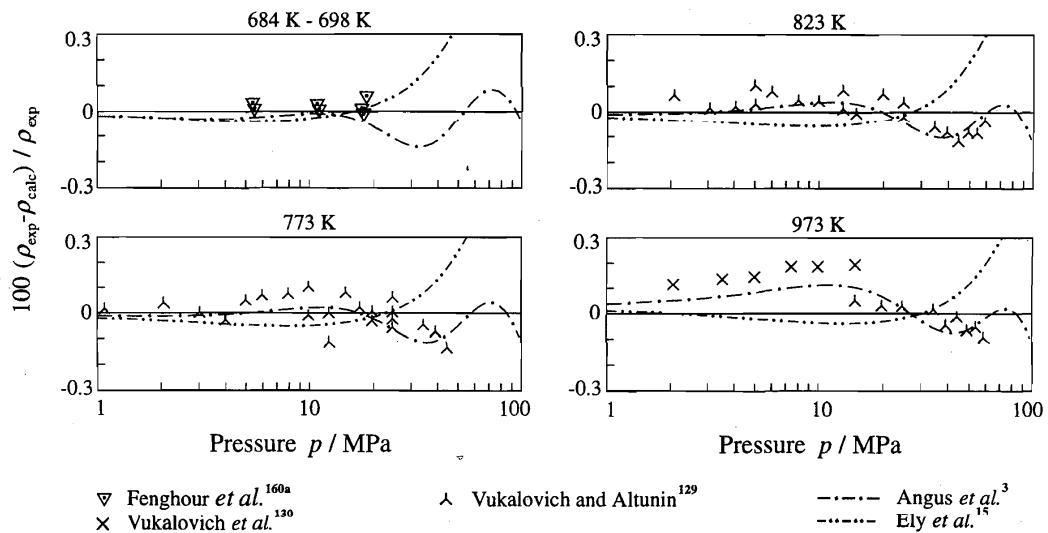


FIG. 25. Relative density deviations of selected $p\rho T$ data at high temperatures from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

in density. For temperatures up to 698 K, the recent data of Fenghour *et al.*^{160a} improve the uncertainty of the $p\rho T$ surface to less than $\pm 0.1\%$ in density.

A representative view on the complete group 1 set of the $p\rho T$ data up to temperatures of 173 K and pressures of

200 MPa is given in Fig. 24. Generally, the new equation of state describes the reliable data better than the older equations. The comparison with the data sets of Duscheck *et al.*¹⁵⁴ and Gilgen *et al.*¹⁵⁹ shows that the use of adjusted data (see Sec. 4.10) was reasonable.

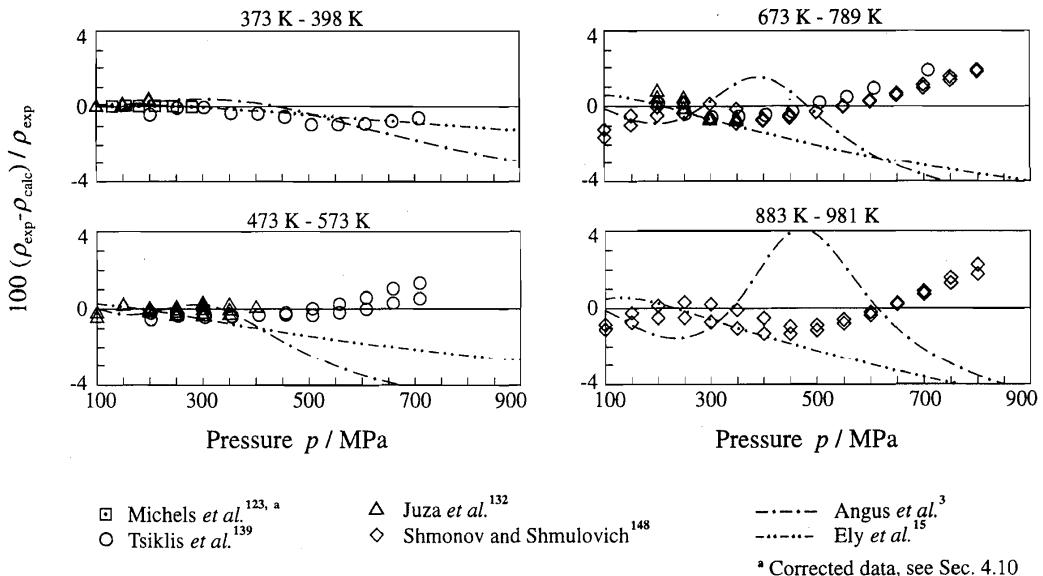


FIG. 26. Relative density deviations of selected $p\rho T$ data at high pressures from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison; in this pressure range, these two equations of state are at least partly extrapolated (see Table 1).

* Corrected data, see Sec. 4.10

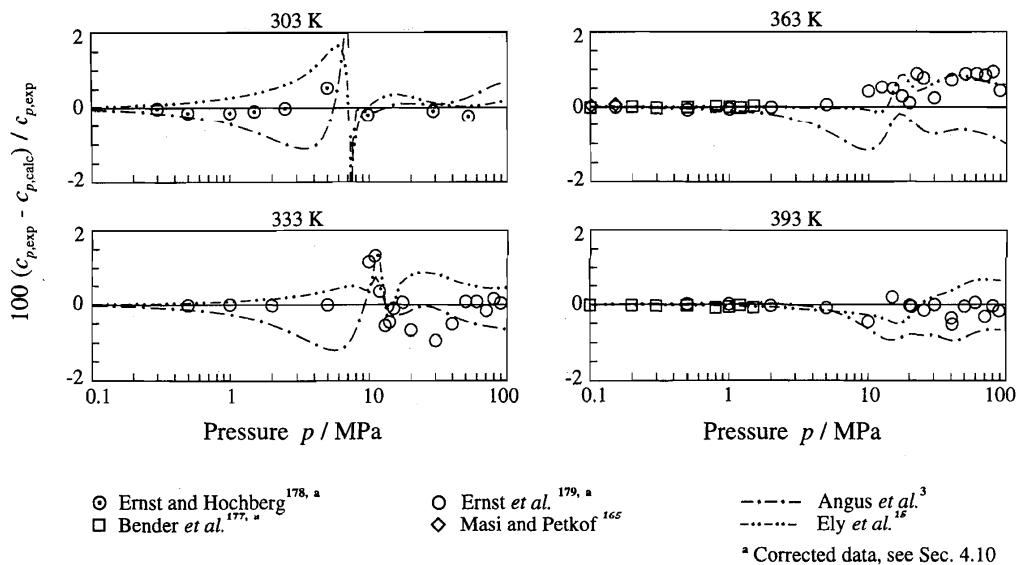


FIG. 27. Relative deviations of selected isobaric heat capacity data from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

At temperatures above 698 K, Eq. (6.1) is essentially based on the same data sets as the equations of Ely *et al.*¹⁵ and Angus *et al.*³ Nevertheless, the three equations show significantly different courses for pressures above 15 MPa. Figure 25 shows that the equation of Angus *et al.*³ yields the best representation of the data of Vukalovich and Altunin.^{128,129} However, in order to achieve a consistent description of the caloric and thermal properties in other regions, we had to assume that this data set exhibits a systematic error. The data of Fenghour *et al.*^{160a} support our interpretation of the $p\rho T$ surface for temperatures up to 698 K.

Figure 26 shows how the $p\rho T$ data at very high pressures are represented. Since the range of validity is limited to 100 MPa for the equation of Angus *et al.*³ and to 300 MPa for the equation of Ely *et al.*¹⁵ these equations are already extrapolated when plotting values calculated from these equations in Fig. 26. With an estimated uncertainty ranging from 1% to 2% in density, the data of Tsiklis *et al.*¹³⁹ and Shmonov and Shmulovich¹⁴⁸ represent the transition to the extrapolation range of Eq. (6.1) which is discussed in Sec. 7.3. Equation (6.1) yields a suitable representation of these data.

7.2.2 Caloric Properties in the Single-Phase Region

In the gas and the supercritical region, the caloric behavior of an equation of state for carbon dioxide can be discussed most advantageously by the example of the specific isobaric heat capacity. Figure 27 shows the deviation between values calculated from Eq. (6.1) and reliable measurements of c_p . The data of Bender *et al.*,¹⁷⁷ Ernst and Hochberg,¹⁷⁸ and of Ernst *et al.*¹⁷⁹ were corrected according to the descriptions in

Sec. 4.10. The excellent representation of the data within the gas region, where the well-known contribution of c_p^0 is predominant, justifies this correction. In the region of the supercritical maximum of c_p , the deviations increase to about $\pm 1\%$ ($+1.3\%$ for a single data point) but the authors estimate that the uncertainty of their data also increases to $\pm 0.9\%$ in this region.

In Fig. 28, absolute values of the specific isobaric heat capacity in the low temperature gas region are plotted. When approaching the sublimation curve, Eq. (6.1) yields a reason-

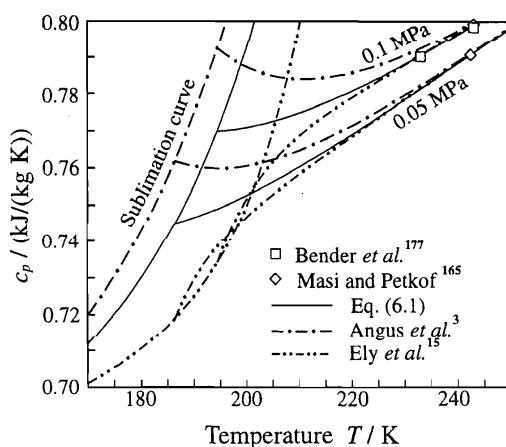


FIG. 28. Representation of the isobaric heat capacity on isobars in the gas region and in states on the sublimation curve (saturated vapor). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

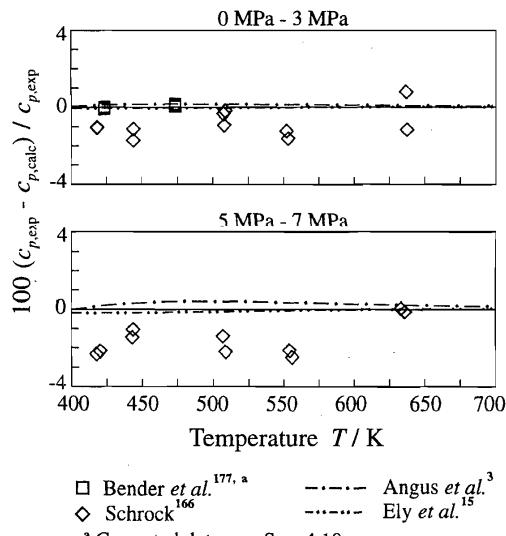


FIG. 29. Relative deviations of isobaric heat capacity data at high temperatures from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

able extrapolation of the plotted isobars. The equation of Angus *et al.*³ also shows a reasonable extrapolation behavior, but comparisons with recent data¹⁷⁷ at a temperature of 233 K indicate that the resulting values are too high. In contrast to this, the isobars calculated from the equation of Ely *et al.*¹⁵ intersect with each other and with the specific iso-

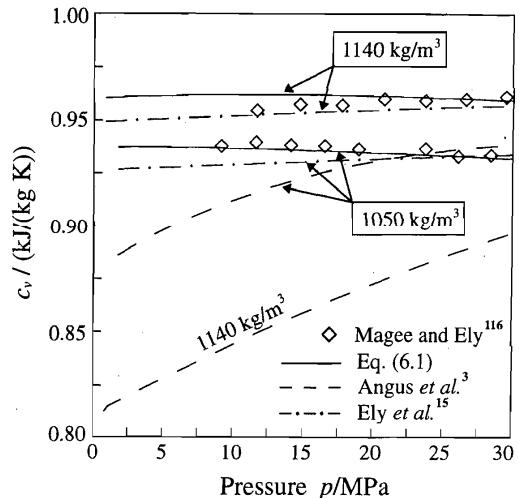


FIG. 31. Representation of the isochoric heat capacity on high-density isochores. For each of the isochores the plotted pressure range starts at the corresponding vapor pressure. Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

baric heat capacity on the sublimation line at temperatures below T_t . Due to the high triple-point pressure of CO₂ ($p_t = 0.51795$ MPa) and the widespread use of dry ice, an unreasonable behavior in this region is less acceptable for carbon dioxide than for other substances.

At temperatures above 400 K, the values calculated from the different equations of state agree much better with each other than with the data of Schrock¹⁶⁶ which are plotted in

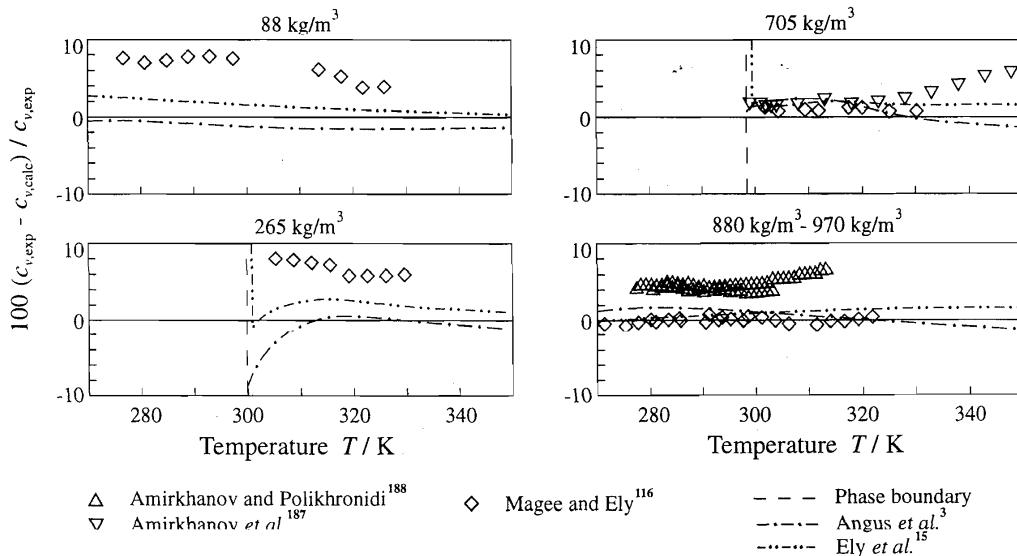


FIG. 30. Relative deviations of selected isochoric heat capacity data from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

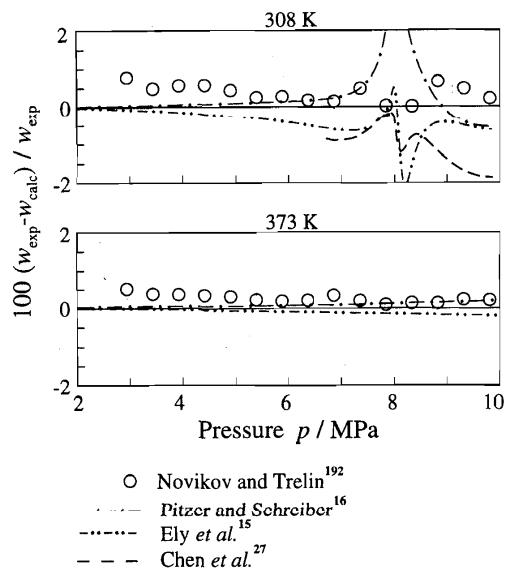


FIG. 32. Relative deviations of speed of sound data at supercritical temperatures from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and of Pitzer and Schreiber,¹⁶ and, in the range of validity, from the crossover equation of Chen *et al.*²⁷ are plotted for comparison.

Fig. 29. Up to 473 K, the data of Bender *et al.* support the results of the equations of state. At higher temperatures and moderate pressures, the influence of the residual part of c_p decreases. Since the uncertainty of $c_p^0(T)$ is very small (see Sec. 6.1) and at least some information on the residual part of the equations of state is available from $p\rho T$ data, the equations seem to be more reliable than the available c_p data in this region.

Deviations with regard to the specific isochoric heat capacity at gas and liquid densities are presented in Fig. 30. In the gas region, the behavior of the new fundamental equation concerning caloric properties is based on the precise data of c_p and w ; the deviations between the c_v data of Magee and Ely¹¹⁶ and values calculated from Eq. (6.1) and from the other equations of state, respectively, probably reflect the uncertainty in the data. This fact has resulted in the low average weighting factor listed in Table 17. At high densities, however, the c_v experiments of Magee and Ely¹¹⁶ yielded reliable results which form the most important source of information on the caloric properties at liquid densities.

Unfortunately, these c_v data only describe states at supercritical pressures (see Fig. 17), so that there is a wide gap between caloric data in the single-phase region and in the saturated liquid state. Figure 31 shows absolute values of the specific isochoric heat capacity on two liquid isochors, plotted versus pressure. Equation (6.1) follows the measurements on the 880 kg/m³, 970 kg/m³, and 1050 kg/m³ isochors and yields with decreasing pressure slightly increasing deviations from the c_v values at the 1140 kg/m³ isochore. In contrast to

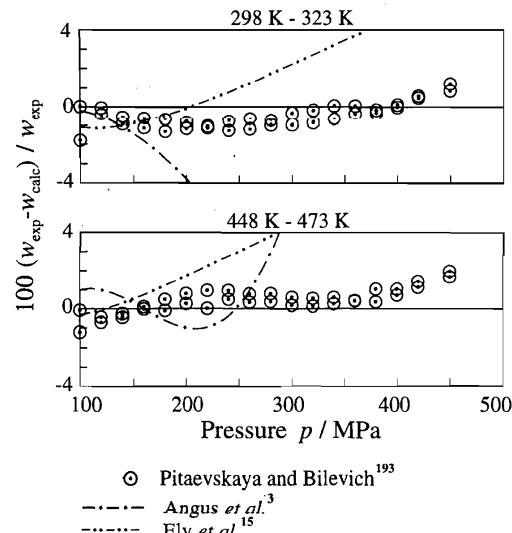


FIG. 33. Relative deviations of speed of sound data at high pressures from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison; in this pressure range, these two equations of state are at least partly extrapolated (see Table 1).

this behavior, the equation of Ely *et al.* follows the course of the 1140 kg/m³ isochore, but it yields slightly too low specific isochoric heat capacities at lower densities. In spite of these different tendencies, the deviations between c_v values calculated from these equations do not exceed 1.5% throughout the extrapolation down to the vapor pressure. Since the uncertainty in the specific heat capacity calculated from Eq. (6.1) is estimated to be $\leq \pm 1.5\%$ in the whole high-density region for pressures up to 40 MPa (see Sec. 8), we believe that the uncertainty at subcritical pressures does not increase due to the gap in the data set. New data which describe the caloric behavior of liquid carbon dioxide more accurately would be desirable in order to prove whether this assessment is correct.

The equation of Angus *et al.*³ fails completely in the description of the specific isochoric heat capacity at high densities. In the liquid region, the deviation between Eq. (6.1) and this formulation grows to 16%.

For carbon dioxide, the representation of speed of sound measurements is a sensitive test for the quality of an equation of state in the following two regions. The data of Novikov and Trelin¹⁹² describe the caloric behavior within the gas and supercritical region. Figure 32 illustrates the representation of w values on two representative isotherms of this data set. While all the considered formulations represent the data within their uncertainty at 373 K, only Eq. (6.1) is able to reproduce the measurements at 308 K; in the extended critical region, the deviations do not exceed $\pm 0.7\%$. On the 308 K isotherm the crossover equation of Chen *et al.*²⁷ yields deviations up to 2%.

At temperatures between 298 K and 473 K, Pitaevskaya and Bilevich¹⁹³ measured speed of sound data at pressures to

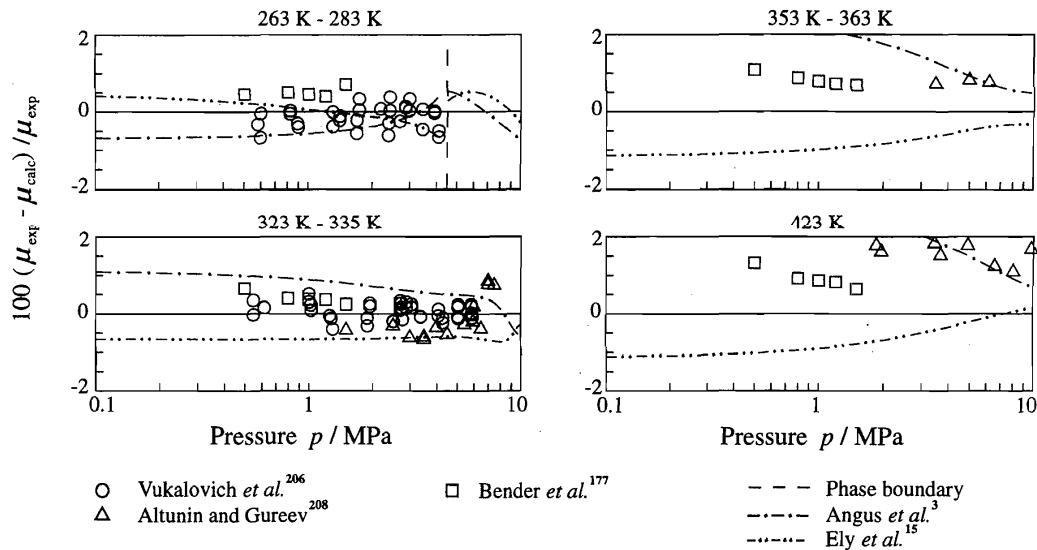


FIG. 34. Relative deviations of experimentally determined Joule-Thomson coefficients from values calculated from Eq. (6.1). Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison. The data of Vukalovich *et al.*²⁰⁶ were not used when establishing Eq. (6.1).

450 MPa. These data are represented by Eq. (6.1) to within their expected uncertainty of approximately $\pm 2\%$. Figure 33 shows representative deviation plots covering the lowest and highest temperatures of this data set. None of the previous equations of state is able to yield a reasonable representation of these data. The equation of Angus *et al.*³ is only valid up to 100 MPa, and extrapolated values of the speed of sound are expected to be uncertain. But the equation of Ely *et al.*¹⁵ should yield reliable results at least within the range of its validity, namely up to 300 MPa.

At pressures up to 1.5 MPa, the Joule Thomson measurements of Bender *et al.*¹⁷⁷ were used in the nonlinear fit but these data could not be represented without systematic, slightly temperature dependent deviations. After work on the new equation of state had been completed, the isothermal Joule-Thomson coefficients measured by Vukalovich *et al.*²⁰⁶ were converted into differential Joule-Thomson coefficients by the use of the specific isobaric heat capacity calculated from Eq. (6.1). The new equation represents the converted data of Vukalovich *et al.* without systematic deviations (see Fig. 34); the very accurate $p\rho T$ data set in the gas region prevented the representation of the measurements of Bender *et al.* which deviate from the correlation by approximately 0.5% to 1%.

7.3 Extrapolation Behavior of the New Fundamental Equation

Inspired by the discussion at the Fifth International Workshop on Equations of State, which took place in Bochum in 1990, the extrapolation behavior of empirical equations of state was examined in some detail during the work on carbon dioxide. Since these results cover features of different sub-

stances and general approaches, they will be discussed elsewhere.³⁵ Here, the considerations are restricted to the new fundamental equation for carbon dioxide; the following subsections will give only a brief survey on the extrapolation behavior of Eq. (6.1).

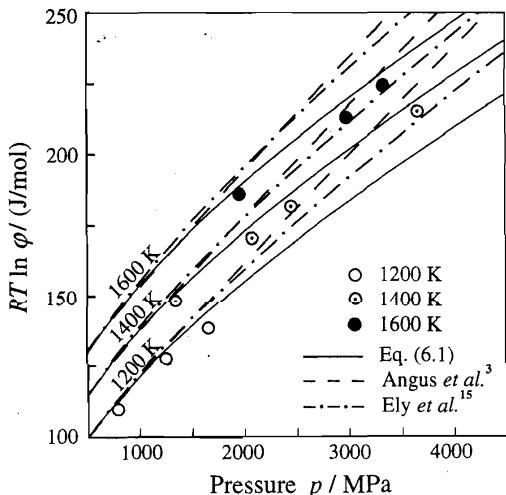


FIG. 35. Representation of experimentally determined fugacities on isotherms at very high temperatures and pressures. Values calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

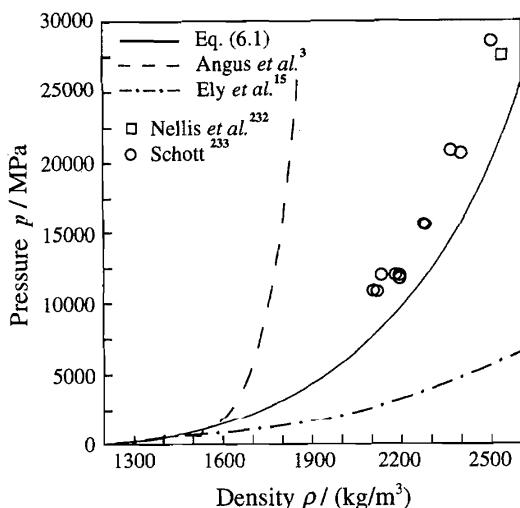


FIG. 36. Representation of experimental data describing the Hugoniot curve of carbon dioxide. Hugoniot curves calculated from the wide-range equations of Ely *et al.*¹⁵ and Angus *et al.*³ are plotted for comparison.

7.3.1 Extrapolation Beyond the Range of Primary Data

The range of validity of Eq. (6.1) is based on the range where reliable data of thermodynamical properties exist. However, two kinds of data exceed this range.

Figure 35 shows the representation of fugacities reaching up to approximately 3600 MPa at temperatures between 1200 K and 1600 K. The data of Haselton *et al.*²³¹ were not used when developing Eq. (6.1) since it is difficult to estimate the uncertainty of data originating from measurements of chemical equilibria and since the logarithmic structure of the dependency between the fugacity φ and the reduced Helmholtz energy (see Table 3) prevents an inclusion into the linear optimization procedure. Nevertheless, Eq. (6.1) follows the course of the measurements, whereas both the equation of Angus *et al.*³ and the equation of Ely *et al.*¹⁵ yield fugacities which are significantly too large. At least at low pressures, the remaining systematic deviations cannot be explained by a misbehavior of the equation of state. All equations of state which have been investigated result in very similar fugacities at pressures below 1000 MPa. In this region, the experimental results are inconsistent with $p\rho T$ data at lower temperatures.

At even higher pressures, shock wave measurements result in data for the Hugoniot relation

TABLE 33. The definition of the zeroth- and first-order ideal curves of the compression factor

| Name of the ideal curve | Definition |
|-------------------------------|---------------------------------|
| Classical ideal curve | $Z = pV/RT = 1$ |
| Boyle curve | $(\partial Z/\partial p)_T = 0$ |
| Joule-Thomson inversion curve | $(\partial Z/\partial T)_p = 0$ |
| Joule inversion curve | $(\partial Z/\partial p)_T = 0$ |

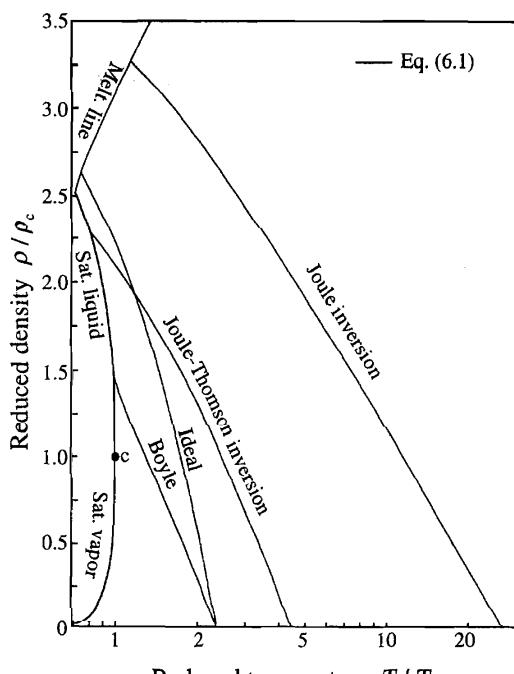


FIG. 37. The so-called ideal curves calculated from Eq. (6.1) and plotted in a ρ/ρ_c , $\log(T/T_c)$ diagram. The Joule-Thomson inversion curve and the Joule inversion curve exceed the temperature range in which Eq. (6.1) is fitted to experimental data.

$$h - h_{0H} = 0.5(p - p_{0H}) \cdot (1/\rho_{0H} + 1/\rho), \quad (7.1)$$

where h is the enthalpy, p the pressure, and ρ the density after releasing the shock wave and h_{0H} , p_{0H} , and ρ_{0H} are the initial values. Even though it is not yet clear whether these measurements describe equilibrium states at all, comparisons with these data are the only source of experimental information on the extrapolation behavior of an equation of state at very high pressures. Figure 36 shows Hugoniot plots calculated from Eq. (6.1) and from the other two equations of state considered here, compared with the data of Nellis *et al.*²³² and Schott.²³³ At approximately 34 000 MPa, Nellis *et al.* observed a kink in the course of the Hugoniot curve which is interpreted as an indication of a spontaneous disintegration reaction. So it can be seen that Eq. (6.1) yields a reasonable description of the Hugoniot curve of carbon dioxide up to the limits of chemical stability. A $T\rho$ plot, which is not given here, shows that the Hugoniot curves calculated from the equations of Ely *et al.*¹⁵ and Angus *et al.*³ run into low temperature solutions corresponding to solid states above densities of about 1400 kg/m³.

7.3.2 Representation of "Ideal Curves"

Various authors (see Refs. 234 to 238) have discussed plots of so-called ideal curves^e as a universal behavior of

^e"Ideal curves" are curves which connect all states where a special property of a fluid is equal to the corresponding property of the hypothetical ideal gas in the same state.

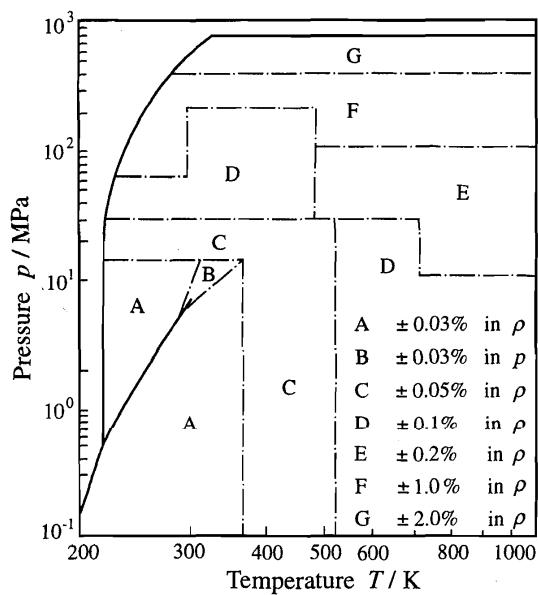


FIG. 38. Tolerance diagram for densities calculated from Eq. (6.1). In region B the uncertainty in pressure is given.

pure substances. In 1991, de Reuck²³⁹ gave a brief survey on this topic.

The most common ideal curves are the zeroth and first order curves of the compression factor which are defined by the relations given in Table 33. Figure 37 shows the plot of

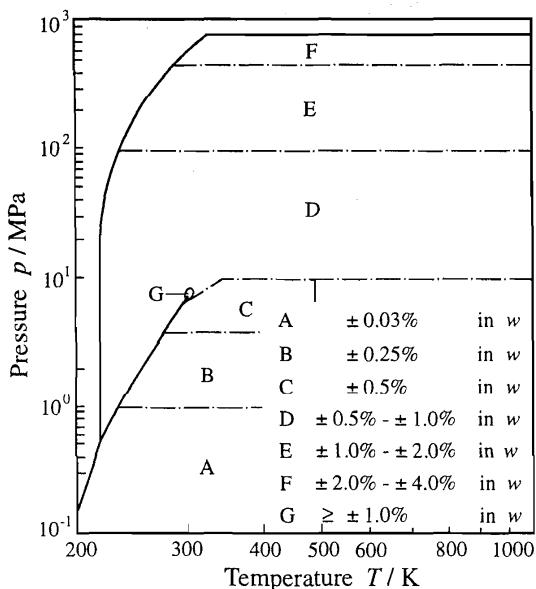


FIG. 39. Tolerance diagram for speed of sound data calculated from Eq. (6.1). In the immediate vicinity of the critical point (region G) it is difficult to estimate an uncertainty in w because of the growing influence of uncertainties in temperature and pressure measurement.

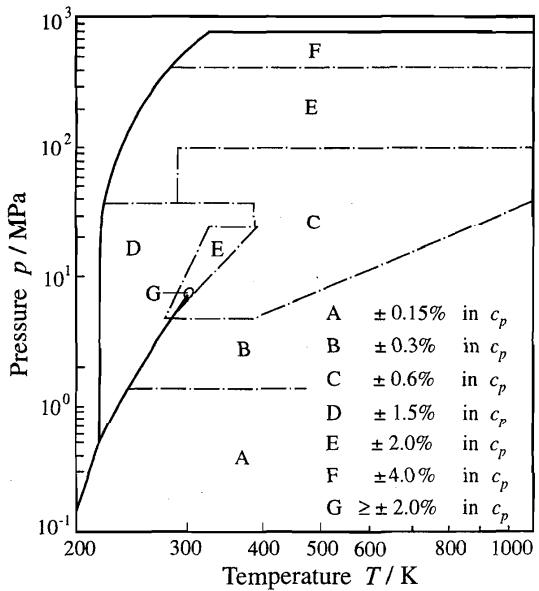


FIG. 40. Tolerance diagram for isobaric heat capacities calculated from Eq. (6.1). In the immediate vicinity of the critical point (region G) it is difficult to estimate an uncertainty in c_p because of the growing influence of uncertainties in temperature and pressure measurement.

these curves calculated from Eq. (6.1). The new fundamental equation was fitted to data up to reduced pressures of $p/p_c \approx 108$ and up to reduced temperatures of $T/T_c \approx 3.5$. Thus, the course of the ideal curves does not significantly exceed the pressure range covered by data, but both the Joule-Thomson inversion curve and the Joule inversion curve reach up to temperatures which clearly exceed the range of the data used to fit Eq. (6.1).

Preliminary equations showed an unreasonable plot of the Joule inversion curve at very high temperatures. In order to force the equation to form a maximum in the course of the second virial coefficient and to ensure that the equation of state yields an intersection of the Joule inversion curve with the zero pressure line at that temperature, 27 $T\rho$ data were determined by graphical extrapolation of the Joule inversion curve in a pT plot (see Ref. 35). At these values of the state variables, the condition of the Joule inversion curve, $\phi_{sr}^r = 0$, was introduced into the data set used during the adjustment of Eq. (6.1). Since it is difficult to estimate the uncertainty of the inversion condition, the weight of these data was determined by using estimations for the uncertainty of the independent variables T and ρ in combination with the Gaussian error propagation formula [see Eq. (2.6)].

Equation (6.1) shows reasonable plots of the ideal curves in the high temperature region, see Fig. 37. The temperature at which the Joule inversion curve intersects the zero pressure line and at which the second virial coefficient passes through a maximum corresponds to about $T/T_c = 26.9$. Thus, the reasonable behavior of Eq. (6.1) reaches even up to tem-

peratures beyond the limits of the chemical stability of carbon dioxide.

8. Uncertainty of the New Equation of State

Estimates for the uncertainty of an empirical equation of state have to be guided by comparisons with experimental data. In regions where no data are available, comparisons with existing equations of state can be used as a substitute. A conservative estimation of the uncertainty of $p\rho T$, w , and c_p values calculated from Eq. (6.1) is illustrated in the tolerance diagrams Figs. 38 to 40. Uncertainties in c_v correspond to the uncertainties given for c_p in the liquid and gas region. In the extended critical region, the uncertainty in c_v may exceed the uncertainty in c_p . The uncertainty of Δh or Δu values calculated from Eq. (6.1) is less than or equal to the uncertainty in c_p or c_v , respectively.

Outside the range of its validity, Eq. (6.1) should yield reasonable results for the basic thermodynamic properties like pressure, enthalpy, and fugacity within the whole chemically stable region of carbon dioxide. Of course, the extrapolation results have an increased uncertainty which cannot be estimated. The calculation of derived properties such as the speed of sound or specific heat capacities is not recommended beyond the limits of validity. If such data are needed, the results should be checked carefully.

9. Conclusions

Based on a comprehensive study on the experimental data for the thermodynamic properties of carbon dioxide, a new fundamental equation in the form of the Helmholtz energy has been developed. This empirical formulation is valid in the fluid region up to temperatures of 1100 K and at pressures up to 800 MPa. The equation is able to represent almost all the reliable data in the homogeneous region and on

the liquid-vapor phase boundary within their experimental uncertainty. The consideration of state-of-the-art data has resulted in a previously unequalled accuracy for the regions of major technical interest. Intensive work on the consistency of the data set used has led to reasonable results in regions with a poor data situation.

Special interest has been focused on the behavior of calorific properties in the critical region and on the extrapolation behavior of empirical equations of state. The introduction of nonanalytic terms enables the new wide-range equation of state to represent the isochoric heat capacity and the speed of sound even in the immediate vicinity of the critical point; up to now, this attribute has only been a domain of scaled equations of state which introduce iterative dependencies between different sets of variables and a limited range of validity. An examination of the extrapolation behavior of empirical equations of state has resulted in new approaches which have been used for the new formulation. For the basic properties of carbon dioxide such as pressure, enthalpy, and fugacity, the new fundamental equation should yield reasonable results within the whole region of chemical stability.

10. Appendix: Thermodynamic Properties of Carbon Dioxide

In order to preserve thermodynamic consistency all values presented in Tables 34 and 35 were calculated only from the new equation of state, Eq. (6.1). Ideally, each entry in the table should be given to one more significant figure than the input data warrant, but a strict adherence to this principle is difficult, and a possible conflict has always been avoided by including more figures than are strictly necessary. Especially in the extended critical region, interpolation between values given may result in uncertainties which are significantly larger than the uncertainties of Eq. (6.1). For sophisticated applications, values should be calculated directly from Eq. (6.1); a computer-code suitable for such applications can be obtained from the authors.

TABLE 34. Thermodynamic properties of saturated carbon dioxide

| Temperature (K) | Pressure (MPa) | Density (kg/m ³) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | <i>c_v</i> [kJ/(kg K)] | <i>c_p</i> [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|-------------------|---------------------------------|---------------------|------------------------|-------------------------------------|-------------------------------------|-------------------------|
| 216.592 ^a | 0.51796 | 1178.46 | -426.74 | -2.2177 | 0.97466 | 1.9532 | 975.85 |
| | | 13.761 | -76.364 | -0.59999 | 0.62921 | 0.90872 | 222.78 |
| 218 | 0.55042 | 1173.40 | -423.98 | -2.2051 | 0.97264 | 1.9566 | 965.66 |
| | | 14.584 | -75.847 | -0.60815 | 0.63318 | 0.91743 | 222.94 |
| 220 | 0.59913 | 1166.14 | -420.05 | -2.1873 | 0.96983 | 1.9618 | 951.21 |
| | | 15.817 | -75.142 | -0.61957 | 0.63894 | 0.93032 | 223.15 |
| 222 | 0.65102 | 1158.81 | -416.11 | -2.1697 | 0.96707 | 1.9676 | 936.79 |
| | | 17.131 | -74.473 | -0.63080 | 0.64485 | 0.94386 | 223.31 |
| 224 | 0.70621 | 1151.40 | -412.16 | -2.1522 | 0.96437 | 1.9739 | 922.37 |
| | | 18.530 | -73.840 | -0.64185 | 0.65091 | 0.95807 | 223.44 |
| 226 | 0.76484 | 1143.92 | -408.19 | -2.1348 | 0.96174 | 1.9810 | 907.95 |
| | | 20.016 | -73.246 | -0.65274 | 0.65712 | 0.97302 | 223.52 |
| 228 | 0.82703 | 1136.34 | -404.21 | -2.1175 | 0.95917 | 1.9886 | 893.53 |
| | | 21.595 | -72.692 | -0.66347 | 0.66350 | 0.98875 | 223.57 |
| 230 | 0.89291 | 1128.68 | -400.21 | -2.1003 | 0.95667 | 1.9970 | 879.09 |
| | | 23.271 | -72.178 | -0.67406 | 0.67004 | 1.0053 | 223.57 |
| 232 | 0.96262 | 1120.93 | -396.19 | -2.0832 | 0.95425 | 2.0061 | 864.63 |
| | | 25.050 | -71.708 | -0.68452 | 0.67675 | 1.0228 | 223.54 |
| 234 | 1.0363 | 1113.08 | -392.16 | -2.0661 | 0.95190 | 2.0160 | 850.14 |
| | | 26.936 | -71.283 | -0.69487 | 0.68363 | 1.0412 | 223.46 |
| 236 | 1.1141 | 1105.12 | -388.11 | -2.0492 | 0.94963 | 2.0267 | 835.61 |
| | | 28.935 | -70.903 | -0.70511 | 0.69068 | 1.0608 | 223.33 |
| 238 | 1.1961 | 1097.05 | -384.04 | -2.0323 | 0.94745 | 2.0384 | 821.02 |
| | | 31.052 | -70.573 | -0.71526 | 0.69792 | 1.0814 | 223.17 |
| 240 | 1.2825 | 1088.87 | -379.94 | -2.0155 | 0.94535 | 2.0510 | 806.38 |
| | | 33.295 | -70.293 | -0.72532 | 0.70534 | 1.1033 | 222.96 |
| 242 | 1.3734 | 1080.56 | -375.82 | -1.9988 | 0.94335 | 2.0647 | 791.67 |
| | | 35.670 | -70.066 | -0.73533 | 0.71297 | 1.1265 | 222.70 |
| 244 | 1.4690 | 1072.13 | -371.68 | -1.9821 | 0.94145 | 2.0795 | 776.87 |
| | | 38.184 | -69.894 | -0.74527 | 0.72081 | 1.1513 | 222.40 |
| 246 | 1.5693 | 1063.56 | -367.51 | -1.9654 | 0.93965 | 2.0956 | 761.97 |
| | | 40.845 | -69.780 | -0.75518 | 0.72889 | 1.1778 | 222.06 |
| 248 | 1.6746 | 1054.84 | -363.30 | -1.9488 | 0.93797 | 2.1131 | 746.95 |
| | | 43.662 | -69.726 | -0.76506 | 0.73725 | 1.2061 | 221.66 |
| 250 | 1.7850 | 1045.97 | -359.07 | -1.9323 | 0.93643 | 2.1320 | 731.78 |
| | | 46.644 | -69.736 | -0.77492 | 0.74591 | 1.2366 | 221.22 |
| 252 | 1.9007 | 1036.93 | -354.80 | -1.9157 | 0.93506 | 2.1577 | 716.44 |
| | | 49.801 | -69.813 | -0.78479 | 0.75489 | 1.2693 | 220.72 |
| 254 | 2.0217 | 1027.72 | -350.50 | -1.8991 | 0.93390 | 2.1751 | 700.88 |
| | | 53.144 | -69.960 | -0.79467 | 0.76421 | 1.3047 | 220.17 |
| 256 | 2.1483 | 1018.32 | -346.15 | -1.8826 | 0.93300 | 2.1995 | 685.08 |
| | | 56.685 | -70.181 | -0.80458 | 0.77388 | 1.3429 | 219.56 |
| 258 | 2.2806 | 1008.71 | -341.77 | -1.8660 | 0.93244 | 2.2262 | 668.99 |
| | | 60.438 | -70.480 | -0.81453 | 0.78390 | 1.3844 | 218.90 |
| 260 | 2.4188 | 998.89 | -337.34 | -1.8495 | 0.93227 | 2.2554 | 652.58 |
| | | 64.417 | -70.862 | -0.82456 | 0.79426 | 1.4295 | 218.19 |
| 262 | 2.5630 | 988.83 | -332.86 | -1.8329 | 0.93258 | 2.2874 | 635.84 |
| | | 68.640 | -71.332 | -0.83467 | 0.80498 | 1.4787 | 217.41 |
| 264 | 2.7134 | 978.51 | -328.33 | -1.8162 | 0.93344 | 2.3226 | 618.75 |
| | | 73.124 | -71.896 | -0.84488 | 0.81604 | 1.5326 | 216.59 |
| 266 | 2.8701 | 967.92 | -323.74 | -1.7995 | 0.93488 | 2.3617 | 601.31 |
| | | 77.891 | -72.561 | -0.85523 | 0.82749 | 1.5919 | 215.70 |
| 268 | 3.0334 | 957.04 | -319.09 | -1.7827 | 0.93693 | 2.4050 | 583.54 |
| | | 82.965 | -73.334 | -0.86573 | 0.83935 | 1.6575 | 214.76 |
| 270 | 3.2033 | 945.83 | -314.37 | -1.7658 | 0.93959 | 2.4534 | 565.46 |
| | | 88.374 | -74.223 | -0.87641 | 0.85168 | 1.7307 | 213.75 |
| 272 | 3.3802 | 934.26 | -309.57 | -1.7488 | 0.94283 | 2.5079 | 547.11 |
| | | 94.148 | 75.240 | 0.88732 | 0.86454 | 1.8128 | 212.68 |
| 274 | 3.5642 | 922.30 | -304.70 | -1.7317 | 0.94659 | 2.5694 | 528.51 |
| | | 100.32 | -76.395 | -0.89849 | 0.87801 | 1.9057 | 211.55 |
| 276 | 3.7555 | 909.90 | -299.73 | -1.7144 | 0.95082 | 2.6396 | 509.71 |
| | | 106.95 | -77.702 | -0.90995 | 0.89218 | 2.0117 | 210.35 |

TABLE 34. Thermodynamic properties of saturated carbon dioxide—Continued

| Temperature (K) | Pressure (MPa) | Density (kg/m ³) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|-----------------------|-------------------|---------------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 278 | 3.9542 | 897.02 | -294.66 | -1.6969 | 0.95545 | 2.7203 | 490.72 |
| | | 114.07 | -79.177 | -0.92178 | 0.90719 | 2.1341 | 209.07 |
| 280 | 4.1607 | 883.58 | -289.48 | -1.6792 | 0.96046 | 2.8141 | 471.54 |
| | | 121.74 | -80.840 | -0.93401 | 0.92316 | 2.2769 | 207.72 |
| 282 | 4.3752 | 869.52 | -284.17 | -1.6611 | 0.96584 | 2.9246 | 452.19 |
| | | 130.05 | -82.713 | -0.94674 | 0.94029 | 2.4458 | 206.28 |
| 284 | 4.5978 | 854.74 | -278.71 | -1.6428 | 0.97166 | 3.0569 | 432.63 |
| | | 139.09 | -84.825 | -0.96006 | 0.95878 | 2.6490 | 204.74 |
| 286 | 4.8289 | 839.12 | -273.08 | -1.6239 | 0.97806 | 3.2181 | 412.81 |
| | | 148.98 | -87.214 | -0.97407 | 0.97895 | 2.8979 | 203.10 |
| 288 | 5.0688 | 822.50 | -267.24 | -1.6046 | 0.98528 | 3.4189 | 392.63 |
| | | 159.87 | -89.926 | -0.98894 | 1.0012 | 3.2104 | 201.34 |
| 290 | 5.3177 | 804.67 | -261.15 | -1.5846 | 0.99373 | 3.6756 | 371.95 |
| | | 171.96 | -93.025 | -1.0049 | 1.0260 | 3.6142 | 199.45 |
| 292 | 5.5761 | 785.33 | -254.76 | -1.5637 | 1.0041 | 4.0145 | 350.49 |
| | | 185.55 | -96.599 | -1.0221 | 1.0543 | 4.1558 | 197.38 |
| 294 | 5.8443 | 764.09 | -247.97 | -1.5418 | 1.0177 | 4.4834 | 327.85 |
| | | 201.06 | 100.77 | 1.0411 | 1.0872 | 4.9196 | 195.09 |
| 296 | 6.1227 | 740.28 | -240.68 | -1.5183 | 1.0371 | 5.1813 | 303.44 |
| | | 219.14 | -105.74 | -1.0624 | 1.1269 | 6.0741 | 192.49 |
| 298 | 6.4121 | 712.77 | -232.64 | -1.4926 | 1.0675 | 6.3473 | 276.42 |
| | | 240.90 | -111.83 | -1.0872 | 1.1774 | 8.0128 | 189.38 |
| 300 | 6.7131 | 679.24 | -223.40 | -1.4631 | 1.1199 | 8.6979 | 245.67 |
| | | 268.58 | -119.70 | -1.1175 | 1.2476 | 11.921 | 185.33 |
| 301 | 6.8683 | 658.69 | -218.03 | -1.4460 | 1.1631 | 11.053 | 228.18 |
| | | 286.15 | -124.73 | -1.1361 | 1.2972 | 15.859 | 182.61 |
| 302 | 7.0268 | 633.69 | -211.76 | -1.4261 | 1.2316 | 15.786 | 208.08 |
| | | 308.15 | -131.05 | -1.1588 | 1.3676 | 23.800 | 178.91 |
| 303 | 7.1890 | 599.86 | -203.73 | -1.4004 | 1.3702 | 30.233 | 182.14 |
| | | 339.00 | -139.91 | -1.1897 | 1.4925 | 47.599 | 172.71 |
| 304 | 7.3555 | 530.30 | -188.42 | -1.3509 | 2.0531 | 386.88 | 134.14 |
| | | 406.42 | -158.84 | -1.2536 | 2.0679 | 555.58 | 147.62 |
| 304.1282 ^b | 7.3773 | 467.60 | -174.53 | -1.3054 | | | |

^aTriple point.^bCritical point.

TABLE 35. Thermodynamic properties of carbon dioxide

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | <i>c_v</i> [kJ/(kg K)] | <i>c_p</i> [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|-------------------------------------|-------------------------------------|-------------------------|
| 0.05 MPa Isobar | | | | | | | |
| 186.436 ^a | 1.4370 | -123.74 | -88.944 | -0.23757 | 0.54404 | 0.74495 | 216.947 |
| 190 | 1.4089 | -121.78 | -86.286 | -0.22345 | 0.54661 | 0.74660 | 218.90 |
| 200 | 1.3359 | -116.22 | -78.792 | -0.18501 | 0.55478 | 0.75266 | 224.26 |
| 210 | 1.2704 | -110.59 | -71.228 | -0.14811 | 0.56398 | 0.76029 | 229.41 |
| 220 | 1.2112 | -104.86 | -63.582 | -0.11254 | 0.57386 | 0.76897 | 234.38 |
| 230 | 1.1575 | -99.044 | -55.846 | -0.07816 | 0.58417 | 0.77834 | 239.20 |
| 240 | 1.1084 | -93.125 | -48.014 | -0.04483 | 0.59473 | 0.78815 | 243.88 |
| 250 | 1.0634 | -87.104 | -40.082 | -0.01245 | 0.60542 | 0.79823 | 248.44 |
| 260 | 1.0219 | -80.978 | -32.049 | 0.01906 | 0.61612 | 0.80845 | 252.88 |
| 270 | 0.98360 | -74.747 | -23.913 | 0.04976 | 0.62679 | 0.81871 | 257.23 |
| 280 | 0.94810 | -68.412 | -15.675 | 0.07972 | 0.63737 | 0.82895 | 261.49 |
| 290 | 0.91510 | -61.973 | -7.3344 | 0.10899 | 0.64782 | 0.83912 | 265.67 |
| 300 | 0.88434 | -55.432 | 1.1072 | 0.13761 | 0.65812 | 0.84917 | 269.77 |
| 325 | 0.81585 | -38.641 | 22.645 | 0.20655 | 0.68307 | 0.87366 | 279.71 |
| 350 | 0.75726 | -21.246 | 44.781 | 0.27216 | 0.70681 | 0.89707 | 289.27 |
| 375 | 0.70656 | -3.2771 | 67.489 | 0.33481 | 0.72932 | 0.91933 | 298.50 |
| 400 | 0.66224 | 15.237 | 90.738 | 0.39483 | 0.75063 | 0.94046 | 307.42 |
| 425 | 0.62317 | 34.268 | 114.50 | 0.45245 | 0.77081 | 0.96051 | 316.08 |
| 450 | 0.58847 | 53.788 | 138.76 | 0.50789 | 0.78995 | 0.97953 | 324.50 |
| 475 | 0.55743 | 73.774 | 163.47 | 0.56134 | 0.80811 | 0.99760 | 332.69 |
| 500 | 0.52951 | 94.201 | 188.63 | 0.61295 | 0.82537 | 1.0148 | 340.67 |
| 525 | 0.50426 | 115.05 | 214.20 | 0.66286 | 0.84179 | 1.0312 | 348.46 |
| 550 | 0.48130 | 136.29 | 240.18 | 0.71120 | 0.85744 | 1.0468 | 356.08 |
| 575 | 0.46035 | 157.92 | 266.54 | 0.75806 | 0.87236 | 1.0616 | 363.53 |
| 600 | 0.44115 | 179.92 | 293.26 | 0.80354 | 0.88660 | 1.0758 | 370.83 |
| 700 | 0.37809 | 271.21 | 403.45 | 0.97331 | 0.93747 | 1.1266 | 398.65 |
| 800 | 0.33081 | 367.15 | 518.30 | 1.1266 | 0.97994 | 1.1690 | 424.64 |
| 900 | 0.29404 | 466.98 | 637.03 | 1.2664 | 1.0155 | 1.2045 | 449.13 |
| 1000 | 0.26463 | 570.06 | 759.01 | 1.3949 | 1.0452 | 1.2342 | 472.37 |
| 1100 | 0.24057 | 675.87 | 883.71 | 1.5137 | 1.0702 | 1.2592 | 494.54 |
| 0.10 MPa Isobar | | | | | | | |
| 194.525 ^a | 2.7796 | -120.24 | -84.267 | -0.34184 | 0.56013 | 0.76998 | 219.98 |
| 200 | 2.6980 | -117.11 | -80.049 | -0.32046 | 0.56339 | 0.77091 | 223.00 |
| 210 | 2.5617 | -111.36 | -72.323 | -0.28276 | 0.57062 | 0.77476 | 228.33 |
| 220 | 2.4394 | -105.54 | -64.547 | -0.24659 | 0.57907 | 0.78067 | 233.45 |
| 230 | 2.3288 | -99.645 | -56.705 | -0.21173 | 0.58833 | 0.78795 | 238.38 |
| 240 | 2.2282 | -93.664 | -48.785 | -0.17803 | 0.59811 | 0.79618 | 243.15 |
| 250 | 2.1363 | -87.589 | -40.780 | -0.14535 | 0.60818 | 0.80501 | 247.79 |
| 260 | 2.0519 | -81.419 | -32.684 | -0.11360 | 0.61843 | 0.81424 | 252.31 |
| 270 | 1.9741 | -75.151 | -24.494 | -0.08269 | 0.62872 | 0.82371 | 256.72 |
| 280 | 1.9021 | -68.784 | -16.209 | -0.05256 | 0.63900 | 0.83330 | 261.03 |
| 290 | 1.8352 | -62.317 | -7.8279 | -0.02315 | 0.64922 | 0.84293 | 265.25 |
| 300 | 1.7730 | -55.751 | 0.64941 | 0.00559 | 0.65932 | 0.85253 | 269.39 |
| 325 | 1.6348 | -38.911 | 22.260 | 0.07477 | 0.68392 | 0.87619 | 279.42 |
| 350 | 1.5167 | -21.479 | 44.452 | 0.14054 | 0.70743 | 0.89903 | 289.04 |
| 375 | 1.4147 | -3.4815 | 67.203 | 0.20332 | 0.72978 | 0.92090 | 298.31 |
| 400 | 1.3257 | 15.056 | 90.488 | 0.26342 | 0.75099 | 0.94173 | 307.28 |
| 425 | 1.2472 | 34.105 | 114.28 | 0.32111 | 0.77109 | 0.96156 | 315.97 |
| 450 | 1.1776 | 53.640 | 138.56 | 0.37661 | 0.79017 | 0.98041 | 324.41 |
| 475 | 1.1154 | 73.639 | 163.29 | 0.43011 | 0.80829 | 0.99835 | 332.62 |
| 500 | 1.0594 | 94.076 | 188.47 | 0.48175 | 0.82552 | 1.0154 | 340.62 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 0.10 MPa Isobar | | | | | | | |
| 525 | 1.0088 | 114.93 | 214.06 | 0.53169 | 0.84192 | 1.0317 | 348.43 |
| 550 | 0.96283 | 136.19 | 240.05 | 0.58005 | 0.85755 | 1.0473 | 356.06 |
| 575 | 0.92087 | 157.82 | 266.42 | 0.62693 | 0.87245 | 1.0621 | 363.52 |
| 600 | 0.88242 | 179.82 | 293.15 | 0.67243 | 0.88668 | 1.0762 | 370.83 |
| 700 | 0.75619 | 271.13 | 403.38 | 0.84226 | 0.93752 | 1.1269 | 398.68 |
| 800 | 0.66158 | 367.09 | 518.24 | 0.99558 | 0.97997 | 1.1692 | 424.68 |
| 900 | 0.58803 | 466.93 | 636.99 | 1.1354 | 1.0155 | 1.2046 | 449.19 |
| 1000 | 0.52921 | 570.02 | 758.98 | 1.2639 | 1.0452 | 1.2343 | 472.43 |
| 1100 | 0.48109 | 675.83 | 883.69 | 1.3827 | 1.0702 | 1.2593 | 494.61 |
| 0.101325 MPa Isobar | | | | | | | |
| 194.685 ^a | 2.8147 | -120.18 | -84.180 | -0.34383 | 0.56049 | 0.77056 | 220.03 |
| 200 | 2.7345 | -117.14 | -80.083 | -0.32307 | 0.56362 | 0.77141 | 222.97 |
| 210 | 2.5963 | -111.38 | -72.352 | -0.28535 | 0.57080 | 0.77516 | 228.30 |
| 220 | 2.4722 | -105.56 | -64.573 | -0.24916 | 0.57921 | 0.78098 | 233.42 |
| 230 | 2.3601 | -99.661 | -56.728 | -0.21429 | 0.58845 | 0.78821 | 238.36 |
| 240 | 2.2581 | -93.678 | -48.806 | -0.18057 | 0.59820 | 0.79639 | 243.14 |
| 250 | 2.1649 | -87.602 | -40.798 | -0.14789 | 0.60826 | 0.80519 | 247.78 |
| 260 | 2.0793 | -81.431 | -32.701 | -0.11613 | 0.61849 | 0.81440 | 252.30 |
| 270 | 2.0004 | -75.162 | -24.509 | -0.08522 | 0.62878 | 0.82384 | 256.71 |
| 280 | 1.9274 | -68.793 | -16.223 | -0.05508 | 0.63905 | 0.83341 | 261.02 |
| 290 | 1.8597 | -62.326 | -7.8410 | -0.02567 | 0.64925 | 0.84303 | 265.24 |
| 300 | 1.7966 | -55.760 | 0.63726 | 0.00307 | 0.65935 | 0.85262 | 269.38 |
| 325 | 1.6565 | -38.918 | 22.250 | 0.07226 | 0.68394 | 0.87625 | 279.41 |
| 350 | 1.5369 | -21.486 | 44.443 | 0.13803 | 0.70745 | 0.89908 | 289.03 |
| 375 | 1.4335 | -3.4869 | 67.196 | 0.20082 | 0.72980 | 0.92094 | 298.31 |
| 400 | 1.3433 | 15.051 | 90.482 | 0.26092 | 0.75100 | 0.94177 | 307.28 |
| 425 | 1.2638 | 34.100 | 114.28 | 0.31862 | 0.77110 | 0.96159 | 315.97 |
| 450 | 1.1932 | 53.637 | 138.55 | 0.37412 | 0.79018 | 0.98044 | 324.41 |
| 475 | 1.1302 | 73.635 | 163.29 | 0.42761 | 0.80829 | 0.99837 | 332.62 |
| 500 | 1.0735 | 94.073 | 188.46 | 0.47926 | 0.82552 | 1.0155 | 340.62 |
| 525 | 1.0222 | 114.93 | 214.06 | 0.52920 | 0.84192 | 1.0317 | 348.43 |
| 550 | 0.97559 | 136.18 | 240.04 | 0.57756 | 0.85755 | 1.0473 | 356.06 |
| 575 | 0.93308 | 157.82 | 266.41 | 0.62444 | 0.87246 | 1.0621 | 363.52 |
| 600 | 0.89412 | 179.82 | 293.14 | 0.66994 | 0.88668 | 1.0762 | 370.83 |
| 700 | 0.76621 | 271.13 | 403.38 | 0.83977 | 0.93752 | 1.1269 | 398.68 |
| 800 | 0.67035 | 367.09 | 518.24 | 0.99309 | 0.97997 | 1.1692 | 424.68 |
| 900 | 0.59582 | 466.93 | 636.99 | 1.1329 | 1.0155 | 1.2046 | 449.19 |
| 1000 | 0.53622 | 570.02 | 758.98 | 1.2614 | 1.0452 | 1.2343 | 472.43 |
| 1100 | 0.48746 | 675.83 | 883.69 | 1.3803 | 1.0702 | 1.2593 | 494.61 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 0.20 MPa Isobar | | | | | | | |
| 203.314 ^a | 5.4054 | -116.97 | -79.973 | -0.44750 | 0.58210 | 0.80842 | 222.32 |
| 210 | 5.2116 | -112.95 | -74.577 | -0.42138 | 0.58456 | 0.80597 | 226.10 |
| 220 | 4.9495 | -106.93 | -66.522 | -0.38391 | 0.58993 | 0.80556 | 231.52 |
| 230 | 4.7152 | -100.87 | -58.456 | -0.34806 | 0.59692 | 0.80819 | 236.70 |
| 240 | 4.5039 | -94.758 | -50.352 | -0.31357 | 0.60502 | 0.81291 | 241.68 |
| 250 | 4.3120 | -88.575 | -42.193 | -0.28026 | 0.61383 | 0.81906 | 246.49 |
| 260 | 4.1369 | -82.313 | -33.967 | -0.24800 | 0.62310 | 0.82618 | 251.16 |
| 270 | 3.9761 | -75.967 | -25.667 | -0.21668 | 0.63264 | 0.83396 | 255.69 |
| 280 | 3.8280 | -69.534 | -17.286 | -0.18620 | 0.64231 | 0.84219 | 260.10 |
| 290 | 3.6909 | -63.010 | -8.8222 | -0.15650 | 0.65203 | 0.85070 | 264.42 |
| 300 | 3.5636 | -56.394 | -0.27188 | -0.12751 | 0.66174 | 0.85938 | 268.64 |
| 325 | 3.2819 | -39.454 | 21.487 | -0.05786 | 0.68562 | 0.88131 | 278.83 |
| 350 | 3.0423 | -21.947 | 43.792 | 0.00825 | 0.70867 | 0.90300 | 288.58 |
| 375 | 2.8360 | -3.8914 | 66.631 | 0.07127 | 0.73072 | 0.92405 | 297.95 |
| 400 | 2.6562 | 14.692 | 89.987 | 0.13156 | 0.75170 | 0.94429 | 306.99 |
| 425 | 2.4981 | 33.778 | 113.84 | 0.18939 | 0.77166 | 0.96367 | 315.74 |
| 450 | 2.3580 | 53.344 | 138.16 | 0.24500 | 0.79062 | 0.98219 | 324.23 |
| 475 | 2.2328 | 73.368 | 162.94 | 0.29858 | 0.80865 | 0.99986 | 332.49 |
| 500 | 2.1204 | 93.827 | 188.15 | 0.35030 | 0.82582 | 1.0167 | 340.53 |
| 525 | 2.0188 | 114.70 | 213.77 | 0.40030 | 0.84217 | 1.0329 | 348.37 |
| 550 | 1.9265 | 135.97 | 239.79 | 0.44871 | 0.85776 | 1.0482 | 356.02 |
| 575 | 1.8424 | 157.62 | 266.18 | 0.49563 | 0.87263 | 1.0630 | 363.51 |
| 600 | 1.7653 | 179.63 | 292.93 | 0.54117 | 0.88684 | 1.0770 | 370.83 |
| 700 | 1.5124 | 270.99 | 403.22 | 0.71109 | 0.93761 | 1.1274 | 398.74 |
| 800 | 1.3230 | 366.97 | 518.13 | 0.86447 | 0.98003 | 1.1696 | 424.78 |
| 900 | 1.1759 | 466.82 | 636.91 | 1.0043 | 1.0155 | 1.2049 | 449.30 |
| 1000 | 1.0582 | 569.93 | 758.93 | 1.1329 | 1.0452 | 1.2345 | 472.56 |
| 1100 | 0.96197 | 675.75 | 883.66 | 1.2517 | 1.0702 | 1.2594 | 494.75 |
| 0.30 MPa Isobar | | | | | | | |
| 208.797 ^a | 8.0141 | -115.37 | -77.936 | -0.51088 | 0.59903 | 0.84154 | 223.07 |
| 210 | 7.9594 | -114.62 | -76.925 | -0.50605 | 0.59918 | 0.84031 | 223.78 |
| 220 | 7.5367 | -108.37 | -68.563 | -0.46715 | 0.60144 | 0.83277 | 229.53 |
| 230 | 7.1633 | -102.13 | -60.253 | -0.43021 | 0.60593 | 0.82996 | 234.98 |
| 240 | 6.8298 | -95.878 | -51.953 | -0.39488 | 0.61219 | 0.83067 | 240.18 |
| 250 | 6.5292 | -89.579 | -43.632 | -0.36091 | 0.61964 | 0.83382 | 245.17 |
| 260 | 6.2564 | -83.222 | -35.271 | -0.32812 | 0.62788 | 0.83863 | 249.98 |
| 270 | 6.0072 | -76.795 | -26.855 | -0.29636 | 0.63662 | 0.84459 | 254.64 |
| 280 | 5.7785 | -70.293 | -18.376 | -0.26553 | 0.64567 | 0.85136 | 259.17 |
| 290 | 5.5675 | -63.710 | -9.8262 | -0.23553 | 0.65488 | 0.85869 | 263.58 |
| 300 | 5.3723 | -57.043 | -1.2010 | -0.20629 | 0.66418 | 0.86640 | 267.88 |
| 325 | 4.9416 | -40.000 | 20.709 | -0.13615 | 0.68733 | 0.88653 | 278.24 |
| 350 | 4.5770 | -22.417 | 43.128 | -0.06970 | 0.70992 | 0.90702 | 288.11 |
| 375 | 4.2638 | -4.3028 | 66.057 | -0.00643 | 0.73165 | 0.92723 | 297.58 |
| 400 | 3.9916 | 14.326 | 89.485 | 0.05404 | 0.75242 | 0.94687 | 306.70 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 0.30 MPa Isobar | | | | | | | |
| 425 | 3.7526 | 33.450 | 113.40 | 0.11202 | 0.77222 | 0.96580 | 315.52 |
| 450 | 3.5410 | 53.048 | 137.77 | 0.16774 | 0.79107 | 0.98397 | 324.06 |
| 475 | 3.3523 | 73.097 | 162.59 | 0.22141 | 0.80902 | 1.0014 | 332.36 |
| 500 | 3.1829 | 93.578 | 187.83 | 0.27320 | 0.82612 | 1.0180 | 340.43 |
| 525 | 3.0299 | 114.47 | 213.48 | 0.32326 | 0.84242 | 1.0340 | 348.30 |
| 550 | 2.8911 | 135.76 | 239.53 | 0.37172 | 0.85797 | 1.0492 | 355.98 |
| 575 | 2.7646 | 157.42 | 265.94 | 0.41868 | 0.87282 | 1.0638 | 363.49 |
| 600 | 2.6487 | 179.45 | 292.71 | 0.46426 | 0.88699 | 1.0778 | 370.84 |
| 700 | 2.2687 | 270.84 | 403.07 | 0.63428 | 0.93770 | 1.1279 | 398.80 |
| 800 | 1.9844 | 366.84 | 518.02 | 0.78771 | 0.98009 | 1.1699 | 424.87 |
| 900 | 1.7635 | 466.72 | 636.83 | 0.92761 | 1.0156 | 1.2052 | 449.41 |
| 1000 | 1.5870 | 569.84 | 758.87 | 1.0562 | 1.0453 | 1.2347 | 472.69 |
| 1100 | 1.4426 | 675.67 | 883.63 | 1.1750 | 1.0703 | 1.2596 | 494.88 |
| 0.50 MPa Isobar | | | | | | | |
| 216.075 ^a | 13.282 | 114.05 | 76.405 | -0.59404 | 0.62692 | 0.90323 | 222.86 |
| 220 | 12.974 | -111.42 | -72.876 | -0.57785 | 0.62625 | 0.89522 | 225.33 |
| 230 | 12.265 | -104.78 | -64.010 | -0.53843 | 0.62547 | 0.87913 | 231.38 |
| 240 | 11.646 | -98.202 | -55.270 | -0.50124 | 0.62750 | 0.86991 | 237.06 |
| 250 | 11.097 | -91.650 | -46.594 | -0.46582 | 0.63186 | 0.86583 | 242.44 |
| 260 | 10.606 | -85.086 | -37.941 | -0.43188 | 0.63782 | 0.86526 | 247.58 |
| 270 | 10.161 | -78.487 | -29.281 | -0.39920 | 0.64484 | 0.86710 | 252.51 |
| 280 | 9.7568 | -71.840 | -20.594 | -0.36761 | 0.65255 | 0.87063 | 257.27 |
| 290 | 9.3864 | -65.133 | -11.865 | -0.33697 | 0.66071 | 0.87537 | 261.87 |
| 300 | 9.0456 | -58.359 | -3.0836 | -0.30721 | 0.66916 | 0.88096 | 266.35 |
| 325 | 8.2996 | -41.105 | 19.139 | -0.23606 | 0.69081 | 0.89726 | 277.05 |
| 350 | 7.6736 | -23.365 | 41.793 | -0.16892 | 0.71244 | 0.91523 | 287.18 |
| 375 | 7.1393 | -5.1305 | 64.905 | -0.10514 | 0.73353 | 0.93370 | 296.85 |
| 400 | 6.6770 | 13.593 | 88.478 | -0.04430 | 0.75386 | 0.95209 | 306.13 |
| 425 | 6.2725 | 32.793 | 112.51 | 0.01397 | 0.77335 | 0.97010 | 315.07 |
| 450 | 5.9154 | 52.453 | 136.98 | 0.06991 | 0.79197 | 0.98757 | 323.72 |
| 475 | 5.5975 | 72.554 | 161.88 | 0.12376 | 0.80975 | 1.0044 | 332.10 |
| 500 | 5.3126 | 93.079 | 187.19 | 0.17570 | 0.82672 | 1.0207 | 340.25 |
| 525 | 5.0558 | 114.01 | 212.91 | 0.22588 | 0.84292 | 1.0363 | 348.18 |
| 550 | 4.8229 | 135.33 | 239.00 | 0.27443 | 0.85840 | 1.0512 | 355.91 |
| 575 | 4.6108 | 157.02 | 265.46 | 0.32148 | 0.87318 | 1.0656 | 363.47 |
| 600 | 4.4168 | 179.07 | 292.28 | 0.36713 | 0.88731 | 1.0794 | 370.85 |
| 700 | 3.7814 | 270.54 | 402.76 | 0.53734 | 0.93789 | 1.1289 | 398.92 |
| 800 | 3.3067 | 366.60 | 517.81 | 0.69090 | 0.98022 | 1.1707 | 425.06 |
| 900 | 2.9383 | 466.51 | 636.68 | 0.83087 | 1.0157 | 1.2057 | 449.64 |
| 1000 | 2.6439 | 569.65 | 758.77 | 0.95947 | 1.0453 | 1.2352 | 472.94 |
| 1100 | 2.4033 | 675.51 | 883.56 | 1.0784 | 1.0703 | 1.2600 | 495.15 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 0.75 MPa Isobar | | | | | | | |
| 216.642 ^b | 1178.77 | -427.22 | -426.58 | -2.2178 | 0.97489 | 1.9518 | 976.77 |
| 220 | 1166.48 | -420.66 | -420.01 | -2.1878 | 0.97002 | 1.9607 | 952.10 |
| 225 | 1147.71 | -410.82 | -410.17 | -2.1435 | 0.96306 | 1.9772 | 915.26 |
| 225.505 ^b | 1145.78 | -409.83 | -409.17 | -2.1391 | 0.96238 | 1.9792 | 911.52 |
| 225.505 ^c | 19.640 | -111.58 | -73.389 | -0.65006 | 0.65557 | 0.96925 | 223.51 |
| 230 | 19.095 | -108.34 | -69.068 | -0.63108 | 0.65297 | 0.95402 | 226.53 |
| 235 | 18.535 | -104.80 | -64.335 | -0.61073 | 0.65047 | 0.93952 | 229.79 |
| 240 | 18.018 | -101.29 | -59.668 | -0.59107 | 0.64888 | 0.92783 | 232.92 |
| 245 | 17.536 | -97.821 | -55.052 | -0.57204 | 0.64826 | 0.91866 | 235.94 |
| 250 | 17.087 | -94.371 | -50.477 | -0.55356 | 0.64852 | 0.91161 | 238.87 |
| 255 | 16.665 | -90.937 | -45.933 | -0.53556 | 0.64951 | 0.90630 | 241.70 |
| 260 | 16.269 | -87.513 | -41.412 | -0.51800 | 0.65110 | 0.90211 | 241.46 |
| 265 | 15.894 | -84.094 | -36.907 | -0.50084 | 0.65318 | 0.89969 | 247.14 |
| 270 | 15.540 | -80.676 | -32.414 | -0.48404 | 0.65565 | 0.89792 | 249.76 |
| 275 | 15.204 | -77.256 | -27.927 | -0.46757 | 0.65844 | 0.89696 | 252.32 |
| 280 | 14.884 | -73.831 | -23.443 | -0.45141 | 0.66150 | 0.89665 | 254.83 |
| 285 | 14.580 | -70.399 | -18.959 | -0.43554 | 0.66478 | 0.89691 | 257.29 |
| 290 | 14.290 | -66.957 | -14.473 | -0.41994 | 0.66824 | 0.89764 | 259.70 |
| 295 | 14.013 | -63.505 | -9.9821 | -0.40458 | 0.67184 | 0.89878 | 262.07 |
| 300 | 13.747 | -60.041 | -5.4847 | -0.38947 | 0.67556 | 0.90026 | 264.41 |
| 305 | 13.493 | -56.564 | -0.97908 | -0.37457 | 0.67937 | 0.90202 | 266.70 |
| 310 | 13.249 | -53.072 | 3.5360 | -0.35989 | 0.68326 | 0.90404 | 268.96 |
| 315 | 13.015 | -49.566 | 8.0617 | -0.34540 | 0.68720 | 0.90627 | 271.19 |
| 320 | 12.789 | -46.044 | 12.599 | -0.33111 | 0.69120 | 0.90868 | 273.39 |
| 325 | 12.572 | -42.507 | 17.149 | -0.31701 | 0.69523 | 0.91126 | 275.56 |
| 330 | 12.363 | -38.952 | 21.712 | -0.30307 | 0.69928 | 0.91397 | 277.70 |
| 335 | 12.162 | -35.381 | 26.289 | -0.28931 | 0.70336 | 0.91680 | 279.82 |
| 340 | 11.967 | -31.793 | 30.880 | -0.27570 | 0.70744 | 0.91973 | 281.91 |
| 345 | 11.779 | -28.187 | 35.486 | -0.26225 | 0.71154 | 0.92274 | 283.98 |
| 350 | 11.597 | -24.563 | 40.107 | -0.24896 | 0.71562 | 0.92583 | 286.02 |
| 360 | 11.251 | -17.262 | 49.397 | -0.22279 | 0.72378 | 0.93217 | 290.05 |
| 370 | 10.927 | -9.8882 | 58.751 | -0.19716 | 0.73188 | 0.93869 | 294.00 |
| 380 | 10.621 | -2.4415 | 68.171 | -0.17204 | 0.73991 | 0.94532 | 297.88 |
| 390 | 10.333 | 5.0782 | 77.658 | -0.14739 | 0.74784 | 0.95202 | 301.68 |
| 400 | 10.062 | 12.671 | 87.212 | -0.12321 | 0.75568 | 0.95875 | 305.42 |
| 410 | 9.8042 | 20.336 | 96.833 | -0.09945 | 0.76340 | 0.96549 | 309.11 |
| 420 | 9.5603 | 28.072 | 106.52 | -0.07610 | 0.77101 | 0.97221 | 312.73 |
| 430 | 9.3287 | 35.880 | 116.28 | -0.05315 | 0.77850 | 0.97890 | 316.31 |
| 440 | 9.1085 | 43.758 | 126.10 | -0.03057 | 0.78586 | 0.98554 | 319.83 |
| 450 | 8.8987 | 51.706 | 135.99 | -0.00835 | 0.79310 | 0.99212 | 323.30 |
| 460 | 8.6988 | 59.723 | 145.94 | 0.01353 | 0.80022 | 0.99864 | 326.73 |
| 470 | 8.5079 | 67.807 | 155.96 | 0.03508 | 0.80722 | 1.0051 | 330.12 |
| 480 | 8.3254 | 75.957 | 166.04 | 0.05631 | 0.81409 | 1.0115 | 333.46 |
| 490 | 8.1508 | 84.174 | 176.19 | 0.07723 | 0.82084 | 1.0178 | 336.76 |
| 500 | 7.9835 | 92.455 | 186.40 | 0.09785 | 0.82748 | 1.0240 | 340.03 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 0.75 MPa Isobar | | | | | | | |
| 525 | 7.5946 | 113.43 | 212.19 | 0.14818 | 0.84355 | 1.0391 | 348.03 |
| 550 | 7.2425 | 134.79 | 238.35 | 0.19686 | 0.85893 | 1.0537 | 355.83 |
| 575 | 6.9222 | 156.52 | 264.87 | 0.24401 | 0.87363 | 1.0678 | 363.44 |
| 600 | 6.6294 | 178.60 | 291.74 | 0.28974 | 0.88769 | 1.0813 | 370.87 |
| 625 | 6.3608 | 201.02 | 318.93 | 0.33415 | 0.90115 | 1.0943 | 378.14 |
| 650 | 6.1133 | 223.76 | 346.45 | 0.37732 | 0.91402 | 1.1068 | 385.26 |
| 675 | 5.8846 | 246.82 | 374.27 | 0.41931 | 0.92634 | 1.1188 | 392.23 |
| 700 | 5.6725 | 270.16 | 402.38 | 0.46021 | 0.93812 | 1.1302 | 399.08 |
| 800 | 4.9589 | 366.29 | 517.53 | 0.61391 | 0.98037 | 1.1716 | 425.30 |
| 900 | 4.4056 | 466.25 | 636.49 | 0.75398 | 1.0158 | 1.2064 | 449.93 |
| 1000 | 3.9639 | 569.43 | 758.63 | 0.88265 | 1.0454 | 1.2357 | 473.27 |
| 1100 | 3.6030 | 675.32 | 883.47 | 1.0016 | 1.0704 | 1.2604 | 495.50 |
| 1.00 MPa Isobar | | | | | | | |
| 216.695 ^b | 1179.10 | -427.26 | -426.41 | -2.2180 | 0.97514 | 1.9503 | 977.76 |
| 220 | 1167.03 | -420.80 | -419.95 | -2.1884 | 0.97034 | 1.9589 | 953.55 |
| 225 | 1148.32 | -410.99 | -410.11 | -2.1442 | 0.96337 | 1.9751 | 916.83 |
| 230 | 1128.97 | -401.08 | -400.19 | -2.1006 | 0.95680 | 1.9959 | 879.82 |
| 233.028 ^c | 1116.90 | -395.02 | -394.12 | -2.0744 | 0.95303 | 2.0111 | 857.18 |
| 233.028 ^d | 26.006 | -109.94 | -71.484 | -0.68986 | 0.68026 | 1.0322 | 223.50 |
| 235 | 25.665 | -108.42 | -69.459 | -0.68120 | 0.67819 | 1.0220 | 224.93 |
| 240 | 24.857 | -104.64 | -64.408 | -0.65993 | 0.67332 | 0.99915 | 228.46 |
| 245 | 24.117 | -100.92 | -59.460 | -0.63953 | 0.66959 | 0.98058 | 231.84 |
| 250 | 23.435 | -97.266 | -54.595 | -0.61987 | 0.66716 | 0.96579 | 235.08 |
| 255 | 22.803 | -93.650 | -49.797 | -0.60087 | 0.66588 | 0.95411 | 238.19 |
| 260 | 22.215 | -90.065 | -45.050 | -0.58243 | 0.66557 | 0.94495 | 241.19 |
| 265 | 21.664 | -86.503 | -40.344 | -0.56450 | 0.66605 | 0.93783 | 244.10 |
| 270 | 21.147 | -82.957 | -35.669 | -0.54703 | 0.66718 | 0.93235 | 246.91 |
| 275 | 20.660 | -79.422 | -31.018 | -0.52996 | 0.66884 | 0.92821 | 249.66 |
| 280 | 20.199 | -75.892 | -26.385 | -0.51326 | 0.67092 | 0.92518 | 252.33 |
| 285 | 19.763 | -72.364 | -21.765 | -0.49691 | 0.67335 | 0.92307 | 254.93 |
| 290 | 19.349 | -68.836 | -17.153 | -0.48087 | 0.67607 | 0.92172 | 257.49 |
| 295 | 18.955 | -65.303 | -12.547 | -0.46512 | 0.67902 | 0.92103 | 259.98 |
| 300 | 18.579 | -61.765 | -7.9420 | -0.44964 | 0.68217 | 0.92089 | 262.43 |
| 305 | 18.221 | -58.220 | -3.3370 | -0.43442 | 0.68547 | 0.92121 | 264.83 |
| 310 | 17.878 | -54.665 | 1.2707 | -0.41943 | 0.68890 | 0.92192 | 267.20 |
| 315 | 17.549 | -51.100 | 5.8828 | -0.40467 | 0.69243 | 0.92298 | 269.52 |
| 320 | 17.234 | -47.523 | 10.501 | -0.39013 | 0.69605 | 0.92433 | 271.80 |
| 325 | 16.932 | -43.934 | 15.126 | -0.37578 | 0.69974 | 0.92594 | 274.06 |
| 330 | 16.641 | -40.331 | 19.761 | -0.36163 | 0.70349 | 0.92777 | 276.28 |
| 335 | 16.361 | -36.715 | 24.405 | -0.34767 | 0.70729 | 0.92981 | 278.46 |
| 340 | 16.092 | -33.084 | 29.059 | -0.33387 | 0.71112 | 0.93200 | 280.62 |
| 345 | 15.832 | -29.438 | 33.725 | -0.32025 | 0.71498 | 0.93435 | 282.76 |
| 350 | 15.581 | -25.777 | 38.403 | -0.30679 | 0.71885 | 0.93681 | 284.86 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | <i>c_v</i> [kJ/(kg K)] | <i>c_p</i> [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|-------------------------------------|-------------------------------------|-------------------------|
| 1.00 MPa Isobar | | | | | | | |
| 360 | 15.105 | -18.406 | 47.797 | -0.28033 | 0.72664 | 0.94206 | 289.00 |
| 370 | 14.659 | -10.970 | 57.245 | -0.25444 | 0.73442 | 0.94763 | 293.05 |
| 380 | 14.241 | -3.4677 | 66.750 | -0.22909 | 0.74217 | 0.95345 | 297.02 |
| 390 | 13.848 | 4.1027 | 76.315 | -0.20425 | 0.74988 | 0.95944 | 300.91 |
| 400 | 13.477 | 11.741 | 85.939 | -0.17988 | 0.75751 | 0.96555 | 304.72 |
| 410 | 13.127 | 19.449 | 95.626 | -0.15596 | 0.76505 | 0.97174 | 308.47 |
| 420 | 12.796 | 27.224 | 105.37 | -0.13247 | 0.77251 | 0.97798 | 312.16 |
| 430 | 12.482 | 35.068 | 115.19 | -0.10939 | 0.77986 | 0.98423 | 315.79 |
| 440 | 12.183 | 42.979 | 125.06 | -0.08669 | 0.78710 | 0.99049 | 319.37 |
| 450 | 11.899 | 50.957 | 135.00 | -0.06436 | 0.79424 | 0.99673 | 322.89 |
| 460 | 11.629 | 59.001 | 144.99 | -0.04238 | 0.80126 | 1.0029 | 326.37 |
| 470 | 11.371 | 67.112 | 155.05 | -0.02075 | 0.80817 | 1.0091 | 329.79 |
| 480 | 11.125 | 75.287 | 165.18 | 0.00056 | 0.81497 | 1.0152 | 333.18 |
| 490 | 10.889 | 83.526 | 175.36 | 0.02156 | 0.82166 | 1.0213 | 336.52 |
| 500 | 10.664 | 91.829 | 185.60 | 0.04225 | 0.82823 | 1.0273 | 339.81 |
| 525 | 10.141 | 112.86 | 211.47 | 0.09273 | 0.84418 | 1.0420 | 347.90 |
| 550 | 9.6675 | 134.26 | 237.70 | 0.14154 | 0.85946 | 1.0563 | 355.76 |
| 575 | 9.2375 | 156.02 | 264.28 | 0.18879 | 0.87408 | 1.0700 | 363.42 |
| 600 | 8.8449 | 178.14 | 291.19 | 0.23462 | 0.88808 | 1.0833 | 370.90 |
| 625 | 8.4849 | 200.58 | 318.44 | 0.27910 | 0.90149 | 1.0961 | 378.20 |
| 650 | 8.1535 | 223.35 | 345.99 | 0.32233 | 0.91432 | 1.1084 | 385.36 |
| 675 | 7.8474 | 246.42 | 373.85 | 0.36438 | 0.92660 | 1.1202 | 392.37 |
| 700 | 7.5638 | 269.79 | 402.00 | 0.40533 | 0.93835 | 1.1315 | 399.24 |
| 800 | 6.6102 | 365.98 | 517.26 | 0.55918 | 0.98053 | 1.1725 | 425.54 |
| 900 | 5.8718 | 465.99 | 636.29 | 0.69934 | 1.0159 | 1.2071 | 450.22 |
| 1000 | 5.2826 | 569.20 | 758.50 | 0.82807 | 1.0455 | 1.2362 | 473.59 |
| 1100 | 4.8014 | 675.12 | 883.39 | 0.94708 | 1.0704 | 1.2608 | 495.84 |
| 2.00 MPa Isobar | | | | | | | |
| 216.908 ^b | 1180.41 | -427.40 | -425.70 | -2.2187 | 0.97612 | 1.9443 | 981.71 |
| 220 | 1169.23 | -421.39 | -419.68 | -2.1911 | 0.97160 | 1.9517 | 959.33 |
| 225 | 1150.73 | -411.63 | -409.89 | -2.1471 | 0.96458 | 1.9667 | 923.07 |
| 230 | 1131.64 | -401.78 | -400.01 | -2.1037 | 0.95796 | 1.9858 | 886.59 |
| 235 | 1111.85 | -391.82 | -390.02 | -2.0607 | 0.95178 | 2.0100 | 849.70 |
| 240 | 1091.24 | -381.73 | -379.90 | -2.0181 | 0.94610 | 2.0404 | 812.17 |
| 245 | 1069.65 | -371.47 | -369.60 | -1.9756 | 0.94098 | 2.0786 | 773.73 |
| 250 | 1046.88 | -361.01 | -359.10 | -1.9332 | 0.93660 | 2.1271 | 733.93 |
| 253.647 ^c | 1029.36 | -353.20 | -351.26 | -1.9021 | 0.93409 | 2.1710 | 703.64 |
| 253.647 ^c | 52.540 | -107.99 | -69.929 | -0.79292 | 0.76254 | 1.2983 | 220.27 |
| 255 | 51.941 | -106.69 | -68.187 | -0.78607 | 0.75793 | 1.2773 | 221.55 |
| 260 | 49.914 | -102.04 | -61.969 | -0.76192 | 0.74331 | 1.2130 | 226.07 |
| 265 | 48.129 | -97.586 | -56.031 | -0.73930 | 0.73233 | 1.1646 | 230.27 |
| 270 | 46.533 | -93.285 | -50.304 | -0.71789 | 0.72439 | 1.1276 | 234.21 |
| 275 | 45.090 | -89.098 | -44.742 | -0.69748 | 0.71881 | 1.0987 | 237.93 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|--------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 2.00 MPa Isobar | | | | | | | |
| 280 | 43.772 | -84.999 | -39.308 | -0.67789 | 0.71503 | 1.0758 | 241.45 |
| 285 | 42.560 | -80.969 | -33.977 | -0.65902 | 0.71265 | 1.0574 | 244.82 |
| 290 | 41.438 | -76.992 | -28.728 | -0.64076 | 0.71135 | 1.0425 | 248.05 |
| 295 | 40.395 | -73.058 | -23.547 | -0.62305 | 0.71092 | 1.0305 | 251.15 |
| 300 | 39.420 | -69.155 | -18.420 | -0.60581 | 0.71116 | 1.0206 | 254.15 |
| 305 | 38.506 | -65.278 | -13.338 | -0.58901 | 0.71195 | 1.0125 | 257.06 |
| 310 | 37.645 | -61.420 | -8.2920 | -0.57260 | 0.71317 | 1.0059 | 259.89 |
| 315 | 36.832 | -57.577 | -3.2763 | -0.55655 | 0.71475 | 1.0005 | 262.63 |
| 320 | 36.063 | -53.744 | 1.7152 | -0.54083 | 0.71664 | 0.99621 | 265.31 |
| 325 | 35.333 | -49.917 | 6.6872 | -0.52541 | 0.71879 | 0.99276 | 267.93 |
| 330 | 34.639 | -46.095 | 11.644 | -0.51028 | 0.72117 | 0.99008 | 270.49 |
| 335 | 33.977 | -42.273 | 16.589 | -0.49541 | 0.72373 | 0.98805 | 272.99 |
| 340 | 33.346 | -38.451 | 21.526 | -0.48078 | 0.72645 | 0.98659 | 275.45 |
| 345 | 32.743 | -34.627 | 26.456 | -0.46638 | 0.72929 | 0.98561 | 277.85 |
| 350 | 32.165 | -30.798 | 31.382 | -0.45221 | 0.73225 | 0.98506 | 280.22 |
| 360 | 31.078 | -23.121 | 41.232 | -0.42446 | 0.73841 | 0.98503 | 284.83 |
| 370 | 30.075 | -15.414 | 51.087 | -0.39746 | 0.74484 | 0.98616 | 289.30 |
| 380 | 29.143 | -7.6685 | 60.958 | -0.37113 | 0.75144 | 0.98819 | 293.64 |
| 390 | 28.276 | 0.12033 | 70.853 | -0.34543 | 0.75815 | 0.99093 | 297.87 |
| 400 | 27.161 | 7.9565 | 80.778 | -0.32030 | 0.76194 | 0.99423 | 301.99 |
| 410 | 26.704 | 15.843 | 90.739 | -0.29571 | 0.77175 | 0.99798 | 306.02 |
| 420 | 25.989 | 23.782 | 100.74 | -0.27161 | 0.77856 | 1.0021 | 309.96 |
| 430 | 25.314 | 31.775 | 110.78 | -0.24798 | 0.78535 | 1.0064 | 313.83 |
| 440 | 24.678 | 39.824 | 120.87 | -0.22479 | 0.79211 | 1.0110 | 317.61 |
| 450 | 24.075 | 47.929 | 131.00 | -0.20202 | 0.79881 | 1.0158 | 321.33 |
| 460 | 23.504 | 56.091 | 141.18 | -0.17964 | 0.80545 | 1.0207 | 324.99 |
| 470 | 22.961 | 64.310 | 151.42 | -0.15763 | 0.81202 | 1.0256 | 328.58 |
| 480 | 22.444 | 72.587 | 161.70 | -0.13599 | 0.81852 | 1.0307 | 332.12 |
| 490 | 21.952 | 80.920 | 172.03 | -0.11468 | 0.82493 | 1.0358 | 335.60 |
| 500 | 21.482 | 89.311 | 182.41 | -0.09371 | 0.83126 | 1.0409 | 339.03 |
| 525 | 20.396 | 110.54 | 208.59 | -0.04261 | 0.84670 | 1.0537 | 347.41 |
| 550 | 19.419 | 132.11 | 235.10 | 0.00670 | 0.86158 | 1.0664 | 355.52 |
| 575 | 18.536 | 154.02 | 261.91 | 0.05438 | 0.87589 | 1.0790 | 363.39 |
| 600 | 17.733 | 176.26 | 289.04 | 0.10056 | 0.88964 | 1.0912 | 371.05 |
| 625 | 16.999 | 198.82 | 316.47 | 0.14535 | 0.90284 | 1.1031 | 378.52 |
| 650 | 16.325 | 221.69 | 344.20 | 0.18884 | 0.91550 | 1.1147 | 385.81 |
| 675 | 15.705 | 244.85 | 372.20 | 0.23112 | 0.92764 | 1.1259 | 392.94 |
| 700 | 15.130 | 268.30 | 400.49 | 0.27227 | 0.93928 | 1.1367 | 399.92 |
| 800 | 13.207 | 364.75 | 516.19 | 0.42670 | 0.98114 | 1.1762 | 426.52 |
| 900 | 11.724 | 464.95 | 635.54 | 0.56724 | 1.0163 | 1.2099 | 451.40 |
| 1000 | 10.544 | 568.30 | 757.99 | 0.69622 | 1.0459 | 1.2384 | 474.89 |
| 1100 | 9.5815 | 674.33 | 883.06 | 0.81542 | 1.0707 | 1.2625 | 497.22 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 3.00 MPa Isobar | | | | | | | |
| 217.121 ^b | 1181.71 | -427.54 | -425.00 | -2.2193 | 0.97705 | 1.9386 | 985.63 |
| 220 | 1171.40 | -421.97 | -419.41 | -2.1938 | 0.97282 | 1.9449 | 965.03 |
| 225 | 1153.10 | -412.25 | -409.65 | -2.1499 | 0.96576 | 1.9587 | 929.22 |
| 230 | 1134.25 | -402.46 | -399.82 | -2.1067 | 0.95909 | 1.9763 | 893.25 |
| 235 | 1114.74 | -392.57 | -389.88 | -2.0639 | 0.95286 | 1.9986 | 856.93 |
| 240 | 1094.46 | -382.56 | -379.82 | -2.0216 | 0.94711 | 2.0265 | 820.08 |
| 245 | 1073.29 | -372.40 | -369.61 | -1.9795 | 0.94190 | 2.0613 | 782.45 |
| 250 | 1051.02 | -362.05 | -359.19 | -1.9374 | 0.93737 | 2.1051 | 743.69 |
| 255 | 1027.42 | -351.46 | -348.54 | -1.8952 | 0.93383 | 2.1608 | 703.23 |
| 260 | 1002.13 | -340.55 | -337.56 | -1.8526 | 0.93209 | 2.2331 | 660.22 |
| 265 | 974.65 | -329.24 | -326.16 | -1.8091 | 0.93362 | 2.3306 | 613.45 |
| 267.598 ^c | 959.25 | -323.15 | -320.03 | -1.7861 | 0.93647 | 2.3959 | 587.14 |
| 267.598 ^c | 81.919 | -109.79 | -73.169 | -0.86360 | 0.83693 | 1.6438 | 214.95 |
| 270 | 79.807 | -106.92 | -69.327 | -0.84931 | 0.82029 | 1.5582 | 217.92 |
| 275 | 76.011 | -101.35 | -61.879 | -0.82197 | 0.79485 | 1.4301 | 223.53 |
| 280 | 72.805 | -96.166 | -54.960 | -0.79703 | 0.77747 | 1.3423 | 228.55 |
| 285 | 70.025 | -91.258 | -48.416 | -0.77387 | 0.76520 | 1.2784 | 233.14 |
| 290 | 67.568 | -86.550 | -42.151 | -0.75207 | 0.75645 | 1.2300 | 237.39 |
| 295 | 65.368 | -81.993 | -36.099 | -0.73138 | 0.75024 | 1.1923 | 241.37 |
| 300 | 63.376 | -77.552 | -30.215 | -0.71160 | 0.74589 | 1.1623 | 245.13 |
| 305 | 61.556 | -73.203 | -24.466 | -0.69260 | 0.74293 | 1.1380 | 248.70 |
| 310 | 59.881 | -68.927 | -18.827 | -0.67426 | 0.74101 | 1.1181 | 252.12 |
| 315 | 58.332 | -64.710 | -13.280 | -0.65650 | 0.73994 | 1.1016 | 255.40 |
| 320 | 56.890 | -60.540 | -7.8071 | -0.63927 | 0.73955 | 1.0878 | 258.56 |
| 325 | 55.544 | -56.409 | -2.3975 | -0.62249 | 0.73974 | 1.0763 | 261.61 |
| 330 | 54.281 | -52.309 | 2.9594 | -0.60614 | 0.74041 | 1.0667 | 264.56 |
| 335 | 53.092 | -48.233 | 8.2721 | -0.59016 | 0.74148 | 1.0586 | 267.43 |
| 340 | 51.970 | -44.178 | 13.548 | -0.57453 | 0.74287 | 1.0518 | 270.21 |
| 345 | 50.908 | -40.137 | 18.792 | -0.55921 | 0.74453 | 1.0462 | 272.93 |
| 350 | 49.901 | -36.108 | 24.011 | -0.54419 | 0.74643 | 1.0414 | 275.58 |
| 360 | 48.031 | -28.073 | 34.387 | -0.51496 | 0.75077 | 1.0343 | 280.71 |
| 370 | 46.327 | -20.052 | 44.705 | -0.48669 | 0.75568 | 1.0296 | 285.63 |
| 380 | 44.765 | -12.030 | 54.986 | -0.45928 | 0.76102 | 1.0269 | 290.37 |
| 390 | 43.326 | -3.9958 | 65.247 | -0.43262 | 0.76667 | 1.0256 | 294.95 |
| 400 | 41.992 | 4.0597 | 75.502 | -0.40666 | 0.77255 | 1.0255 | 299.39 |
| 410 | 40.752 | 12.143 | 85.760 | -0.38133 | 0.77858 | 1.0263 | 303.70 |
| 420 | 39.594 | 20.261 | 96.030 | -0.35658 | 0.78472 | 1.0279 | 307.90 |
| 430 | 38.509 | 28.416 | 106.32 | -0.33237 | 0.79093 | 1.0301 | 312.00 |
| 440 | 37.491 | 36.613 | 116.63 | -0.30866 | 0.79717 | 1.0327 | 316.00 |
| 450 | 36.531 | 44.854 | 126.98 | -0.28542 | 0.80343 | 1.0358 | 319.91 |
| 460 | 35.625 | 53.141 | 137.35 | -0.26261 | 0.80967 | 1.0392 | 323.74 |
| 470 | 34.768 | 61.475 | 147.76 | -0.24023 | 0.81589 | 1.0428 | 327.50 |
| 480 | 33.956 | 69.858 | 158.21 | -0.21823 | 0.82207 | 1.0467 | 331.19 |
| 490 | 33.185 | 78.291 | 168.69 | -0.19661 | 0.82821 | 1.0507 | 334.81 |
| 500 | 32.451 | 86.774 | 179.22 | 0.17534 | 0.83429 | 1.0549 | 338.37 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 3.00 MPa Isobar | | | | | | | |
| 525 | 30.761 | 108.20 | 205.73 | -0.12361 | 0.84921 | 1.0656 | 347.04 |
| 550 | 29.252 | 129.95 | 232.51 | -0.07378 | 0.86369 | 1.0768 | 355.39 |
| 575 | 27.893 | 152.01 | 259.57 | -0.02567 | 0.87769 | 1.0880 | 363.46 |
| 600 | 26.661 | 174.38 | 286.91 | 0.02087 | 0.89118 | 1.0992 | 371.30 |
| 625 | 25.540 | 197.06 | 314.53 | 0.06597 | 0.90418 | 1.1102 | 378.92 |
| 650 | 24.513 | 220.03 | 342.42 | 0.10972 | 0.91667 | 1.1211 | 386.34 |
| 675 | 23.569 | 243.29 | 370.58 | 0.15223 | 0.92868 | 1.1316 | 393.58 |
| 700 | 22.697 | 266.82 | 399.00 | 0.19357 | 0.94020 | 1.1419 | 400.65 |
| 800 | 19.789 | 363.53 | 515.13 | 0.34859 | 0.98175 | 1.1799 | 427.55 |
| 900 | 17.556 | 463.91 | 634.79 | 0.48950 | 1.0168 | 1.2126 | 452.61 |
| 1000 | 15.783 | 567.41 | 757.48 | 0.61874 | 1.0462 | 1.2405 | 476.21 |
| 1100 | 14.340 | 673.54 | 882.75 | 0.73811 | 1.0710 | 1.2642 | 498.61 |
| 4.00 MPa Isobar | | | | | | | |
| 217.334 ^b | 1182.98 | -427.67 | -424.29 | -2.2200 | 0.97796 | 1.9330 | 989.53 |
| 220 | 1173.53 | -422.54 | -419.13 | -2.1964 | 0.97402 | 1.9384 | 970.66 |
| 225 | 1155.43 | -412.87 | -409.41 | -2.1527 | 0.96691 | 1.9510 | 935.29 |
| 230 | 1136.80 | -403.13 | -399.62 | -2.1096 | 0.96020 | 1.9673 | 899.79 |
| 235 | 1117.56 | -393.31 | -389.73 | -2.0671 | 0.95391 | 1.9878 | 864.02 |
| 240 | 1097.60 | -383.37 | -379.73 | -2.0250 | 0.94810 | 2.0134 | 827.80 |
| 245 | 1076.81 | -373.30 | -369.59 | -1.9832 | 0.94281 | 2.0452 | 790.92 |
| 250 | 1055.01 | -363.06 | -359.26 | -1.9415 | 0.93814 | 2.0849 | 753.10 |
| 255 | 1032.00 | -352.60 | -348.72 | -1.8997 | 0.93435 | 2.1348 | 713.89 |
| 260 | 1007.49 | -341.86 | -337.89 | -1.8577 | 0.93199 | 2.1986 | 672.67 |
| 265 | 981.06 | -330.78 | -326.70 | -1.8150 | 0.93201 | 2.2823 | 628.62 |
| 270 | 952.10 | -319.22 | -315.02 | -1.7714 | 0.93573 | 2.3972 | 580.72 |
| 275 | 919.56 | -306.99 | -302.64 | -1.7259 | 0.94504 | 2.5660 | 527.52 |
| 278.450 ^c | 894.05 | -297.98 | -293.51 | -1.6929 | 0.95655 | 2.7401 | 486.42 |
| 278.450 ^c | 115.74 | -114.09 | -79.534 | -0.92449 | 0.91069 | 2.1642 | 208.78 |
| 280 | 113.08 | -111.66 | -76.288 | -0.91286 | 0.89131 | 2.0294 | 211.36 |
| 285 | 106.02 | -104.65 | -66.920 | -0.87969 | 0.84827 | 1.7461 | 218.60 |
| 290 | 100.47 | -98.453 | -58.641 | -0.85089 | 0.82129 | 1.5780 | 224.72 |
| 295 | 95.884 | -92.766 | -51.048 | -0.82493 | 0.80299 | 1.4657 | 230.14 |
| 300 | 91.965 | -87.427 | -43.932 | -0.80101 | 0.79011 | 1.3850 | 235.04 |
| 305 | 88.543 | -82.340 | -37.165 | -0.77864 | 0.78082 | 1.3244 | 239.56 |
| 310 | 85.508 | -77.445 | -30.665 | -0.75750 | 0.77402 | 1.2773 | 243.77 |
| 315 | 82.781 | -72.697 | -24.376 | -0.73737 | 0.76906 | 1.2397 | 247.73 |
| 320 | 80.306 | -68.066 | -18.256 | -0.71809 | 0.76551 | 1.2092 | 251.49 |
| 325 | 78.043 | -63.529 | -12.275 | -0.69955 | 0.76308 | 1.1842 | 255.07 |
| 330 | 75.958 | -59.068 | -6.4078 | -0.68163 | 0.76156 | 1.1633 | 258.49 |
| 335 | 74.028 | -54.670 | -0.63601 | -0.66427 | 0.76076 | 1.1459 | 261.78 |
| 340 | 72.231 | -50.322 | 5.0556 | -0.64741 | 0.76054 | 1.1312 | 264.95 |
| 345 | 70.552 | -46.017 | 10.679 | -0.63099 | 0.76080 | 1.1187 | 268.01 |
| 350 | 68.976 | -41.746 | 16.245 | -0.61497 | 0.76145 | 1.1080 | 270.98 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 4.00 MPa Isobar | | | | | | | |
| 360 | 66.092 | -33.284 | 27.237 | -0.58400 | 0.76371 | 1.0912 | 276.67 |
| 370 | 63.509 | -24.899 | 38.084 | -0.55428 | 0.76695 | 1.0789 | 282.06 |
| 380 | 61.173 | -16.562 | 48.826 | -0.52564 | 0.77091 | 1.0700 | 287.22 |
| 390 | 59.045 | -8.2521 | 59.493 | -0.49793 | 0.77542 | 1.0637 | 292.17 |
| 400 | 57.094 | 0.04711 | 70.107 | -0.47105 | 0.78032 | 1.0595 | 296.93 |
| 410 | 55.294 | 8.3478 | 80.688 | -0.44493 | 0.78553 | 1.0569 | 301.53 |
| 420 | 53.627 | 16.660 | 91.249 | -0.41948 | 0.79097 | 1.0555 | 305.99 |
| 430 | 52.076 | 24.990 | 101.80 | -0.39465 | 0.79657 | 1.0552 | 310.31 |
| 440 | 50.628 | 33.346 | 112.35 | -0.37039 | 0.80228 | 1.0556 | 314.52 |
| 450 | 49.270 | 41.732 | 122.92 | -0.34665 | 0.80808 | 1.0568 | 318.63 |
| 460 | 47.995 | 50.151 | 133.49 | -0.32341 | 0.81391 | 1.0585 | 322.64 |
| 470 | 46.794 | 58.607 | 144.09 | -0.30062 | 0.81978 | 1.0607 | 326.55 |
| 480 | 45.659 | 67.102 | 154.71 | -0.27826 | 0.82564 | 1.0633 | 330.39 |
| 490 | 44.585 | 75.638 | 165.35 | -0.25631 | 0.83150 | 1.0661 | 334.15 |
| 500 | 43.566 | 84.217 | 176.03 | -0.23474 | 0.83733 | 1.0692 | 337.84 |
| 525 | 41.233 | 105.86 | 202.87 | -0.18237 | 0.85173 | 1.0779 | 346.77 |
| 550 | 39.160 | 127.79 | 229.93 | -0.13201 | 0.86580 | 1.0873 | 355.36 |
| 575 | 37.302 | 150.00 | 257.24 | -0.08346 | 0.87948 | 1.0971 | 363.63 |
| 600 | 35.625 | 172.51 | 284.79 | -0.03655 | 0.89272 | 1.1072 | 371.63 |
| 625 | 34.103 | 195.30 | 312.60 | 0.00885 | 0.90551 | 1.1174 | 379.39 |
| 650 | 32.712 | 218.38 | 340.66 | 0.05287 | 0.91784 | 1.1274 | 386.93 |
| 675 | 31.437 | 241.73 | 368.97 | 0.09561 | 0.92971 | 1.1374 | 394.28 |
| 700 | 30.262 | 265.35 | 397.52 | 0.13715 | 0.94111 | 1.1471 | 401.45 |
| 800 | 26.355 | 362.32 | 514.09 | 0.29274 | 0.98236 | 1.1835 | 428.62 |
| 900 | 23.367 | 462.88 | 634.07 | 0.43402 | 1.0172 | 1.2153 | 453.84 |
| 1000 | 21.001 | 566.52 | 756.99 | 0.56351 | 1.0465 | 1.2425 | 477.55 |
| 1100 | 19.077 | 672.77 | 882.44 | 0.68306 | 1.0712 | 1.2658 | 500.01 |
| 5.00 MPa Isobar | | | | | | | |
| 217.546 ^b | 1184.25 | -427.80 | -423.58 | -2.2206 | 0.97883 | 1.9275 | 993.41 |
| 220 | 1175.62 | -423.10 | -418.85 | -2.1990 | 0.97518 | 1.9321 | 976.23 |
| 225 | 1157.72 | -413.48 | -409.16 | -2.1554 | 0.96803 | 1.9436 | 941.27 |
| 230 | 1139.31 | -403.79 | -399.41 | -2.1125 | 0.96127 | 1.9586 | 906.23 |
| 235 | 1120.32 | -394.03 | -389.57 | -2.0702 | 0.95493 | 1.9775 | 870.97 |
| 240 | 1100.66 | -384.17 | -379.62 | -2.0283 | 0.94906 | 2.0011 | 835.35 |
| 245 | 1080.22 | -374.18 | -369.55 | -1.9868 | 0.94369 | 2.0302 | 799.17 |
| 250 | 1058.86 | -364.03 | -359.31 | -1.9454 | 0.93891 | 2.0660 | 762.21 |
| 255 | 1036.39 | -353.69 | -348.87 | -1.9041 | 0.93492 | 2.1112 | 724.10 |
| 260 | 1012.57 | -343.12 | -338.18 | -1.8626 | 0.93209 | 2.1678 | 684.39 |
| 265 | 987.07 | -332.23 | -327.16 | -1.8206 | 0.93107 | 2.2407 | 642.50 |
| 270 | 959.39 | -320.94 | -315.73 | -1.7779 | 0.93262 | 2.3377 | 597.75 |
| 275 | 928.78 | -309.11 | -303.72 | -1.7338 | 0.93765 | 2.4735 | 549.26 |
| 280 | 893.90 | -296.47 | -290.88 | -1.6875 | 0.94778 | 2.6797 | 495.52 |
| 285 | 852.04 | -282.54 | -276.67 | -1.6373 | 0.96716 | 3.0437 | 433.50 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | <i>c_v</i> [kJ/(kg K)] | <i>c_p</i> [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|-------------------------------------|-------------------------------------|-------------------------|
| 5.00 MPa Isobar | | | | | | | |
| 287.434 ^c | 827.32 | -274.96 | -268.91 | -1.6101 | 0.98314 | 3.3572 | 398.39 |
| 287.434 ^c | 156.67 | -121.04 | -89.122 | -0.98464 | 0.99465 | 3.1142 | 201.86 |
| 290 | 148.41 | -115.58 | -81.892 | -0.95959 | 0.94334 | 2.5783 | 207.56 |
| 295 | 136.85 | -106.98 | -70.445 | -0.92044 | 0.88615 | 2.0671 | 216.24 |
| 300 | 128.40 | -99.772 | -60.830 | -0.88811 | 0.85258 | 1.8025 | 223.25 |
| 305 | 121.69 | -93.344 | -52.258 | -0.85977 | 0.83051 | 1.6378 | 229.28 |
| 310 | 116.13 | -87.423 | -44.367 | -0.83411 | 0.81508 | 1.5246 | 234.66 |
| 315 | 111.37 | -81.856 | -36.961 | -0.81041 | 0.80388 | 1.4418 | 239.55 |
| 320 | 107.22 | -76.552 | -29.917 | -0.78822 | 0.79562 | 1.3786 | 244.08 |
| 325 | 103.53 | -71.448 | -23.153 | -0.76724 | 0.78951 | 1.3289 | 248.32 |
| 330 | 100.22 | -66.502 | -16.612 | -0.74727 | 0.78505 | 1.2890 | 252.30 |
| 335 | 97.221 | -61.681 | -10.251 | -0.72814 | 0.78185 | 1.2564 | 256.08 |
| 340 | 94.478 | -56.961 | -4.0388 | -0.70973 | 0.77963 | 1.2294 | 259.68 |
| 345 | 91.955 | -52.325 | 2.0498 | -0.69195 | 0.77820 | 1.2067 | 263.13 |
| 350 | 89.619 | -47.757 | 8.0342 | -0.67473 | 0.77739 | 1.1875 | 266.45 |
| 360 | 85.418 | -38.785 | 19.750 | -0.64172 | 0.77727 | 1.1573 | 272.74 |
| 370 | 81.726 | -29.974 | 31.205 | -0.61034 | 0.77863 | 1.1349 | 278.64 |
| 380 | 78.440 | -21.276 | 42.467 | -0.58030 | 0.78109 | 1.1182 | 284.23 |
| 390 | 75.484 | -12.655 | 53.584 | -0.55142 | 0.78436 | 1.1058 | 289.55 |
| 400 | 72.804 | -4.0846 | 64.593 | -0.52355 | 0.78824 | 1.0965 | 294.63 |
| 410 | 70.355 | 4.4545 | 75.523 | -0.49656 | 0.79259 | 1.0898 | 299.52 |
| 420 | 68.104 | 12.978 | 86.396 | -0.47036 | 0.79729 | 1.0850 | 304.24 |
| 430 | 66.024 | 21.498 | 97.228 | -0.44487 | 0.80226 | 1.0818 | 308.79 |
| 440 | 64.094 | 30.024 | 108.03 | -0.42003 | 0.80743 | 1.0798 | 313.21 |
| 450 | 62.295 | 38.564 | 118.83 | -0.39578 | 0.81274 | 1.0788 | 317.50 |
| 460 | 60.613 | 47.123 | 129.61 | -0.37207 | 0.81817 | 1.0787 | 321.68 |
| 470 | 59.035 | 55.707 | 140.40 | -0.34886 | 0.82367 | 1.0792 | 325.75 |
| 480 | 57.550 | 64.320 | 151.20 | -0.32613 | 0.82921 | 1.0804 | 329.73 |
| 490 | 56.150 | 72.964 | 162.01 | -0.30384 | 0.83478 | 1.0820 | 333.62 |
| 500 | 54.826 | 81.644 | 172.84 | -0.28196 | 0.84035 | 1.0840 | 337.43 |
| 525 | 51.807 | 103.51 | 200.02 | -0.22893 | 0.85423 | 1.0903 | 346.63 |
| 550 | 49.140 | 125.62 | 227.37 | -0.17803 | 0.86790 | 1.0979 | 355.43 |
| 575 | 46.761 | 147.99 | 254.92 | -0.12904 | 0.88126 | 1.1064 | 363.88 |
| 600 | 44.621 | 170.64 | 282.69 | -0.08177 | 0.89425 | 1.1153 | 372.04 |
| 625 | 42.685 | 193.55 | 310.69 | -0.03605 | 0.90684 | 1.1245 | 379.93 |
| 650 | 40.921 | 216.73 | 338.92 | 0.00823 | 0.91900 | 1.1338 | 387.59 |
| 675 | 39.307 | 240.17 | 367.38 | 0.05120 | 0.93073 | 1.1431 | 395.04 |
| 700 | 37.823 | 263.87 | 396.07 | 0.09293 | 0.94202 | 1.1523 | 402.30 |
| 800 | 32.904 | 361.11 | 513.07 | 0.24911 | 0.98296 | 1.1871 | 429.72 |
| 900 | 29.156 | 461.86 | 633.35 | 0.39075 | 1.0176 | 1.2179 | 455.10 |
| 1000 | 26.196 | 565.64 | 756.51 | 0.52048 | 1.0469 | 1.2446 | 478.91 |
| 1100 | 23.793 | 671.99 | 882.14 | 0.64021 | 1.0715 | 1.2674 | 501.43 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 6.00 MPa Isobar | | | | | | | |
| 217.758 ^b | 1185.49 | -427.93 | -422.87 | -2.2212 | 0.97967 | 1.9222 | 997.26 |
| 220 | 1177.69 | -423.65 | -418.56 | -2.2015 | 0.97632 | 1.9260 | 981.74 |
| 225 | 1159.97 | -414.07 | -408.90 | -2.1581 | 0.96912 | 1.9366 | 947.17 |
| 230 | 1141.77 | -404.44 | -399.19 | -2.1154 | 0.96232 | 1.9504 | 912.57 |
| 235 | 1123.02 | -394.73 | -389.39 | -2.0733 | 0.95593 | 1.9678 | 877.80 |
| 240 | 1103.65 | -384.94 | -379.50 | -2.0316 | 0.95000 | 1.9894 | 842.74 |
| 245 | 1083.55 | -375.03 | -369.49 | -1.9903 | 0.94456 | 2.0162 | 807.22 |
| 250 | 1062.59 | -364.98 | -359.33 | -1.9493 | 0.93968 | 2.0491 | 771.04 |
| 255 | 1040.62 | -354.75 | -348.99 | -1.9083 | 0.93551 | 2.0897 | 733.92 |
| 260 | 1017.43 | -344.31 | -338.42 | -1.8673 | 0.93233 | 2.1402 | 695.50 |
| 265 | 992.74 | -333.60 | -327.56 | -1.8259 | 0.93057 | 2.2042 | 655.38 |
| 270 | 966.16 | -322.55 | -316.34 | -1.7840 | 0.93070 | 2.2873 | 613.08 |
| 275 | 937.12 | -311.04 | -304.64 | -1.7410 | 0.93321 | 2.3994 | 568.01 |
| 280 | 904.68 | -298.90 | -292.27 | -1.6965 | 0.93889 | 2.5598 | 519.20 |
| 285 | 867.13 | -285.81 | -278.89 | -1.6491 | 0.94979 | 2.8131 | 464.94 |
| 290 | 820.77 | -271.08 | -263.77 | -1.5965 | 0.97135 | 3.2947 | 401.70 |
| 295 | 753.39 | -252.51 | -244.55 | -1.5308 | 1.0250 | 4.7540 | 317.23 |
| 295.128 ^c | 751.03 | -251.92 | -243.93 | -1.5288 | 1.0277 | 4.8386 | 314.35 |
| 295.128 ^c | 210.88 | -131.91 | -103.46 | -1.0528 | 1.1086 | 5.5056 | 193.67 |
| 300 | 182.31 | -117.53 | -84.623 | -0.98943 | 0.96413 | 2.9858 | 207.78 |
| 305 | 166.26 | -107.73 | -71.643 | -0.94650 | 0.90457 | 2.3038 | 217.07 |
| 310 | 154.99 | -99.750 | -61.037 | -0.91200 | 0.87020 | 1.9705 | 224.44 |
| 315 | 146.25 | -92.751 | -51.726 | -0.88220 | 0.84761 | 1.7687 | 230.73 |
| 320 | 139.11 | -86.373 | -43.243 | -0.85548 | 0.83170 | 1.6322 | 236.30 |
| 325 | 133.08 | -80.425 | -35.341 | -0.83098 | 0.82010 | 1.5335 | 241.37 |
| 330 | 127.87 | -74.792 | -27.869 | -0.80816 | 0.81151 | 1.4588 | 246.04 |
| 335 | 123.27 | -69.398 | -20.726 | -0.78668 | 0.80512 | 1.4004 | 250.39 |
| 340 | 119.18 | -64.191 | -13.846 | -0.76629 | 0.80035 | 1.3536 | 254.48 |
| 345 | 115.48 | -59.133 | -7.1762 | -0.74682 | 0.79684 | 1.3154 | 258.36 |
| 350 | 112.12 | -54.197 | -0.68096 | -0.72812 | 0.79430 | 1.2837 | 262.05 |
| 360 | 106.19 | -44.606 | 11.897 | -0.69269 | 0.79142 | 1.2346 | 268.98 |
| 370 | 101.10 | -35.295 | 24.054 | -0.65937 | 0.79070 | 1.1988 | 275.41 |
| 380 | 96.643 | -26.182 | 35.903 | -0.62778 | 0.79152 | 1.1722 | 281.43 |
| 390 | 92.694 | -17.210 | 47.519 | -0.59760 | 0.79347 | 1.1521 | 287.12 |
| 400 | 89.155 | -8.3384 | 58.960 | -0.56863 | 0.79627 | 1.1368 | 292.53 |
| 410 | 85.954 | 0.46261 | 70.268 | -0.54071 | 0.79971 | 1.1252 | 297.71 |
| 420 | 83.036 | 9.2162 | 81.474 | -0.51371 | 0.80365 | 1.1164 | 302.67 |
| 430 | 80.360 | 17.940 | 92.604 | -0.48752 | 0.80797 | 1.1099 | 307.45 |
| 440 | 77.892 | 26.648 | 103.68 | -0.46206 | 0.81258 | 1.1051 | 312.07 |
| 450 | 75.605 | 35.351 | 114.71 | -0.43726 | 0.81742 | 1.1018 | 316.54 |
| 460 | 73.477 | 44.059 | 125.72 | -0.41307 | 0.82242 | 1.0996 | 320.88 |
| 470 | 71.488 | 52.778 | 136.71 | -0.38944 | 0.82755 | 1.0984 | 325.10 |
| 480 | 69.625 | 61.513 | 147.69 | -0.36632 | 0.83277 | 1.0980 | 329.21 |
| 490 | 67.874 | 70.271 | 158.67 | -0.34367 | 0.83805 | 1.0983 | 333.23 |
| 500 | 66.223 | 79.054 | 169.66 | -0.32148 | 0.84337 | 1.0991 | 337.15 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 6.00 MPa Isobar | | | | | | | |
| 525 | 62.477 | 101.14 | 197.18 | -0.26777 | 0.85672 | 1.1030 | 346.60 |
| 550 | 59.186 | 123.45 | 224.82 | -0.21633 | 0.86998 | 1.1087 | 355.60 |
| 575 | 56.264 | 145.98 | 252.62 | -0.16690 | 0.88302 | 1.1157 | 364.23 |
| 600 | 53.645 | 168.76 | 280.61 | -0.11925 | 0.89577 | 1.1234 | 372.54 |
| 625 | 51.282 | 191.80 | 308.80 | -0.07323 | 0.90815 | 1.1317 | 380.56 |
| 650 | 49.136 | 215.09 | 337.20 | -0.02868 | 0.92015 | 1.1402 | 388.32 |
| 675 | 47.176 | 238.62 | 365.81 | 0.01451 | 0.93174 | 1.1488 | 395.86 |
| 700 | 45.377 | 262.41 | 394.64 | 0.05645 | 0.94292 | 1.1574 | 403.20 |
| 800 | 39.435 | 359.91 | 512.06 | 0.21320 | 0.98356 | 1.1906 | 430.87 |
| 900 | 34.924 | 460.85 | 632.65 | 0.35520 | 1.0181 | 1.2206 | 456.39 |
| 1000 | 31.368 | 564.76 | 756.04 | 0.48518 | 1.0472 | 1.2466 | 480.28 |
| 1100 | 28.486 | 671.23 | 881.85 | 0.60507 | 1.0718 | 1.2691 | 502.86 |
| 7.00 MPa Isobar | | | | | | | |
| 217.969 ^b | 1186.73 | -428.06 | -422.16 | -2.2218 | 0.98048 | 1.9170 | 1001.1 |
| 220 | 1179.72 | -424.19 | -418.26 | -2.2040 | 0.97743 | 1.9202 | 987.18 |
| 225 | 1162.17 | -414.66 | -408.64 | -2.1607 | 0.97018 | 1.9298 | 952.99 |
| 230 | 1144.18 | -405.07 | -398.96 | -2.1182 | 0.96334 | 1.9425 | 918.81 |
| 235 | 1125.67 | -395.42 | -389.21 | -2.0763 | 0.95691 | 1.9585 | 884.52 |
| 240 | 1106.56 | -385.69 | -379.36 | -2.0348 | 0.95092 | 1.9785 | 849.99 |
| 245 | 1086.78 | -375.85 | -369.41 | -1.9938 | 0.94542 | 2.0030 | 815.07 |
| 250 | 1066.20 | -365.89 | -359.33 | -1.9530 | 0.94045 | 2.0330 | 779.62 |
| 255 | 1044.69 | -355.77 | -349.07 | -1.9124 | 0.93613 | 2.0699 | 743.39 |
| 260 | 1022.07 | -345.46 | -338.61 | -1.8718 | 0.93267 | 2.1152 | 706.11 |
| 265 | 998.11 | -334.91 | -327.90 | -1.8310 | 0.93037 | 2.1718 | 667.47 |
| 270 | 972.50 | -324.07 | -316.87 | -1.7898 | 0.92952 | 2.2439 | 627.14 |
| 275 | 944.77 | -312.83 | -305.42 | -1.7478 | 0.93042 | 2.3383 | 584.70 |
| 280 | 914.25 | -301.09 | -293.43 | -1.7045 | 0.93353 | 2.4674 | 539.49 |
| 285 | 879.80 | -288.61 | -280.65 | -1.6593 | 0.94003 | 2.6565 | 490.42 |
| 290 | 839.25 | -275.01 | -266.66 | -1.6107 | 0.95290 | 2.9683 | 435.61 |
| 295 | 787.63 | -259.35 | -250.47 | -1.5553 | 0.97893 | 3.5994 | 371.18 |
| 300 | 706.06 | -238.25 | -228.34 | -1.4810 | 1.0529 | 5.9775 | 281.10 |
| 301.833 ^c | 638.31 | -223.87 | -212.90 | -1.4297 | 1.2173 | 14.685 | 211.72 |
| 301.833 ^c | 304.03 | -152.89 | -129.87 | -1.1546 | 1.3535 | 21.953 | 179.63 |
| 305 | 243.08 | -131.34 | -102.55 | -1.0644 | 1.0602 | 5.0681 | 199.60 |
| 310 | 210.63 | -116.70 | -83.469 | -1.0024 | 0.95569 | 3.0512 | 212.29 |
| 315 | 191.97 | -106.54 | -70.071 | -0.95947 | 0.90676 | 2.3936 | 221.05 |
| 320 | 178.74 | -98.192 | -59.029 | -0.92468 | 0.87690 | 2.0539 | 228.16 |
| 325 | 168.48 | -90.870 | -49.322 | -0.89458 | 0.85650 | 1.8433 | 234.30 |
| 330 | 160.11 | -84.207 | -40.487 | -0.86760 | 0.84183 | 1.6992 | 239.80 |
| 335 | 153.05 | -78.004 | -32.266 | -0.84287 | 0.83102 | 1.5942 | 244.81 |
| 340 | 146.95 | -72.139 | -24.503 | -0.81987 | 0.82293 | 1.5144 | 249.45 |
| 345 | 141.59 | -66.532 | -17.094 | -0.79823 | 0.81682 | 1.4517 | 253.79 |
| 350 | 136.82 | -61.129 | -9.9662 | -0.77772 | 0.81220 | 1.4012 | 257.89 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | <i>c_v</i> [kJ/(kg K)] | <i>c_p</i> [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|-------------------------------------|-------------------------------------|-------------------------|
| 7.00 MPa Isobar | | | | | | | |
| 360 | 128.61 | -50.782 | 3.6440 | -0.73937 | 0.80615 | 1.3254 | 265.47 |
| 370 | 121.75 | -40.880 | 16.616 | -0.70383 | 0.80311 | 1.2718 | 272.42 |
| 380 | 115.86 | -31.289 | 29.127 | -0.67046 | 0.80216 | 1.2325 | 278.88 |
| 390 | 110.73 | -21.922 | 41.298 | -0.63885 | 0.80271 | 1.2030 | 284.94 |
| 400 | 106.18 | -12.716 | 53.210 | -0.60869 | 0.80437 | 1.1805 | 290.66 |
| 410 | 102.11 | -3.6281 | 64.925 | -0.57976 | 0.80688 | 1.1632 | 296.11 |
| 420 | 98.436 | 5.3748 | 76.487 | -0.55189 | 0.81003 | 1.1499 | 301.31 |
| 430 | 95.090 | 14.318 | 87.932 | -0.52496 | 0.81369 | 1.1396 | 306.30 |
| 440 | 92.024 | 23.220 | 99.287 | -0.49886 | 0.81773 | 1.1317 | 311.11 |
| 450 | 89.200 | 32.097 | 110.57 | -0.47350 | 0.82208 | 1.1258 | 315.75 |
| 460 | 86.584 | 40.960 | 121.81 | -0.44880 | 0.82666 | 1.1214 | 320.24 |
| 470 | 84.151 | 49.820 | 133.00 | 0.42472 | 0.83141 | 1.1183 | 324.61 |
| 480 | 81.880 | 58.684 | 144.18 | -0.40120 | 0.83631 | 1.1162 | 328.85 |
| 490 | 79.752 | 67.559 | 155.33 | -0.37820 | 0.84130 | 1.1150 | 332.98 |
| 500 | 77.753 | 76.450 | 166.48 | -0.35568 | 0.84636 | 1.1145 | 337.01 |
| 525 | 73.239 | 98.773 | 194.35 | -0.30129 | 0.85919 | 1.1158 | 346.69 |
| 550 | 69.294 | 121.27 | 222.29 | -0.24930 | 0.87205 | 1.1196 | 355.89 |
| 575 | 65.807 | 143.97 | 250.34 | -0.19942 | 0.88478 | 1.1250 | 364.68 |
| 600 | 62.694 | 166.90 | 278.55 | -0.15140 | 0.89727 | 1.1316 | 373.12 |
| 625 | 59.892 | 190.05 | 306.93 | -0.10506 | 0.90945 | 1.1388 | 381.25 |
| 650 | 57.354 | 213.45 | 335.50 | -0.06025 | 0.92129 | 1.1465 | 389.12 |
| 675 | 55.041 | 237.08 | 364.26 | -0.01683 | 0.93275 | 1.1545 | 396.75 |
| 700 | 52.922 | 260.95 | 393.22 | 0.02530 | 0.94382 | 1.1625 | 404.16 |
| 800 | 45.945 | 358.71 | 511.07 | 0.18262 | 0.98415 | 1.1942 | 432.04 |
| 900 | 40.668 | 459.84 | 631.96 | 0.32498 | 1.0185 | 1.2232 | 457.70 |
| 1000 | 36.517 | 563.89 | 755.58 | 0.45520 | 1.0475 | 1.2486 | 481.67 |
| 1100 | 33.158 | 670.46 | 881.58 | 0.57527 | 1.0720 | 1.2707 | 504.30 |
| 7.50 MPa Isobar | | | | | | | |
| 218.074 ^b | 1187.34 | -428.12 | -421.80 | -2.2221 | 0.98087 | 1.9145 | 1003.0 |
| 220 | 1180.72 | -424.46 | -418.11 | -2.2052 | 0.97797 | 1.9173 | 989.88 |
| 225 | 1163.26 | -414.95 | -408.50 | -2.1621 | 0.97071 | 1.9265 | 955.88 |
| 230 | 1145.37 | -405.39 | -398.84 | -2.1196 | 0.96384 | 1.9387 | 921.90 |
| 235 | 1126.97 | -395.76 | -389.11 | -2.0777 | 0.95738 | 1.9541 | 887.83 |
| 240 | 1107.99 | -386.06 | -379.29 | -2.0364 | 0.95138 | 1.9732 | 853.55 |
| 245 | 1088.36 | -376.26 | -369.37 | -1.9955 | 0.94584 | 1.9967 | 818.94 |
| 250 | 1067.96 | -366.34 | -359.32 | -1.9549 | 0.94083 | 2.0254 | 783.82 |
| 255 | 1046.67 | -356.27 | -349.10 | -1.9144 | 0.93644 | 2.0605 | 748.00 |
| 260 | 1024.32 | -346.02 | -338.70 | -1.8740 | 0.93286 | 2.1036 | 711.24 |
| 265 | 1000.70 | -335.55 | -328.05 | -1.8334 | 0.93034 | 2.1570 | 673.27 |
| 270 | 975.52 | -324.79 | -317.10 | -1.7925 | 0.92912 | 2.2243 | 633.79 |
| 275 | 948.38 | -313.68 | -305.78 | -1.7510 | 0.92943 | 2.3115 | 592.46 |
| 280 | 918.68 | -302.10 | -293.94 | -1.7083 | 0.93163 | 2.4284 | 548.71 |
| 285 | 885.48 | -289.88 | -281.41 | -1.6640 | 0.93668 | 2.5947 | 501.67 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 7.50 MPa Isobar | | | | | | | |
| 290 | 847.07 | -276.69 | -267.84 | -1.6168 | 0.94689 | 2.8557 | 449.91 |
| 295 | 799.88 | -261.88 | -252.50 | -1.5643 | 0.96694 | 3.3335 | 390.87 |
| 300 | 733.90 | -243.62 | -233.40 | -1.5001 | 1.0115 | 4.5507 | 317.38 |
| 305 | 389.85 | -171.22 | -151.98 | -1.2323 | 1.5317 | 67.567 | 168.55 |
| 310 | 253.36 | -129.11 | -99.510 | -1.0611 | 1.0261 | 4.5173 | 204.64 |
| 315 | 222.11 | -115.30 | -81.528 | -1.0035 | 0.94620 | 2.9805 | 215.79 |
| 320 | 203.04 | -105.22 | -68.283 | -0.96181 | 0.90445 | 2.3876 | 223.97 |
| 325 | 189.27 | -96.845 | -57.220 | -0.92750 | 0.87759 | 2.0648 | 230.79 |
| 330 | 178.52 | -89.456 | -47.442 | -0.89764 | 0.85879 | 1.8598 | 236.76 |
| 335 | 169.70 | -82.714 | -38.518 | -0.87080 | 0.84513 | 1.7176 | 242.13 |
| 340 | 162.24 | -76.430 | -30.204 | -0.84616 | 0.83499 | 1.6131 | 247.06 |
| 345 | 155.80 | -70.486 | -22.346 | -0.82322 | 0.82734 | 1.5331 | 251.64 |
| 350 | 150.13 | -64.802 | -14.845 | -0.80163 | 0.82151 | 1.4699 | 255.93 |
| 360 | 140.52 | -54.014 | -0.64140 | -0.76161 | 0.81370 | 1.3768 | 263.84 |
| 370 | 132.60 | -43.777 | 12.785 | -0.72482 | 0.80942 | 1.3121 | 271.05 |
| 380 | 125.88 | -33.921 | 25.660 | -0.69048 | 0.80754 | 1.2652 | 277.72 |
| 390 | 120.06 | -24.337 | 38.129 | -0.65809 | 0.80736 | 1.2302 | 283.95 |
| 400 | 114.95 | -14.951 | 50.293 | -0.62729 | 0.80844 | 1.2036 | 289.83 |
| 410 | 110.40 | -5.7101 | 62.222 | -0.59783 | 0.81047 | 1.1832 | 295.40 |
| 420 | 106.31 | 3.4250 | 73.971 | -0.56952 | 0.81323 | 1.1673 | 300.72 |
| 430 | 102.60 | 12.483 | 85.580 | -0.54220 | 0.81654 | 1.1550 | 305.81 |
| 440 | 99.215 | 21.487 | 97.080 | -0.51576 | 0.82030 | 1.1454 | 310.71 |
| 450 | 96.102 | 30.454 | 108.50 | -0.49011 | 0.82440 | 1.1381 | 315.43 |
| 460 | 93.227 | 39.399 | 119.85 | -0.46516 | 0.82877 | 1.1325 | 319.99 |
| 470 | 90.558 | 48.331 | 131.15 | -0.44085 | 0.83334 | 1.1284 | 324.42 |
| 480 | 88.072 | 57.262 | 142.42 | -0.41713 | 0.83807 | 1.1254 | 328.72 |
| 490 | 85.747 | 66.197 | 153.66 | -0.39394 | 0.84291 | 1.1235 | 332.91 |
| 500 | 83.566 | 75.143 | 164.89 | -0.37126 | 0.84785 | 1.1224 | 336.99 |
| 525 | 78.652 | 97.585 | 192.94 | -0.31651 | 0.86041 | 1.1223 | 346.78 |
| 550 | 74.369 | 120.18 | 221.03 | -0.26425 | 0.87307 | 1.1251 | 356.07 |
| 575 | 70.592 | 142.97 | 249.21 | -0.21414 | 0.88565 | 1.1297 | 364.93 |
| 600 | 67.225 | 165.96 | 277.53 | -0.16594 | 0.89802 | 1.1357 | 373.44 |
| 625 | 64.201 | 189.18 | 306.00 | -0.11944 | 0.91010 | 1.1424 | 381.63 |
| 650 | 61.464 | 212.63 | 334.65 | -0.07450 | 0.92186 | 1.1497 | 389.54 |
| 675 | 58.972 | 236.31 | 363.49 | -0.03096 | 0.93325 | 1.1573 | 397.21 |
| 700 | 56.691 | 260.22 | 392.52 | 0.01126 | 0.94426 | 1.1651 | 404.66 |
| 800 | 49.193 | 358.12 | 510.58 | 0.16887 | 0.98445 | 1.1959 | 432.65 |
| 900 | 43.532 | 459.34 | 631.63 | 0.31141 | 1.0187 | 1.2245 | 458.36 |
| 1000 | 39.083 | 563.46 | 755.36 | 0.44175 | 1.0477 | 1.2496 | 482.37 |
| 1100 | 35.485 | 670.08 | 881.44 | 0.56190 | 1.0722 | 1.2714 | 505.03 |
| 8.00 MPa Isobar | | | | | | | |
| 218.180 ^b | 1187.95 | -428.17 | -421.44 | -2.2224 | 0.98126 | 1.9120 | 1004.9 |
| 220 | 1181.72 | -424.73 | -417.96 | -2.2065 | 0.97851 | 1.9145 | 992.56 |
| 225 | 1164.35 | -415.23 | -408.36 | -2.1634 | 0.97122 | 1.9233 | 958.75 |
| 230 | 1146.54 | -405.70 | -398.72 | -2.1210 | 0.96433 | 1.9349 | 924.97 |
| 235 | 1128.26 | -396.10 | -389.01 | -2.0792 | 0.95786 | 1.9497 | 891.12 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|--------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 8.00 MPa Isobar | | | | | | | |
| 240 | 1109.41 | -386.43 | -379.22 | -2.0380 | 0.95182 | 1.9681 | 857.09 |
| 245 | 1089.93 | -376.66 | -369.32 | -1.9972 | 0.94626 | 1.9906 | 822.75 |
| 250 | 1069.70 | -366.78 | -359.30 | -1.9567 | 0.94120 | 2.0181 | 787.97 |
| 255 | 1048.62 | -356.76 | -349.13 | -1.9164 | 0.93676 | 2.0516 | 752.55 |
| 260 | 1026.53 | -346.57 | -338.77 | -1.8762 | 0.93307 | 2.0925 | 716.27 |
| 265 | 1003.23 | -336.16 | -328.19 | -1.8359 | 0.93036 | 2.1429 | 678.91 |
| 270 | 978.46 | -325.50 | -317.32 | -1.7952 | 0.92882 | 2.2060 | 640.22 |
| 275 | 951.86 | -314.51 | -306.10 | -1.7541 | 0.92864 | 2.2867 | 599.89 |
| 280 | 922.92 | -303.08 | -294.41 | -1.7119 | 0.93010 | 2.3931 | 557.45 |
| 285 | 890.82 | -291.08 | -282.10 | -1.6684 | 0.93400 | 2.5408 | 512.17 |
| 290 | 854.20 | -278.25 | -268.88 | -1.6224 | 0.94218 | 2.7633 | 462.96 |
| 295 | 810.40 | -264.09 | -254.22 | -1.5722 | 0.95803 | 3.1417 | 408.04 |
| 300 | 753.17 | -247.44 | -236.82 | -1.5138 | 0.98934 | 3.9320 | 343.66 |
| 305 | 656.77 | -223.65 | -211.47 | -1.4301 | 1.0822 | 7.3125 | 255.09 |
| 310 | 327.71 | -149.25 | -124.84 | -1.1485 | 1.1499 | 9.5864 | 194.28 |
| 315 | 261.29 | -126.27 | -95.650 | -1.0550 | 0.99624 | 4.0300 | 210.19 |
| 320 | 231.91 | -113.35 | -78.854 | -1.0021 | 0.93636 | 2.8750 | 219.80 |
| 325 | 212.90 | -103.49 | -65.909 | -0.96190 | 0.90103 | 2.3574 | 227.35 |
| 330 | 198.87 | -95.152 | -54.926 | -0.92836 | 0.87714 | 2.0594 | 233.83 |
| 335 | 187.79 | -87.747 | -45.146 | -0.89894 | 0.86009 | 1.8648 | 239.57 |
| 340 | 178.65 | -80.965 | -36.184 | -0.87239 | 0.84758 | 1.7274 | 244.79 |
| 345 | 170.89 | -74.629 | -27.814 | -0.84795 | 0.83820 | 1.6253 | 249.61 |
| 350 | 164.16 | -68.627 | -19.893 | -0.82515 | 0.83106 | 1.5463 | 254.10 |
| 360 | 152.93 | -57.348 | -5.0372 | -0.78329 | 0.82137 | 1.4326 | 262.32 |
| 370 | 143.82 | -46.747 | 8.8792 | -0.74516 | 0.81579 | 1.3552 | 269.78 |
| 380 | 136.18 | -36.607 | 22.140 | -0.70979 | 0.81295 | 1.2998 | 276.65 |
| 390 | 129.63 | -26.793 | 34.923 | -0.67659 | 0.81202 | 1.2588 | 283.05 |
| 400 | 123.90 | -17.218 | 47.348 | -0.64513 | 0.81251 | 1.2277 | 289.07 |
| 410 | 118.84 | -7.8163 | 59.501 | -0.61512 | 0.81406 | 1.2038 | 294.76 |
| 420 | 114.31 | 1.4561 | 71.442 | -0.58634 | 0.81641 | 1.1852 | 300.19 |
| 430 | 110.21 | 10.634 | 83.219 | -0.55863 | 0.81939 | 1.1708 | 305.37 |
| 440 | 106.49 | 19.742 | 94.868 | -0.53185 | 0.82286 | 1.1594 | 310.36 |
| 450 | 103.07 | 28.802 | 106.42 | -0.50589 | 0.82671 | 1.1506 | 315.15 |
| 460 | 99.928 | 37.829 | 117.89 | -0.48068 | 0.83087 | 1.1438 | 319.79 |
| 470 | 97.016 | 46.837 | 129.30 | -0.45614 | 0.83525 | 1.1386 | 324.28 |
| 480 | 94.307 | 55.834 | 140.66 | -0.43221 | 0.83982 | 1.1348 | 328.64 |
| 490 | 91.778 | 64.831 | 152.00 | -0.40884 | 0.84452 | 1.1321 | 332.88 |
| 500 | 89.410 | 73.833 | 163.31 | -0.38599 | 0.84933 | 1.1302 | 337.00 |
| 525 | 84.085 | 96.397 | 191.54 | -0.33090 | 0.86163 | 1.1288 | 346.90 |
| 550 | 79.458 | 119.09 | 219.78 | -0.27835 | 0.87409 | 1.1306 | 356.28 |
| 575 | 75.385 | 141.96 | 248.08 | -0.22802 | 0.88651 | 1.1345 | 365.22 |
| 600 | 71.762 | 165.03 | 276.51 | -0.17963 | 0.89876 | 1.1398 | 373.78 |
| 625 | 68.511 | 188.31 | 305.08 | -0.13298 | 0.91075 | 1.1460 | 382.03 |
| 650 | 65.573 | 211.81 | 333.82 | -0.08790 | 0.92242 | 1.1529 | 389.98 |
| 675 | 62.901 | 235.54 | 362.73 | -0.04425 | 0.93375 | 1.1601 | 397.69 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 8.00 MPa Isobar | | | | | | | |
| 700 | 60.457 | 259.50 | 391.82 | -0.00193 | 0.94470 | 1.1676 | 405.18 |
| 800 | 52.435 | 357.53 | 510.10 | 0.15596 | 0.98474 | 1.1977 | 433.26 |
| 900 | 46.389 | 458.84 | 631.29 | 0.29867 | 1.0189 | 1.2257 | 459.03 |
| 1000 | 41.644 | 563.03 | 755.14 | 0.42913 | 1.0478 | 1.2506 | 483.08 |
| 1100 | 37.807 | 669.71 | 881.31 | 0.54937 | 1.0723 | 1.2722 | 505.75 |
| 10.00 MPa Isobar | | | | | | | |
| 218.600 ^b | 1190.34 | -428.40 | -420.00 | -2.2235 | 0.98274 | 1.9023 | 1012.5 |
| 220 | 1185.63 | -425.77 | -417.34 | -2.2113 | 0.98061 | 1.9039 | 1003.1 |
| 225 | 1168.59 | -416.36 | -407.80 | -2.1685 | 0.97323 | 1.9111 | 970.04 |
| 230 | 1151.15 | -406.91 | -398.22 | -2.1264 | 0.96625 | 1.9208 | 937.02 |
| 235 | 1133.28 | -397.41 | -388.59 | -2.0849 | 0.95969 | 1.9333 | 904.01 |
| 240 | 1114.92 | -387.85 | -378.88 | -2.0441 | 0.95356 | 1.9488 | 870.91 |
| 245 | 1095.99 | -378.22 | -369.09 | -2.0037 | 0.94788 | 1.9679 | 837.63 |
| 250 | 1076.42 | -368.49 | -359.20 | -1.9637 | 0.94269 | 1.9910 | 804.05 |
| 255 | 1056.11 | -358.64 | -349.18 | -1.9240 | 0.93803 | 2.0189 | 770.05 |
| 260 | 1034.95 | -348.66 | -339.00 | -1.8845 | 0.93400 | 2.0524 | 735.50 |
| 265 | 1012.80 | -338.51 | -328.64 | -1.8450 | 0.93072 | 2.0930 | 700.25 |
| 270 | 989.46 | -328.16 | -318.06 | -1.8055 | 0.92828 | 2.1425 | 664.15 |
| 275 | 964.71 | -317.56 | -307.20 | -1.7656 | 0.92676 | 2.2034 | 627.04 |
| 280 | 938.22 | -306.65 | -296.00 | -1.7253 | 0.92632 | 2.2798 | 588.67 |
| 285 | 909.56 | -295.36 | -284.36 | -1.6841 | 0.92734 | 2.3782 | 548.68 |
| 290 | 878.06 | -283.55 | -272.16 | -1.6416 | 0.93072 | 2.5108 | 506.63 |
| 295 | 842.67 | -271.03 | -259.16 | -1.5972 | 0.93777 | 2.7009 | 461.99 |
| 300 | 801.62 | -257.46 | -244.98 | -1.5496 | 0.94964 | 2.9906 | 414.28 |
| 305 | 751.67 | -242.25 | -228.94 | -1.4965 | 0.96817 | 3.4711 | 363.01 |
| 310 | 685.77 | -224.06 | -209.48 | -1.4333 | 0.99962 | 4.4460 | 307.04 |
| 315 | 586.02 | -199.41 | -182.35 | -1.3465 | 1.0487 | 6.6962 | 249.42 |
| 320 | 448.28 | -166.19 | -143.88 | -1.2253 | 1.0577 | 7.6175 | 219.14 |
| 325 | 358.04 | -140.73 | -112.80 | -1.1289 | 1.0095 | 4.9438 | 219.84 |
| 330 | 310.25 | -124.28 | -92.049 | -1.0655 | 0.96291 | 3.5312 | 225.91 |
| 335 | 280.11 | -112.06 | -76.359 | -1.0183 | 0.92780 | 2.8165 | 232.23 |
| 340 | 258.62 | -102.06 | -63.396 | -0.97991 | 0.90255 | 2.4017 | 238.14 |
| 345 | 242.11 | -93.404 | -52.100 | -0.94692 | 0.88431 | 2.1341 | 243.58 |
| 350 | 228.80 | -85.626 | -41.921 | -0.91762 | 0.87083 | 1.9480 | 248.62 |
| 360 | 208.25 | -71.776 | -23.756 | -0.86644 | 0.85262 | 1.7065 | 257.77 |
| 370 | 192.74 | -59.374 | -7.4896 | -0.82186 | 0.84146 | 1.5574 | 265.97 |
| 380 | 180.38 | -47.885 | 7.5523 | -0.78174 | 0.83458 | 1.4570 | 273.47 |
| 390 | 170.18 | -37.015 | 21.746 | -0.74486 | 0.83060 | 1.3856 | 280.40 |
| 400 | 161.53 | -26.584 | 35.325 | -0.71048 | 0.82867 | 1.3327 | 286.88 |
| 410 | 154.05 | -16.473 | 48.443 | -0.67809 | 0.82827 | 1.2927 | 292.99 |
| 420 | 147.48 | -6.5998 | 61.208 | -0.64733 | 0.82901 | 1.2616 | 298.77 |
| 430 | 141.63 | 3.0936 | 73.698 | -0.61794 | 0.83064 | 1.2373 | 304.28 |
| 440 | 136.39 | 12.651 | 85.972 | -0.58972 | 0.83297 | 1.2181 | 309.55 |
| 450 | 131.63 | 22.106 | 98.073 | -0.56252 | 0.83584 | 1.2028 | 314.60 |
| 460 | 127.30 | 31.483 | 110.04 | -0.53623 | 0.83915 | 1.1906 | 319.48 |
| 470 | 123.32 | 40.803 | 121.89 | -0.51073 | 0.84280 | 1.1809 | 324.18 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 10.00 MPa Isobar | | | | | | | |
| 480 | 119.65 | 50.083 | 133.66 | -0.48595 | 0.84672 | 1.1732 | 328.74 |
| 490 | 116.24 | 59.335 | 145.36 | -0.46183 | 0.85085 | 1.1671 | 333.16 |
| 500 | 113.07 | 68.569 | 157.01 | -0.43830 | 0.85516 | 1.1624 | 337.45 |
| 525 | 106.01 | 91.633 | 185.97 | -0.38178 | 0.86644 | 1.1552 | 347.71 |
| 550 | 99.930 | 114.74 | 214.81 | -0.32811 | 0.87812 | 1.1527 | 357.39 |
| 575 | 94.626 | 137.95 | 243.63 | -0.27686 | 0.88993 | 1.1533 | 366.58 |
| 600 | 89.941 | 161.31 | 272.49 | -0.22773 | 0.90169 | 1.1561 | 375.37 |
| 625 | 85.761 | 184.84 | 301.45 | -0.18045 | 0.91329 | 1.1603 | 383.79 |
| 650 | 81.999 | 208.57 | 330.52 | -0.13485 | 0.92464 | 1.1655 | 391.91 |
| 675 | 78.592 | 232.49 | 359.73 | -0.09075 | 0.93571 | 1.1714 | 399.76 |
| 700 | 75.486 | 256.61 | 389.09 | -0.04804 | 0.94645 | 1.1777 | 407.36 |
| 800 | 63.349 | 355.17 | 508.20 | 0.11097 | 0.98391 | 1.2046 | 435.79 |
| 900 | 57.759 | 456.85 | 629.99 | 0.25438 | 1.0198 | 1.2308 | 461.77 |
| 1000 | 51.825 | 561.32 | 754.28 | 0.38532 | 1.0485 | 1.2545 | 485.94 |
| 1100 | 47.040 | 668.21 | 880.79 | 0.50588 | 1.0728 | 1.2753 | 508.69 |
| 15.00 MPa Isobar | | | | | | | |
| 219.644 ^b | 1196.11 | -428.91 | -416.37 | -2.2260 | 0.98604 | 1.8799 | 1030.9 |
| 220 | 1194.96 | -428.25 | -415.70 | -2.2230 | 0.98548 | 1.8801 | 1028.7 |
| 225 | 1178.64 | -419.02 | -406.29 | -2.1807 | 0.97789 | 1.8841 | 991.14 |
| 230 | 1162.02 | -409.76 | -396.86 | -2.1392 | 0.97070 | 1.8900 | 965.81 |
| 235 | 1145.06 | -400.49 | -387.39 | -2.0985 | 0.96394 | 1.8980 | 934.61 |
| 240 | 1127.73 | -391.17 | -377.87 | -2.0584 | 0.95760 | 1.9081 | 903.50 |
| 245 | 1109.98 | -381.82 | -368.30 | -2.0190 | 0.95169 | 1.9206 | 872.40 |
| 250 | 1091.77 | -372.40 | -358.66 | -1.9800 | 0.94623 | 1.9358 | 841.27 |
| 255 | 1073.03 | -362.92 | -348.94 | -1.9415 | 0.94121 | 1.9539 | 810.04 |
| 260 | 1053.71 | -353.35 | -339.12 | -1.9034 | 0.93667 | 1.9752 | 778.68 |
| 265 | 1033.73 | -343.69 | -329.18 | -1.8655 | 0.93264 | 2.0002 | 747.13 |
| 270 | 1013.01 | -333.92 | -319.11 | -1.8279 | 0.92914 | 2.0294 | 715.36 |
| 275 | 991.45 | -324.01 | -308.88 | -1.7903 | 0.92619 | 2.0635 | 683.32 |
| 280 | 968.93 | -313.95 | -298.47 | -1.7528 | 0.92381 | 2.1034 | 650.96 |
| 285 | 945.30 | -303.70 | -287.83 | -1.7152 | 0.92211 | 2.1501 | 618.23 |
| 290 | 920.40 | -293.25 | -276.95 | -1.6773 | 0.92132 | 2.2055 | 585.07 |
| 295 | 894.00 | -282.54 | -265.76 | -1.6390 | 0.92183 | 2.2727 | 551.45 |
| 300 | 865.82 | -271.52 | -254.20 | -1.6002 | 0.92380 | 2.3557 | 517.40 |
| 305 | 835.48 | -260.12 | -242.17 | -1.5604 | 0.92683 | 2.4583 | 483.07 |
| 310 | 802.54 | -248.27 | -229.58 | -1.5195 | 0.93036 | 2.5830 | 448.77 |
| 315 | 766.51 | -235.86 | -216.30 | -1.4770 | 0.93449 | 2.7343 | 414.97 |
| 320 | 726.83 | -222.81 | -202.18 | -1.4325 | 0.93978 | 2.9188 | 382.22 |
| 325 | 683.09 | -209.02 | -187.06 | -1.3857 | 0.94662 | 3.1280 | 351.34 |
| 330 | 635.51 | -194.51 | -170.91 | -1.3363 | 0.95475 | 3.3309 | 323.89 |
| 335 | 585.40 | -179.47 | -153.85 | -1.2850 | 0.96004 | 3.4748 | 301.72 |
| 340 | 535.55 | -164.42 | -136.41 | -1.2333 | 0.95711 | 3.4738 | 286.11 |
| 345 | 489.42 | -150.03 | -119.38 | -1.1836 | 0.94688 | 3.3164 | 276.63 |
| 350 | 449.20 | -136.79 | -103.39 | -1.1376 | 0.93439 | 3.0688 | 271.76 |
| 360 | 387.08 | -114.04 | -75.292 | -1.0584 | 0.91214 | 2.5672 | 270.06 |
| 370 | 343.43 | -95.274 | -51.596 | -0.99347 | 0.89468 | 2.1949 | 273.34 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 15.00 MPa Isobar | | | | | | | |
| 380 | 311.48 | -79.159 | -31.001 | -0.93853 | 0.88143 | 1.9402 | 278.46 |
| 390 | 286.97 | -64.804 | -12.533 | -0.89055 | 0.87178 | 1.7638 | 284.22 |
| 400 | 267.42 | -51.652 | 4.4406 | 0.84757 | 0.86502 | 1.6376 | 290.12 |
| 410 | 251.33 | -39.353 | 20.329 | -0.80833 | 0.86053 | 1.5445 | 295.97 |
| 420 | 237.78 | -27.678 | 35.405 | -0.77200 | 0.85782 | 1.4739 | 301.68 |
| 430 | 226.14 | -16.471 | 49.860 | -0.73798 | 0.85650 | 1.4192 | 307.22 |
| 440 | 215.98 | -5.6217 | 63.828 | -0.70587 | 0.85630 | 1.3761 | 312.59 |
| 450 | 207.01 | 4.9509 | 77.410 | -0.67534 | 0.85698 | 1.3416 | 317.79 |
| 460 | 199.00 | 15.307 | 90.682 | -0.64617 | 0.85839 | 1.3138 | 322.83 |
| 470 | 191.79 | 25.492 | 103.70 | -0.61817 | 0.86037 | 1.2911 | 327.70 |
| 480 | 185.24 | 35.541 | 116.52 | -0.59119 | 0.86283 | 1.2725 | 332.43 |
| 490 | 179.26 | 45.484 | 129.16 | -0.56511 | 0.86568 | 1.2572 | 337.03 |
| 500 | 173.76 | 55.342 | 141.67 | -0.53985 | 0.86884 | 1.2445 | 341.50 |
| 525 | 161.74 | 79.733 | 172.48 | -0.47972 | 0.87776 | 1.2218 | 352.18 |
| 550 | 151.63 | 103.91 | 202.83 | -0.42323 | 0.88763 | 1.2080 | 362.24 |
| 575 | 142.97 | 128.01 | 232.93 | -0.36972 | 0.89803 | 1.2002 | 371.77 |
| 600 | 135.43 | 152.12 | 262.88 | -0.31873 | 0.90867 | 1.1963 | 380.86 |
| 625 | 128.78 | 176.29 | 292.77 | -0.26992 | 0.91936 | 1.1953 | 389.55 |
| 650 | 122.86 | 200.57 | 322.66 | -0.22303 | 0.92998 | 1.1963 | 397.91 |
| 675 | 117.54 | 224.98 | 352.59 | -0.17784 | 0.94044 | 1.1987 | 403.96 |
| 700 | 112.72 | 249.53 | 382.60 | -0.13418 | 0.95067 | 1.2022 | 413.74 |
| 800 | 97.199 | 349.41 | 503.73 | 0.02753 | 0.98876 | 1.2213 | 442.71 |
| 900 | 85.740 | 452.00 | 626.95 | 0.17264 | 1.0218 | 1.2430 | 469.01 |
| 1000 | 76.856 | 557.14 | 752.31 | 0.30470 | 1.0501 | 1.2639 | 493.37 |
| 1100 | 69.730 | 664.55 | 879.66 | 0.42606 | 1.0741 | 1.2828 | 516.21 |
| 20.00 MPa Isobar | | | | | | | |
| 220.677 ^b | 1201.58 | -429.34 | 412.70 | 2.2283 | 0.98884 | 1.8600 | 1048.9 |
| 225 | 1188.00 | -421.49 | -404.66 | -2.1922 | 0.98212 | 1.8614 | 1022.8 |
| 230 | 1172.07 | -412.41 | -395.34 | -2.1513 | 0.97475 | 1.8644 | 992.92 |
| 235 | 1155.89 | -403.31 | -386.01 | -2.1111 | 0.96780 | 1.8690 | 963.24 |
| 240 | 1139.41 | -394.20 | -376.65 | -2.0717 | 0.96128 | 1.8753 | 933.74 |
| 245 | 1122.62 | -385.07 | -367.25 | -2.0330 | 0.95519 | 1.8833 | 904.38 |
| 250 | 1105.47 | -375.91 | -357.81 | -1.9948 | 0.94951 | 1.8932 | 875.14 |
| 255 | 1087.95 | -366.70 | -348.32 | -1.9572 | 0.94426 | 1.9050 | 845.98 |
| 260 | 1070.01 | -357.45 | -338.76 | -1.9201 | 0.93944 | 1.9188 | 816.88 |
| 265 | 1051.60 | -348.15 | -329.13 | -1.8834 | 0.93504 | 1.9349 | 787.84 |
| 270 | 1032.69 | -338.77 | -319.41 | -1.8471 | 0.93107 | 1.9533 | 758.85 |
| 275 | 1013.23 | -329.33 | -309.59 | -1.8110 | 0.92753 | 1.9742 | 729.90 |
| 280 | 993.16 | -319.80 | -299.66 | -1.7753 | 0.92441 | 1.9979 | 701.00 |
| 285 | 972.43 | -310.17 | -289.61 | -1.7397 | 0.92176 | 2.0245 | 672.16 |
| 290 | 950.97 | -300.44 | -279.41 | -1.7042 | 0.91964 | 2.0543 | 643.38 |
| 295 | 928.71 | -290.59 | -269.06 | -1.6688 | 0.91824 | 2.0881 | 614.69 |
| 300 | 905.57 | -280.61 | -258.52 | -1.6334 | 0.91763 | 2.1267 | 586.17 |
| 305 | 881.46 | -270.47 | -247.78 | -1.5979 | 0.91763 | 2.1709 | 557.91 |
| 310 | 856.27 | -260.16 | -236.80 | -1.5622 | 0.91780 | 2.2204 | 530.04 |
| 315 | 829.92 | -249.67 | -225.57 | -1.5262 | 0.91794 | 2.2743 | 502.71 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 20.00 MPa Isobar | | | | | | | |
| 320 | 802.33 | -238.98 | -214.05 | -1.4900 | 0.91835 | 2.3324 | 476.13 |
| 325 | 773.46 | -228.09 | -202.24 | -1.4533 | 0.91938 | 2.3952 | 450.59 |
| 330 | 743.30 | -217.00 | -190.10 | -1.4163 | 0.92095 | 2.4610 | 420.44 |
| 335 | 711.96 | -205.72 | -177.63 | -1.3788 | 0.92254 | 2.5246 | 404.10 |
| 340 | 679.68 | -194.29 | -164.87 | -1.3410 | 0.92342 | 2.5778 | 384.01 |
| 345 | 646.90 | -182.80 | -151.88 | -1.3030 | 0.92298 | 2.6122 | 366.45 |
| 350 | 614.18 | -171.35 | -138.79 | -1.2654 | 0.92115 | 2.6207 | 351.52 |
| 360 | 551.54 | -149.10 | -112.84 | -1.1923 | 0.91549 | 2.5511 | 329.54 |
| 370 | 496.14 | -128.36 | -88.048 | -1.1243 | 0.90910 | 2.3976 | 316.94 |
| 380 | 449.68 | -109.47 | -64.990 | -1.0628 | 0.90195 | 2.2129 | 311.16 |
| 390 | 411.63 | -92.347 | -43.760 | -1.0077 | 0.89472 | 2.0369 | 309.69 |
| 400 | 380.50 | -76.728 | -24.165 | -0.95804 | 0.88827 | 1.8868 | 310.75 |
| 410 | 354.77 | -62.306 | -5.9310 | -0.91301 | 0.88304 | 1.7645 | 313.29 |
| 420 | 333.19 | -48.819 | 11.205 | -0.87171 | 0.87912 | 1.6664 | 316.66 |
| 430 | 314.83 | -36.064 | 27.462 | -0.83346 | 0.87643 | 1.5878 | 320.52 |
| 440 | 298.99 | -23.881 | 43.011 | -0.79771 | 0.87484 | 1.5244 | 324.64 |
| 450 | 285.14 | -12.151 | 57.989 | -0.76405 | 0.87419 | 1.4729 | 328.91 |
| 460 | 272.92 | -0.78247 | 72.500 | -0.73215 | 0.87434 | 1.4307 | 333.22 |
| 470 | 262.02 | 10.296 | 86.627 | -0.70177 | 0.87517 | 1.3959 | 337.54 |
| 480 | 252.21 | 21.140 | 100.44 | -0.67269 | 0.87657 | 1.3671 | 341.84 |
| 490 | 243.34 | 31.794 | 113.98 | -0.64476 | 0.87845 | 1.3430 | 346.09 |
| 500 | 235.24 | 42.292 | 127.31 | -0.61783 | 0.88074 | 1.3228 | 350.29 |
| 525 | 217.77 | 68.036 | 159.88 | -0.55427 | 0.88779 | 1.2852 | 360.49 |
| 550 | 203.30 | 93.302 | 191.68 | -0.49509 | 0.89618 | 1.2606 | 370.28 |
| 575 | 191.06 | 118.30 | 222.98 | -0.43943 | 0.90540 | 1.2446 | 379.65 |
| 600 | 180.50 | 143.15 | 253.95 | -0.38670 | 0.91508 | 1.2344 | 388.65 |
| 625 | 171.28 | 167.96 | 284.73 | -0.33644 | 0.92499 | 1.2284 | 397.29 |
| 650 | 163.12 | 192.79 | 315.40 | -0.28833 | 0.93496 | 1.2254 | 405.62 |
| 675 | 155.83 | 217.68 | 346.02 | -0.24210 | 0.94487 | 1.2246 | 413.67 |
| 700 | 149.27 | 242.66 | 376.64 | -0.19756 | 0.95465 | 1.2253 | 421.46 |
| 800 | 128.34 | 343.83 | 499.67 | -0.03329 | 0.99149 | 1.2370 | 450.47 |
| 900 | 113.04 | 447.31 | 624.23 | 0.11340 | 1.0238 | 1.2545 | 476.80 |
| 1000 | 101.27 | 553.10 | 750.60 | 0.24652 | 1.0516 | 1.2727 | 501.16 |
| 1100 | 91.857 | 661.01 | 878.74 | 0.36864 | 1.0754 | 1.2898 | 523.98 |
| 25.00 MPa Isobar | | | | | | | |
| 221.701 ^b | 1206.79 | -429.71 | -409.00 | -2.2303 | 0.99124 | 1.8421 | 1066.4 |
| 225 | 1196.78 | -423.81 | -402.92 | -2.2031 | 0.98601 | 1.8419 | 1047.3 |
| 230 | 1181.45 | -414.87 | -393.71 | -2.1626 | 0.97846 | 1.8427 | 1018.6 |
| 235 | 1165.92 | -405.93 | -384.49 | -2.1230 | 0.97135 | 1.8448 | 990.21 |
| 240 | 1150.17 | -396.99 | -375.26 | -2.0841 | 0.96468 | 1.8482 | 962.06 |
| 245 | 1134.16 | -388.05 | -366.00 | -2.0460 | 0.95843 | 1.8530 | 934.14 |
| 250 | 1117.90 | -379.09 | -356.73 | -2.0085 | 0.95259 | 1.8591 | 906.41 |
| 255 | 1101.35 | -370.11 | -347.41 | -1.9716 | 0.94717 | 1.8666 | 878.88 |
| 260 | 1084.49 | -361.11 | -338.06 | -1.9352 | 0.94215 | 1.8755 | 851.52 |
| 265 | 1067.29 | -352.08 | -328.65 | -1.8994 | 0.93752 | 1.8859 | 824.34 |

A NEW EQUATION OF STATE FOR CARBON DIOXIDE

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TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|--------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 25.00 MPa Isobar | | | | | | | |
| 270 | 1049.74 | -343.01 | -319.20 | -1.8641 | 0.93329 | 1.8978 | 797.36 |
| 275 | 1031.80 | -333.90 | -309.67 | -1.8291 | 0.92943 | 1.9111 | 770.56 |
| 280 | 1013.45 | -324.75 | -300.08 | -1.7946 | 0.92595 | 1.9259 | 743.98 |
| 285 | 994.67 | -315.55 | -290.41 | -1.7603 | 0.92283 | 1.9422 | 717.64 |
| 290 | 975.42 | -306.29 | -280.66 | -1.7264 | 0.92013 | 1.9600 | 691.56 |
| 295 | 955.68 | -296.97 | -270.81 | -1.6927 | 0.91792 | 1.9794 | 665.77 |
| 300 | 935.42 | -287.59 | -260.86 | -1.6593 | 0.91623 | 2.0008 | 640.35 |
| 305 | 914.62 | -278.13 | -250.80 | -1.6260 | 0.91497 | 2.0242 | 615.36 |
| 310 | 893.25 | -268.60 | -240.61 | -1.5929 | 0.91387 | 2.0495 | 590.90 |
| 315 | 871.29 | -258.99 | -230.30 | -1.5599 | 0.91273 | 2.0760 | 567.03 |
| 320 | 848.72 | -249.31 | -219.85 | -1.5270 | 0.91162 | 2.1032 | 543.81 |
| 325 | 825.55 | -239.55 | -209.27 | -1.4942 | 0.91081 | 2.1309 | 521.34 |
| 330 | 801.80 | -229.72 | -198.54 | -1.4614 | 0.91044 | 2.1592 | 499.77 |
| 335 | 777.50 | -219.83 | -187.68 | -1.4287 | 0.91042 | 2.1876 | 479.28 |
| 340 | 752.73 | -209.88 | -176.67 | -1.3961 | 0.91046 | 2.2143 | 460.05 |
| 345 | 727.58 | -199.90 | -165.54 | -1.3636 | 0.91032 | 2.2369 | 442.23 |
| 350 | 702.22 | -189.91 | -154.31 | -1.3313 | 0.90989 | 2.2525 | 425.97 |
| 360 | 651.72 | -170.10 | -131.74 | -1.2677 | 0.90829 | 2.2554 | 398.41 |
| 370 | 603.10 | -150.79 | -109.34 | -1.2064 | 0.90620 | 2.2187 | 377.41 |
| 380 | 557.99 | -132.28 | -87.474 | -1.1480 | 0.90373 | 2.1495 | 362.54 |
| 390 | 517.36 | -114.74 | -66.415 | -1.0933 | 0.90075 | 2.0598 | 352.86 |
| 400 | 481.55 | -98.223 | -46.307 | -1.0424 | 0.89744 | 1.9613 | 347.18 |
| 410 | 450.35 | -82.696 | -27.183 | -0.99520 | 0.89418 | 1.8644 | 344.41 |
| 420 | 423.27 | -68.058 | -8.9932 | -0.95136 | 0.89131 | 1.7753 | 343.67 |
| 430 | 399.72 | -54.187 | 8.3578 | -0.91053 | 0.88902 | 1.6967 | 344.32 |
| 440 | 379.13 | -40.963 | 24.978 | -0.87232 | 0.88742 | 1.6290 | 345.93 |
| 450 | 361.01 | -28.279 | 40.971 | -0.83637 | 0.88650 | 1.5713 | 348.19 |
| 460 | 344.95 | -16.042 | 56.432 | -0.80239 | 0.88624 | 1.5222 | 350.90 |
| 470 | 330.61 | -4.1769 | 71.440 | -0.77011 | 0.88657 | 1.4806 | 353.92 |
| 480 | 317.72 | 7.3809 | 86.066 | -0.73932 | 0.88744 | 1.4453 | 357.14 |
| 490 | 306.07 | 18.683 | 100.36 | -0.70983 | 0.88878 | 1.4153 | 360.51 |
| 500 | 295.46 | 29.772 | 114.39 | -0.68150 | 0.89052 | 1.3897 | 363.96 |
| 525 | 272.64 | 56.782 | 148.48 | -0.61496 | 0.89633 | 1.3407 | 372.76 |
| 550 | 253.87 | 83.077 | 181.55 | -0.55341 | 0.90365 | 1.3073 | 381.59 |
| 575 | 238.08 | 108.92 | 213.93 | -0.49583 | 0.91195 | 1.2845 | 390.28 |
| 600 | 224.54 | 134.50 | 245.84 | -0.44152 | 0.92086 | 1.2689 | 398.77 |
| 625 | 212.77 | 159.92 | 277.42 | -0.38994 | 0.93012 | 1.2586 | 407.04 |
| 650 | 202.40 | 185.28 | 308.80 | -0.34072 | 0.93954 | 1.2520 | 415.08 |
| 675 | 193.18 | 210.63 | 340.05 | -0.29354 | 0.94899 | 1.2483 | 422.90 |
| 700 | 184.90 | 236.02 | 371.23 | -0.24818 | 0.95838 | 1.2465 | 430.51 |
| 800 | 158.65 | 338.44 | 496.02 | -0.08156 | 0.99409 | 1.2516 | 459.06 |
| 900 | 139.62 | 442.77 | 621.83 | 0.06661 | 1.0258 | 1.2653 | 485.14 |
| 1000 | 125.04 | 549.19 | 749.14 | 0.20073 | 1.0532 | 1.2810 | 509.32 |
| 1100 | 113.42 | 657.58 | 878.01 | 0.32355 | 1.0766 | 1.2964 | 531.99 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | <i>c_v</i> [kJ/(kg K)] | <i>c_p</i> [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|-------------------------------------|-------------------------------------|-------------------------|
| 30.00 MPa Isobar | | | | | | | |
| 222.715 ^b | 1211.77 | -430.02 | -405.26 | -2.2321 | 0.99332 | 1.8259 | 1083.4 |
| 225 | 1205.06 | -425.99 | -401.09 | -2.2135 | 0.98964 | 1.8251 | 1070.6 |
| 230 | 1190.25 | -417.17 | -391.97 | -2.1734 | 0.98193 | 1.8241 | 1043.0 |
| 235 | 1175.29 | -408.37 | -382.85 | -2.1342 | 0.97467 | 1.8242 | 1015.8 |
| 240 | 1160.15 | -399.58 | -373.72 | -2.0958 | 0.96786 | 1.8254 | 988.76 |
| 245 | 1144.83 | -390.80 | -364.59 | -2.0581 | 0.96147 | 1.8277 | 962.05 |
| 250 | 1129.30 | -382.01 | -355.45 | -2.0211 | 0.95550 | 1.8311 | 935.59 |
| 255 | 1113.55 | -373.22 | -346.28 | -1.9848 | 0.94994 | 1.8355 | 909.37 |
| 260 | 1097.57 | -364.42 | -337.09 | -1.9491 | 0.94478 | 1.8410 | 883.41 |
| 265 | 1081.34 | -355.61 | -327.87 | -1.9140 | 0.94000 | 1.8475 | 857.70 |
| 270 | 1064.86 | -346.78 | -318.61 | -1.8794 | 0.93559 | 1.8550 | 832.25 |
| 275 | 1048.09 | -337.94 | -309.32 | -1.8453 | 0.93153 | 1.8635 | 807.08 |
| 280 | 1031.04 | -329.07 | -299.97 | -1.8116 | 0.92783 | 1.8729 | 782.21 |
| 285 | 1013.68 | -320.18 | -290.58 | -1.7784 | 0.92446 | 1.8831 | 757.65 |
| 290 | 996.01 | -311.26 | -281.14 | -1.7456 | 0.92145 | 1.8942 | 733.44 |
| 295 | 978.02 | -302.32 | -271.64 | -1.7131 | 0.91882 | 1.9060 | 709.61 |
| 300 | 959.70 | -293.34 | -262.08 | -1.6809 | 0.91659 | 1.9186 | 686.21 |
| 305 | 941.04 | -284.33 | -252.45 | -1.6491 | 0.91471 | 1.9322 | 663.31 |
| 310 | 922.04 | -275.29 | -242.76 | -1.6176 | 0.91301 | 1.9464 | 640.96 |
| 315 | 902.69 | -266.22 | -232.99 | -1.5863 | 0.91135 | 1.9610 | 619.20 |
| 320 | 883.00 | -257.12 | -223.15 | -1.5553 | 0.90973 | 1.9756 | 598.05 |
| 325 | 862.99 | -248.00 | -213.23 | -1.5246 | 0.90830 | 1.9899 | 577.56 |
| 330 | 842.66 | -238.85 | -203.25 | -1.4941 | 0.90721 | 2.0041 | 557.78 |
| 335 | 822.06 | -229.69 | -193.19 | -1.4639 | 0.90648 | 2.0179 | 538.80 |
| 340 | 801.21 | -220.51 | -183.07 | -1.4339 | 0.90599 | 2.0312 | 520.72 |
| 345 | 780.17 | -211.34 | -172.88 | -1.4041 | 0.90560 | 2.0432 | 503.62 |
| 350 | 758.98 | -202.17 | -162.64 | -1.3746 | 0.90520 | 2.0529 | 487.58 |
| 360 | 716.55 | -183.92 | -142.05 | -1.3166 | 0.90427 | 2.0618 | 458.95 |
| 370 | 674.75 | -165.93 | -121.47 | -1.2602 | 0.90323 | 2.0517 | 435.21 |
| 380 | 634.51 | -148.37 | -101.09 | -1.2059 | 0.90215 | 2.0224 | 416.28 |
| 390 | 596.59 | -131.36 | -81.073 | -1.1539 | 0.90099 | 1.9781 | 401.73 |
| 400 | 561.50 | -114.99 | -61.559 | -1.1045 | 0.89970 | 1.9233 | 390.99 |
| 410 | 529.46 | -99.289 | -42.627 | -1.0577 | 0.89833 | 1.8625 | 383.45 |
| 420 | 500.50 | -84.257 | -24.317 | -1.0136 | 0.89698 | 1.7995 | 378.49 |
| 430 | 474.48 | -69.860 | -6.6324 | -0.97200 | 0.89581 | 1.7378 | 375.55 |
| 440 | 451.16 | -56.044 | 10.452 | -0.93272 | 0.89494 | 1.6799 | 374.14 |
| 450 | 430.25 | -42.746 | 26.982 | -0.89557 | 0.89446 | 1.6270 | 373.89 |
| 460 | 411.46 | -29.901 | 43.010 | -0.86034 | 0.89440 | 1.5796 | 374.49 |
| 470 | 394.52 | -17.449 | 58.593 | -0.82682 | 0.89476 | 1.5378 | 375.74 |
| 480 | 379.18 | -5.3349 | 73.783 | -0.79484 | 0.89554 | 1.5011 | 377.47 |
| 490 | 365.24 | 6.4911 | 88.629 | -0.76423 | 0.89671 | 1.4689 | 379.56 |
| 500 | 352.51 | 18.071 | 103.18 | -0.73484 | 0.89824 | 1.4409 | 381.92 |
| 525 | 325.03 | 46.167 | 138.47 | -0.66595 | 0.90339 | 1.3857 | 388.60 |
| 550 | 302.37 | 73.376 | 172.59 | -0.60245 | 0.91002 | 1.3465 | 395.90 |
| 575 | 283.31 | 99.995 | 205.89 | -0.54324 | 0.91767 | 1.3187 | 403.46 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 30.00 MPa Isobar | | | | | | | |
| 600 | 266.99 | 126.23 | 238.59 | -0.48756 | 0.92601 | 1.2990 | 411.10 |
| 625 | 252.82 | 152.22 | 270.88 | -0.43483 | 0.93476 | 1.2852 | 418.70 |
| 650 | 240.36 | 178.08 | 302.89 | -0.38462 | 0.94374 | 1.2757 | 426.21 |
| 675 | 229.30 | 203.86 | 334.70 | -0.33660 | 0.95281 | 1.2695 | 433.60 |
| 700 | 219.39 | 229.64 | 366.38 | -0.29051 | 0.96185 | 1.2657 | 440.86 |
| 800 | 188.05 | 333.24 | 492.77 | -0.12174 | 0.99658 | 1.2650 | 468.48 |
| 900 | 165.44 | 438.40 | 619.73 | 0.02779 | 1.0277 | 1.2752 | 494.02 |
| 1000 | 148.15 | 545.42 | 747.91 | 0.16283 | 1.0547 | 1.2887 | 517.84 |
| 1100 | 134.40 | 654.27 | 877.48 | 0.28631 | 1.0778 | 1.3026 | 540.25 |
| 40.00 MPa Isobar | | | | | | | |
| 224.715 ^b | 1221.12 | -430.49 | -397.73 | -2.2352 | 0.99675 | 1.7975 | 1116.0 |
| 225 | 1220.33 | -429.99 | -397.22 | -2.2329 | 0.99628 | 1.7973 | 1114.5 |
| 230 | 1206.41 | -421.40 | -388.24 | -2.1935 | 0.98829 | 1.7937 | 1088.7 |
| 235 | 1192.39 | -412.82 | -379.28 | -2.1549 | 0.98078 | 1.7910 | 1063.3 |
| 240 | 1178.27 | -404.28 | -370.33 | -2.1172 | 0.97373 | 1.7892 | 1038.2 |
| 245 | 1164.03 | -395.75 | -361.39 | -2.0804 | 0.96713 | 1.7881 | 1013.4 |
| 250 | 1149.68 | -387.24 | -352.45 | -2.0442 | 0.96096 | 1.7877 | 988.91 |
| 255 | 1135.19 | -378.74 | -343.51 | -2.0088 | 0.95520 | 1.7881 | 964.76 |
| 260 | 1120.58 | -370.26 | -334.56 | -1.9741 | 0.94983 | 1.7892 | 940.93 |
| 265 | 1105.83 | -361.79 | -325.61 | -1.9400 | 0.94484 | 1.7908 | 917.41 |
| 270 | 1090.93 | -353.32 | -316.65 | -1.9065 | 0.94022 | 1.7931 | 894.22 |
| 275 | 1075.88 | -344.86 | -307.68 | -1.8736 | 0.93594 | 1.7959 | 871.38 |
| 280 | 1060.68 | -336.41 | -298.69 | -1.8412 | 0.93198 | 1.7991 | 848.90 |
| 285 | 1045.33 | -327.96 | -289.69 | -1.8093 | 0.92835 | 1.8027 | 826.79 |
| 290 | 1029.82 | -319.51 | -280.67 | -1.7779 | 0.92502 | 1.8066 | 805.09 |
| 295 | 1014.16 | -311.07 | -271.62 | -1.7470 | 0.92201 | 1.8108 | 783.81 |
| 300 | 998.35 | -302.62 | -262.56 | -1.7166 | 0.91930 | 1.8152 | 762.99 |
| 305 | 982.39 | -294.19 | -253.47 | -1.6865 | 0.91688 | 1.8198 | 742.65 |
| 310 | 966.29 | -285.76 | -244.36 | -1.6569 | 0.91467 | 1.8245 | 722.85 |
| 315 | 950.05 | -277.33 | -235.23 | -1.6277 | 0.91261 | 1.8291 | 703.59 |
| 320 | 933.68 | -268.91 | -226.07 | -1.5988 | 0.91069 | 1.8334 | 684.89 |
| 325 | 917.21 | -260.50 | -216.89 | -1.5704 | 0.90894 | 1.8375 | 666.75 |
| 330 | 900.63 | -252.11 | -207.70 | -1.5423 | 0.90743 | 1.8412 | 649.20 |
| 335 | 883.97 | -243.73 | -198.48 | -1.5146 | 0.90618 | 1.8444 | 632.25 |
| 340 | 867.25 | -235.37 | -189.25 | -1.4872 | 0.90518 | 1.8473 | 615.94 |
| 345 | 850.50 | -227.04 | -180.01 | -1.4602 | 0.90437 | 1.8497 | 600.32 |
| 350 | 833.72 | -218.73 | -170.76 | -1.4336 | 0.90369 | 1.8514 | 585.39 |
| 360 | 800.23 | -202.22 | -152.23 | -1.3814 | 0.90261 | 1.8525 | 557.71 |
| 370 | 767.03 | -185.87 | -133.72 | -1.3307 | 0.90182 | 1.8492 | 533.02 |
| 380 | 734.39 | -169.74 | -115.27 | -1.2815 | 0.90130 | 1.8400 | 511.44 |
| 390 | 702.64 | -153.87 | -96.942 | -1.2339 | 0.90102 | 1.8242 | 493.01 |
| 400 | 672.08 | -138.32 | -78.806 | -1.1880 | 0.90094 | 1.8021 | 477.59 |
| 410 | 642.96 | -123.13 | -60.917 | -1.1438 | 0.90101 | 1.7750 | 464.90 |
| 420 | 615.44 | -108.31 | -43.316 | -1.1014 | 0.90123 | 1.7446 | 454.60 |
| 430 | 589.59 | -93.874 | -26.030 | -1.0607 | 0.90157 | 1.7123 | 446.38 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | <i>c_v</i> [kJ/(kg K)] | <i>c_p</i> [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|-------------------------------------|-------------------------------------|-------------------------|
| 40.00 MPa Isobar | | | | | | | |
| 440 | 565.45 | -79.814 | -9.0735 | -1.0217 | 0.90206 | 1.6790 | 439.96 |
| 450 | 542.98 | -66.118 | 7.5496 | -0.98436 | 0.90270 | 1.6457 | 435.07 |
| 460 | 522.12 | -52.769 | 23.842 | -0.94855 | 0.90351 | 1.6129 | 431.49 |
| 470 | 502.79 | 39.744 | 39.812 | 0.91420 | 0.90452 | 1.5814 | 429.01 |
| 480 | 484.89 | -27.017 | 55.476 | -0.88122 | 0.90574 | 1.5516 | 427.45 |
| 490 | 468.31 | -14.563 | 70.851 | -0.84952 | 0.90717 | 1.5238 | 426.63 |
| 500 | 452.94 | -2.3539 | 85.959 | -0.81899 | 0.90882 | 1.4981 | 426.42 |
| 525 | 419.10 | 27.259 | 122.70 | -0.74727 | 0.91383 | 1.4435 | 427.89 |
| 550 | 390.67 | 55.849 | 158.24 | -0.68114 | 0.91996 | 1.4013 | 431.27 |
| 575 | 366.46 | 83.699 | 192.85 | -0.61959 | 0.92697 | 1.3692 | 435.81 |
| 600 | 345.60 | 111.02 | 226.76 | -0.56185 | 0.93462 | 1.3451 | 441.07 |
| 625 | 327.40 | 137.98 | 260.16 | -0.50733 | 0.94271 | 1.3271 | 446.76 |
| 650 | 311.36 | 164.69 | 293.16 | -0.45555 | 0.95107 | 1.3139 | 452.71 |
| 675 | 297.09 | 191.24 | 325.88 | -0.40615 | 0.95957 | 1.3043 | 458.80 |
| 700 | 284.29 | 217.70 | 358.40 | -0.35885 | 0.96810 | 1.2975 | 464.97 |
| 800 | 243.83 | 323.44 | 487.49 | -0.18646 | 1.0012 | 1.2880 | 489.58 |
| 900 | 214.66 | 430.11 | 616.45 | -0.03457 | 1.0313 | 1.2926 | 513.34 |
| 1000 | 192.37 | 538.25 | 746.18 | 0.10210 | 1.0575 | 1.3024 | 535.98 |
| 1100 | 174.67 | 647.97 | 876.98 | 0.22676 | 1.0802 | 1.3137 | 557.53 |
| 50.00 MPa Isobar | | | | | | | |
| 226.679 ^b | 1229.78 | -430.78 | -390.13 | -2.2377 | 0.99951 | 1.7735 | 1146.9 |
| 230 | 1221.01 | -425.19 | -384.24 | -2.2119 | 0.99412 | 1.7700 | 1130.8 |
| 235 | 1207.74 | -416.81 | -375.41 | -2.1739 | 0.98640 | 1.7654 | 1106.8 |
| 240 | 1194.42 | -408.45 | -366.59 | -2.1368 | 0.97918 | 1.7615 | 1083.2 |
| 245 | 1181.04 | -400.13 | -357.79 | -2.1005 | 0.97242 | 1.7582 | 1059.9 |
| 250 | 1167.59 | -391.83 | -349.01 | -2.0650 | 0.96609 | 1.7556 | 1037.0 |
| 255 | 1154.07 | -383.56 | -340.23 | -2.0303 | 0.96020 | 1.7534 | 1014.4 |
| 260 | 1140.47 | -375.31 | -331.47 | -1.9962 | 0.95470 | 1.7518 | 992.10 |
| 265 | 1126.80 | -367.09 | -322.71 | -1.9629 | 0.94958 | 1.7507 | 970.17 |
| 270 | 1113.05 | -358.88 | -313.96 | -1.9301 | 0.94483 | 1.7500 | 948.60 |
| 275 | 1099.22 | -350.70 | -305.21 | -1.8980 | 0.94042 | 1.7496 | 927.39 |
| 280 | 1085.32 | -342.53 | -296.47 | -1.8665 | 0.93634 | 1.7496 | 906.55 |
| 285 | 1071.33 | -334.39 | -287.72 | -1.8355 | 0.93257 | 1.7498 | 886.10 |
| 290 | 1057.27 | -326.26 | -278.97 | -1.8051 | 0.92910 | 1.7502 | 866.05 |
| 295 | 1043.14 | -318.15 | -270.21 | -1.7752 | 0.92592 | 1.7507 | 846.42 |
| 300 | 1028.94 | -310.05 | -261.46 | -1.7458 | 0.92303 | 1.7514 | 827.23 |
| 305 | 1014.67 | -301.98 | -252.70 | -1.7168 | 0.92039 | 1.7521 | 808.50 |
| 310 | 1000.35 | -293.92 | -243.94 | -1.6883 | 0.91799 | 1.7527 | 790.25 |
| 315 | 985.97 | -285.88 | -235.17 | -1.6603 | 0.91578 | 1.7533 | 772.50 |
| 320 | 971.55 | -277.87 | -226.41 | -1.6326 | 0.91376 | 1.7538 | 755.25 |
| 325 | 957.10 | -269.88 | -217.64 | -1.6055 | 0.91193 | 1.7540 | 738.51 |
| 330 | 942.63 | -261.91 | -208.87 | -1.5787 | 0.91030 | 1.7539 | 722.28 |
| 335 | 928.14 | -253.97 | -200.10 | -1.5523 | 0.90890 | 1.7536 | 706.59 |
| 340 | 913.66 | -246.06 | -191.33 | -1.5263 | 0.90769 | 1.7529 | 691.43 |
| 345 | 899.19 | -238.17 | -182.57 | -1.5007 | 0.90668 | 1.7520 | 676.84 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 50.00 MPa Isobar | | | | | | | |
| 350 | 884.76 | -230.32 | -173.81 | -1.4755 | 0.90581 | 1.7507 | 662.81 |
| 360 | 856.03 | -214.73 | -156.32 | -1.4263 | 0.90448 | 1.7469 | 636.48 |
| 370 | 827.61 | -199.29 | -138.88 | -1.3785 | 0.90360 | 1.7414 | 612.45 |
| 380 | 799.62 | -184.03 | -121.50 | -1.3321 | 0.90311 | 1.7340 | 590.70 |
| 390 | 772.18 | -168.96 | -104.21 | -1.2872 | 0.90297 | 1.7243 | 571.22 |
| 400 | 745.45 | -154.10 | -87.024 | -1.2437 | 0.90314 | 1.7120 | 554.02 |
| 410 | 719.54 | -139.47 | -69.977 | -1.2016 | 0.90357 | 1.6970 | 539.02 |
| 420 | 694.59 | -125.08 | -53.092 | -1.1609 | 0.90423 | 1.6796 | 526.11 |
| 430 | 670.67 | -110.94 | -36.392 | -1.1216 | 0.90508 | 1.6602 | 515.13 |
| 440 | 647.87 | -97.069 | -19.893 | -1.0837 | 0.90612 | 1.6394 | 505.87 |
| 450 | 626.20 | -83.452 | -3.6055 | -1.0471 | 0.90732 | 1.6180 | 498.11 |
| 460 | 605.67 | -70.087 | 12.466 | 1.0118 | 0.90868 | 1.5964 | 491.68 |
| 470 | 586.26 | -56.964 | 28.322 | -0.97766 | 0.91018 | 1.5749 | 486.40 |
| 480 | 567.95 | -44.071 | 43.965 | -0.94473 | 0.91184 | 1.5538 | 482.14 |
| 490 | 550.68 | -31.396 | 59.400 | -0.91290 | 0.91363 | 1.5333 | 478.77 |
| 500 | 534.42 | -18.926 | 74.634 | -0.88213 | 0.91557 | 1.5136 | 476.18 |
| 525 | 497.78 | 11.454 | 111.90 | -0.80939 | 0.92101 | 1.4687 | 472.48 |
| 550 | 466.18 | 40.875 | 148.13 | -0.74197 | 0.92723 | 1.4308 | 471.73 |
| 575 | 438.78 | 69.547 | 183.50 | -0.67907 | 0.93410 | 1.3999 | 472.96 |
| 600 | 414.84 | 97.651 | 218.18 | -0.62003 | 0.94148 | 1.3753 | 475.52 |
| 625 | 393.77 | 125.33 | 252.31 | -0.56429 | 0.94924 | 1.3561 | 479.00 |
| 650 | 375.06 | 152.71 | 286.02 | -0.51141 | 0.95724 | 1.3412 | 483.09 |
| 675 | 358.33 | 179.87 | 319.40 | -0.46101 | 0.96537 | 1.3300 | 487.62 |
| 700 | 343.27 | 206.88 | 352.54 | -0.41281 | 0.97355 | 1.3215 | 492.43 |
| 800 | 295.34 | 314.44 | 483.74 | -0.23759 | 1.0055 | 1.3064 | 513.16 |
| 900 | 260.55 | 422.42 | 614.33 | -0.08378 | 1.0347 | 1.3070 | 534.47 |
| 1000 | 233.89 | 531.57 | 745.34 | 0.05425 | 1.0603 | 1.3140 | 555.44 |
| 1100 | 212.66 | 642.08 | 877.19 | 0.17991 | 1.0825 | 1.3232 | 575.78 |
| 75.00 MPa Isobar | | | | | | | |
| 231.448 ^b | 1249.06 | -430.98 | -370.94 | -2.2420 | 1.0049 | 1.7265 | 1217.6 |
| 235 | 1240.63 | -425.27 | -364.81 | -2.2157 | 0.99929 | 1.7213 | 1202.5 |
| 240 | 1228.76 | -417.26 | -356.22 | -2.1795 | 0.99178 | 1.7146 | 1181.5 |
| 245 | 1216.90 | -409.30 | -347.67 | -2.1442 | 0.98477 | 1.7083 | 1160.9 |
| 250 | 1205.04 | -401.38 | -339.14 | -2.1098 | 0.97824 | 1.7025 | 1140.6 |
| 255 | 1193.18 | -393.50 | -330.64 | -2.0761 | 0.97215 | 1.6972 | 1120.6 |
| 260 | 1181.32 | -385.66 | -322.17 | -2.0432 | 0.96649 | 1.6922 | 1101.0 |
| 265 | 1169.46 | -377.85 | -313.72 | -2.0110 | 0.96122 | 1.6876 | 1081.7 |
| 270 | 1157.60 | -370.08 | -305.29 | -1.9795 | 0.95633 | 1.6833 | 1062.7 |
| 275 | 1145.74 | -362.34 | -296.88 | -1.9487 | 0.95179 | 1.6793 | 1044.1 |
| 280 | 1133.89 | -354.64 | -288.50 | -1.9184 | 0.94758 | 1.6756 | 1025.9 |
| 285 | 1122.04 | -346.97 | -280.13 | -1.8888 | 0.94369 | 1.6720 | 1008.0 |
| 290 | 1110.20 | -339.33 | -271.78 | -1.8598 | 0.94010 | 1.6687 | 990.43 |
| 295 | 1098.37 | -331.72 | -263.44 | -1.8313 | 0.93680 | 1.6654 | 973.27 |
| 300 | 1086.56 | -324.15 | -255.12 | -1.8033 | 0.93376 | 1.6623 | 956.50 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|--------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 75.00 MPa Isobar | | | | | | | |
| 305 | 1074.76 | -316.60 | -246.82 | -1.7759 | 0.93097 | 1.6593 | 940.12 |
| 310 | 1062.97 | -309.09 | -238.53 | -1.7489 | 0.92843 | 1.6563 | 924.14 |
| 315 | 1051.22 | -301.60 | -230.25 | -1.7224 | 0.92610 | 1.6534 | 908.56 |
| 320 | 1039.49 | -294.15 | -222.00 | -1.6964 | 0.92399 | 1.6504 | 893.38 |
| 325 | 1027.79 | -286.72 | -213.75 | -1.6708 | 0.92208 | 1.6474 | 878.62 |
| 330 | 1016.13 | -279.33 | -205.52 | -1.6457 | 0.92037 | 1.6444 | 864.28 |
| 335 | 1004.51 | -271.97 | -197.31 | -1.6210 | 0.91884 | 1.6413 | 850.35 |
| 340 | 992.95 | -264.64 | -189.11 | -1.5967 | 0.91750 | 1.6381 | 836.84 |
| 345 | 981.43 | -257.35 | -180.93 | -1.5728 | 0.91632 | 1.6348 | 823.75 |
| 350 | 969.98 | -250.08 | -172.76 | -1.5493 | 0.91530 | 1.6314 | 811.08 |
| 360 | 947.28 | -235.66 | -156.48 | -1.5035 | 0.91369 | 1.6244 | 787.00 |
| 370 | 924.90 | -221.36 | -140.27 | -1.4591 | 0.91262 | 1.6170 | 764.58 |
| 380 | 902.87 | -207.21 | -124.14 | -1.4160 | 0.91202 | 1.6091 | 743.77 |
| 390 | 881.23 | -193.20 | -108.09 | -1.3744 | 0.91184 | 1.6009 | 724.52 |
| 400 | 860.03 | -179.33 | -92.126 | -1.3339 | 0.91204 | 1.5924 | 706.78 |
| 410 | 839.31 | -165.61 | -76.246 | -1.2947 | 0.91258 | 1.5836 | 690.47 |
| 420 | 819.07 | -152.02 | -60.456 | -1.2567 | 0.91342 | 1.5745 | 675.53 |
| 430 | 799.37 | -138.58 | -44.757 | -1.2197 | 0.91452 | 1.5652 | 661.90 |
| 440 | 780.21 | -125.28 | -29.152 | -1.1838 | 0.91585 | 1.5557 | 649.53 |
| 450 | 761.62 | -112.12 | -13.843 | -1.1490 | 0.91738 | 1.5460 | 638.34 |
| 460 | 743.60 | -99.093 | 1.7669 | -1.1151 | 0.91910 | 1.5360 | 628.29 |
| 470 | 726.18 | -86.204 | 17.076 | -1.0822 | 0.92098 | 1.5258 | 619.31 |
| 480 | 709.36 | -73.446 | 32.283 | -1.0502 | 0.92300 | 1.5155 | 611.32 |
| 490 | 693.14 | -60.816 | 47.387 | -1.0190 | 0.92515 | 1.5052 | 604.25 |
| 500 | 677.52 | -48.311 | 62.387 | -0.98873 | 0.92742 | 1.4949 | 598.02 |
| 525 | 641.03 | -17.555 | 99.444 | -0.91641 | 0.93352 | 1.4699 | 585.62 |
| 550 | 608.02 | 12.545 | 135.90 | -0.84857 | 0.94012 | 1.4468 | 576.92 |
| 575 | 578.19 | 42.085 | 171.80 | -0.78473 | 0.94711 | 1.4260 | 571.08 |
| 600 | 551.22 | 71.156 | 207.22 | -0.72443 | 0.95439 | 1.4077 | 567.48 |
| 625 | 526.81 | 99.843 | 242.21 | -0.66730 | 0.96187 | 1.3920 | 565.64 |
| 650 | 504.66 | 128.22 | 276.84 | -0.61297 | 0.96949 | 1.3786 | 565.16 |
| 675 | 484.49 | 156.36 | 311.16 | -0.56116 | 0.97717 | 1.3675 | 565.73 |
| 700 | 466.06 | 184.31 | 345.23 | -0.51159 | 0.98486 | 1.3585 | 567.11 |
| 800 | 405.95 | 295.12 | 479.87 | -0.33177 | 1.0149 | 1.3379 | 577.61 |
| 900 | 361.14 | 405.66 | 613.33 | -0.17457 | 1.0424 | 1.3330 | 592.07 |
| 1000 | 326.23 | 516.83 | 746.72 | -0.03403 | 1.0668 | 1.3356 | 608.08 |
| 1100 | 298.11 | 628.97 | 880.55 | 0.09352 | 1.0880 | 1.3414 | 624.65 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | <i>c_v</i> [kJ/(kg K)] | <i>c_p</i> [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|-------------------------------------|-------------------------------------|-------------------------|
| 100.00 MPa Isobar | | | | | | | |
| 236.031 ^b | 1265.83 | -430.62 | -351.62 | -2.2443 | 1.0097 | 1.6919 | 1280.4 |
| 240 | 1257.21 | -424.46 | -344.92 | -2.2162 | 1.0037 | 1.6854 | 1265.1 |
| 245 | 1246.37 | -416.74 | -336.51 | -2.1815 | 0.99659 | 1.6778 | 1246.2 |
| 250 | 1235.57 | -409.07 | -328.14 | -2.1477 | 0.98997 | 1.6706 | 1227.6 |
| 255 | 1224.80 | -401.45 | -319.80 | -2.1147 | 0.98383 | 1.6637 | 1209.4 |
| 260 | 1214.06 | -393.87 | -311.50 | -2.0824 | 0.97812 | 1.6573 | 1191.4 |
| 265 | 1203.36 | -386.33 | -303.23 | -2.0509 | 0.97282 | 1.6512 | 1173.7 |
| 270 | 1192.69 | -378.83 | -294.99 | -2.0201 | 0.96790 | 1.6454 | 1156.4 |
| 275 | 1182.06 | -371.37 | -286.77 | -1.9900 | 0.96335 | 1.6399 | 1139.3 |
| 280 | 1171.46 | -363.95 | -278.59 | -1.9605 | 0.95913 | 1.6347 | 1122.6 |
| 285 | 1160.90 | -356.57 | -270.43 | -1.9316 | 0.95524 | 1.6297 | 1106.2 |
| 290 | 1150.37 | -349.22 | -262.29 | -1.9033 | 0.95164 | 1.6249 | 1090.2 |
| 295 | 1139.89 | -341.90 | -254.18 | -1.8755 | 0.94833 | 1.6203 | 1074.5 |
| 300 | 1129.45 | -334.63 | -246.09 | -1.8484 | 0.94528 | 1.6158 | 1059.1 |
| 305 | 1119.04 | -327.38 | -238.02 | -1.8217 | 0.94249 | 1.6115 | 1044.0 |
| 310 | 1108.69 | -320.17 | -229.97 | -1.7955 | 0.93993 | 1.6073 | 1029.3 |
| 315 | 1098.38 | -312.99 | -221.94 | -1.7698 | 0.93760 | 1.6032 | 1015.0 |
| 320 | 1088.12 | -305.84 | -213.94 | -1.7446 | 0.93548 | 1.5992 | 1001.0 |
| 325 | 1077.91 | -298.72 | -205.95 | -1.7198 | 0.93356 | 1.5953 | 987.36 |
| 330 | 1067.76 | -291.64 | -197.99 | -1.6955 | 0.93183 | 1.5914 | 974.07 |
| 335 | 1057.66 | -284.59 | -190.04 | -1.6716 | 0.93028 | 1.5876 | 961.13 |
| 340 | 1047.62 | -277.56 | -182.11 | -1.6481 | 0.92891 | 1.5838 | 948.54 |
| 345 | 1037.64 | -270.57 | -174.20 | -1.6250 | 0.92769 | 1.5800 | 936.31 |
| 350 | 1027.73 | -263.61 | -166.31 | -1.6023 | 0.92663 | 1.5762 | 924.42 |
| 360 | 1008.12 | -249.78 | -150.58 | -1.5580 | 0.92495 | 1.5687 | 901.70 |
| 370 | 988.80 | -236.07 | -134.93 | -1.5151 | 0.92378 | 1.5612 | 880.34 |
| 380 | 969.80 | -222.47 | -119.36 | -1.4736 | 0.92309 | 1.5537 | 860.31 |
| 390 | 951.13 | -209.00 | -103.86 | -1.4333 | 0.92283 | 1.5461 | 841.58 |
| 400 | 932.81 | -195.64 | -88.438 | -1.3943 | 0.92295 | 1.5386 | 824.08 |
| 410 | 914.87 | -182.39 | -73.089 | -1.3564 | 0.92341 | 1.5311 | 807.78 |
| 420 | 897.31 | -169.26 | -57.815 | -1.3196 | 0.92418 | 1.5237 | 792.60 |
| 430 | 880.14 | -156.23 | -42.614 | -1.2838 | 0.92522 | 1.5164 | 778.51 |
| 440 | 863.37 | -143.31 | -27.486 | -1.2490 | 0.92650 | 1.5092 | 765.42 |
| 450 | 847.00 | -130.49 | -12.430 | -1.2152 | 0.92801 | 1.5021 | 753.30 |
| 460 | 831.05 | -117.77 | 2.5559 | -1.1823 | 0.92970 | 1.4952 | 742.08 |
| 470 | 815.51 | -105.15 | 17.473 | -1.1502 | 0.93157 | 1.4884 | 731.73 |
| 480 | 800.39 | -92.616 | 32.324 | -1.1189 | 0.93359 | 1.4817 | 722.18 |
| 490 | 785.67 | -80.171 | 47.108 | -1.0884 | 0.93574 | 1.4752 | 713.39 |
| 500 | 771.37 | -67.812 | 61.828 | -1.0587 | 0.93801 | 1.4688 | 705.34 |
| 525 | 737.38 | -37.261 | 98.354 | -0.98741 | 0.94412 | 1.4534 | 688.12 |
| 550 | 705.86 | -7.1663 | 134.50 | 0.92014 | 0.95070 | 1.4388 | 674.60 |
| 575 | 676.71 | 22.527 | 170.30 | -0.85649 | 0.95763 | 1.4251 | 664.18 |
| 600 | 649.77 | 51.872 | 205.77 | -0.79610 | 0.96480 | 1.4127 | 656.31 |
| 625 | 624.90 | 80.921 | 240.95 | -0.73867 | 0.97211 | 1.4016 | 650.49 |
| 650 | 601.91 | 109.72 | 275.86 | -0.68389 | 0.97951 | 1.3918 | 646.36 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 100.00 MPa Isobar | | | | | | | |
| 675 | 580.64 | 138.32 | 310.55 | -0.63153 | 0.98693 | 1.3833 | 643.59 |
| 700 | 560.93 | 166.76 | 345.04 | -0.58135 | 0.99434 | 1.3760 | 641.95 |
| 800 | 494.96 | 279.54 | 481.58 | -0.39900 | 1.0231 | 1.3573 | 643.10 |
| 900 | 444.32 | 391.83 | 616.89 | -0.23962 | 1.0494 | 1.3505 | 651.25 |
| 1000 | 404.15 | 504.47 | 751.91 | -0.09737 | 1.0728 | 1.3507 | 662.59 |
| 1100 | 371.36 | 617.86 | 887.14 | 0.03152 | 1.0931 | 1.3544 | 675.48 |
| 200.00 MPa Isobar | | | | | | | |
| 252.864 ^b | 1318.45 | -426.12 | -274.43 | -2.2449 | 1.0320 | 1.6131 | 1476.5 |
| 255 | 1314.84 | -423.09 | -270.99 | -2.2314 | 1.0295 | 1.6096 | 1470.1 |
| 260 | 1306.44 | -416.05 | -262.96 | -2.2002 | 1.0240 | 1.6016 | 1455.4 |
| 265 | 1298.11 | -409.04 | -254.97 | -2.1697 | 1.0188 | 1.5940 | 1440.8 |
| 270 | 1289.84 | -402.08 | -247.02 | -2.1400 | 1.0141 | 1.5867 | 1426.6 |
| 275 | 1281.64 | -395.15 | -239.10 | -2.1110 | 1.0097 | 1.5797 | 1412.5 |
| 280 | 1273.50 | -388.27 | -231.22 | -2.0826 | 1.0057 | 1.5730 | 1398.7 |
| 285 | 1265.43 | -381.42 | -223.37 | -2.0548 | 1.0020 | 1.5666 | 1385.1 |
| 290 | 1257.43 | -374.61 | -215.55 | -2.0276 | 0.99855 | 1.5604 | 1371.8 |
| 295 | 1249.48 | -367.83 | -207.77 | -2.0010 | 0.99539 | 1.5545 | 1358.7 |
| 300 | 1241.61 | -361.09 | -200.01 | -1.9749 | 0.99248 | 1.5488 | 1345.9 |
| 305 | 1233.79 | -354.38 | -192.28 | -1.9493 | 0.98981 | 1.5434 | 1333.3 |
| 310 | 1226.04 | -347.70 | -184.57 | -1.9243 | 0.98736 | 1.5381 | 1321.0 |
| 315 | 1218.35 | -341.05 | -176.90 | -1.8997 | 0.98512 | 1.5331 | 1308.9 |
| 320 | 1210.72 | -334.43 | -169.24 | -1.8756 | 0.98307 | 1.5282 | 1297.1 |
| 325 | 1203.16 | -327.84 | -161.61 | -1.8519 | 0.98121 | 1.5235 | 1285.5 |
| 330 | 1195.66 | -321.28 | -154.01 | -1.8287 | 0.97952 | 1.5190 | 1274.2 |
| 335 | 1188.22 | -314.74 | -146.42 | -1.8059 | 0.97799 | 1.5146 | 1263.1 |
| 340 | 1180.84 | -308.23 | -138.86 | -1.7835 | 0.97662 | 1.5104 | 1252.2 |
| 345 | 1173.53 | -301.75 | -131.32 | -1.7615 | 0.97539 | 1.5064 | 1241.6 |
| 350 | 1166.27 | -295.28 | -123.80 | -1.7398 | 0.97430 | 1.5025 | 1231.2 |
| 360 | 1151.94 | -282.43 | -108.81 | -1.6976 | 0.97249 | 1.4950 | 1211.2 |
| 370 | 1137.86 | -269.67 | -93.896 | -1.6568 | 0.97114 | 1.4880 | 1192.1 |
| 380 | 1124.01 | -256.98 | -79.049 | -1.6172 | 0.97020 | 1.4815 | 1173.9 |
| 390 | 1110.41 | -244.38 | -64.266 | -1.5788 | 0.96963 | 1.4753 | 1156.5 |
| 400 | 1097.04 | -231.85 | -49.543 | -1.5415 | 0.96940 | 1.4695 | 1140.0 |
| 410 | 1083.91 | -219.39 | -34.876 | -1.5053 | 0.96947 | 1.4640 | 1124.3 |
| 420 | 1071.02 | -207.00 | -20.262 | -1.4700 | 0.96981 | 1.4588 | 1109.4 |
| 430 | 1058.36 | -194.67 | -5.6992 | -1.4358 | 0.97040 | 1.4539 | 1095.3 |
| 440 | 1045.94 | -182.40 | 8.8159 | -1.4024 | 0.97121 | 1.4492 | 1081.9 |
| 450 | 1033.74 | -170.19 | 23.286 | -1.3699 | 0.97222 | 1.4448 | 1069.2 |
| 460 | 1021.78 | -158.02 | 37.713 | -1.3382 | 0.97341 | 1.4406 | 1057.1 |
| 470 | 1010.04 | -145.91 | 52.099 | -1.3072 | 0.97477 | 1.4367 | 1045.7 |
| 480 | 998.53 | -133.85 | 66.447 | -1.2770 | 0.97627 | 1.4329 | 1034.8 |
| 490 | 987.24 | -121.83 | 80.758 | -1.2475 | 0.97791 | 1.4294 | 1024.6 |
| 500 | 976.16 | -109.85 | 95.035 | -1.2187 | 0.97967 | 1.4260 | 1014.9 |
| 525 | 949.42 | -80.066 | 130.59 | -1.1493 | 0.98451 | 1.4185 | 992.79 |
| 550 | 923.96 | -50.491 | 165.97 | -1.0835 | 0.98986 | 1.4120 | 973.51 |
| 575 | 899.74 | -21.088 | 201.20 | -1.0208 | 0.99559 | 1.4065 | 956.68 |
| 600 | 876.69 | 8.1703 | 236.30 | -0.96106 | 1.0016 | 1.4019 | 942.00 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | <i>c_v</i> [kJ/(kg K)] | <i>c_p</i> [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|-------------------------------------|-------------------------------------|-------------------------|
| 200.00 MPa Isobar | | | | | | | |
| 625 | 854.75 | 37.312 | 271.30 | -0.90391 | 1.0078 | 1.3980 | 929.18 |
| 650 | 833.86 | 66.359 | 306.21 | -0.84915 | 1.0140 | 1.3948 | 918.02 |
| 675 | 813.97 | 95.331 | 341.04 | -0.79656 | 1.0204 | 1.3922 | 908.32 |
| 700 | 795.00 | 124.25 | 375.82 | -0.74597 | 1.0267 | 1.3900 | 899.91 |
| 800 | 727.46 | 239.61 | 514.53 | -0.56073 | 1.0513 | 1.3851 | 876.78 |
| 900 | 671.10 | 354.93 | 652.94 | -0.39771 | 1.0740 | 1.3836 | 865.84 |
| 1000 | 623.57 | 470.58 | 791.32 | -0.25192 | 1.0942 | 1.3841 | 862.60 |
| 1100 | 583.00 | 586.76 | 929.81 | -0.11992 | 1.1119 | 1.3860 | 864.16 |
| 400.00 MPa Isobar | | | | | | | |
| 281.544 ^b | 1392.45 | -410.72 | -123.46 | -2.2315 | 1.0894 | 1.5590 | 1732.5 |
| 285 | 1388.17 | -406.23 | -118.08 | -2.2125 | 1.0870 | 1.5546 | 1724.6 |
| 290 | 1382.04 | -399.75 | -110.32 | -2.1855 | 1.0838 | 1.5485 | 1713.3 |
| 295 | 1375.97 | -393.30 | -102.59 | -2.1591 | 1.0808 | 1.5426 | 1702.1 |
| 300 | 1369.95 | -386.88 | -94.895 | -2.1332 | 1.0780 | 1.5369 | 1691.2 |
| 305 | 1364.00 | -380.48 | -87.224 | -2.1078 | 1.0754 | 1.5314 | 1680.4 |
| 310 | 1358.11 | -374.11 | -79.581 | -2.0830 | 1.0729 | 1.5260 | 1669.9 |
| 315 | 1352.28 | -367.76 | -71.964 | -2.0586 | 1.0707 | 1.5209 | 1659.5 |
| 320 | 1346.50 | -361.44 | -64.371 | -2.0347 | 1.0686 | 1.5160 | 1649.3 |
| 325 | 1340.78 | 355.14 | 56.803 | 2.0112 | 1.0667 | 1.5112 | 1639.3 |
| 330 | 1335.11 | -348.86 | -49.259 | -1.9882 | 1.0650 | 1.5067 | 1629.5 |
| 335 | 1329.50 | -342.60 | -41.737 | -1.9656 | 1.0633 | 1.5022 | 1619.8 |
| 340 | 1323.95 | -336.36 | -34.236 | -1.9433 | 1.0618 | 1.4980 | 1610.3 |
| 345 | 1318.44 | -330.14 | -26.757 | -1.9215 | 1.0605 | 1.4939 | 1601.1 |
| 350 | 1312.99 | -323.94 | -19.297 | -1.9000 | 1.0592 | 1.4899 | 1591.9 |
| 360 | 1302.24 | -311.60 | -4.4362 | -1.8582 | 1.0570 | 1.4824 | 1574.2 |
| 370 | 1291.69 | -299.32 | 10.353 | -1.8177 | 1.0552 | 1.4754 | 1557.2 |
| 380 | 1281.33 | -287.10 | 25.074 | -1.7784 | 1.0537 | 1.4690 | 1540.8 |
| 390 | 1271.16 | -274.94 | 39.733 | -1.7403 | 1.0525 | 1.4630 | 1525.0 |
| 400 | 1261.17 | -262.83 | 54.335 | -1.7033 | 1.0516 | 1.4574 | 1509.8 |
| 410 | 1251.35 | -250.77 | 68.883 | -1.6674 | 1.0510 | 1.4522 | 1495.3 |
| 420 | 1241.70 | -238.76 | 83.381 | -1.6325 | 1.0506 | 1.4475 | 1481.2 |
| 430 | 1232.22 | -226.78 | 97.833 | -1.5985 | 1.0504 | 1.4430 | 1467.7 |
| 440 | 1222.89 | -214.85 | 112.24 | -1.5654 | 1.0503 | 1.4389 | 1454.8 |
| 450 | 1213.72 | -202.95 | 126.61 | -1.5331 | 1.0505 | 1.4352 | 1442.3 |
| 460 | 1204.70 | -191.08 | 140.95 | -1.5016 | 1.0508 | 1.4317 | 1430.3 |
| 470 | 1195.83 | -179.25 | 155.25 | -1.4708 | 1.0513 | 1.4285 | 1418.8 |
| 480 | 1187.10 | -167.44 | 169.52 | -1.4408 | 1.0519 | 1.4255 | 1407.7 |
| 490 | 1178.51 | -155.65 | 183.76 | -1.4114 | 1.0526 | 1.4228 | 1397.1 |
| 500 | 1170.05 | -143.89 | 197.97 | -1.3827 | 1.0534 | 1.4203 | 1386.9 |
| 525 | 1149.47 | -114.58 | 233.41 | -1.3135 | 1.0559 | 1.4149 | 1363.0 |
| 550 | 1129.67 | -85.361 | 268.72 | -1.2478 | 1.0588 | 1.4106 | 1341.4 |
| 575 | 1110.59 | -56.223 | 303.94 | -1.1852 | 1.0622 | 1.4072 | 1321.8 |
| 600 | 1092.21 | -27.143 | 339.09 | -1.1253 | 1.0659 | 1.4045 | 1304.1 |
| 625 | 1074.47 | 1.8990 | 374.18 | -1.0681 | 1.0698 | 1.4025 | 1288.1 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 400.00 MPa Isobar | | | | | | | |
| 650 | 1057.35 | 30.916 | 409.22 | -1.0131 | 1.0739 | 1.4011 | 1273.5 |
| 675 | 1040.82 | 59.921 | 444.23 | -0.96022 | 1.0781 | 1.4001 | 1260.4 |
| 700 | 1024.84 | 88.926 | 479.23 | -0.90931 | 1.0825 | 1.3995 | 1248.5 |
| 800 | 966.02 | 205.09 | 619.16 | -0.72246 | 1.0999 | 1.3997 | 1211.0 |
| 900 | 914.22 | 321.71 | 759.24 | -0.55747 | 1.1165 | 1.4023 | 1185.7 |
| 1000 | 868.27 | 438.97 | 899.65 | -0.40954 | 1.1316 | 1.4060 | 1168.7 |
| 1100 | 827.20 | 556.88 | 1040.44 | -0.27535 | 1.1451 | 1.4098 | 1157.6 |
| 600.00 MPa Isobar | | | | | | | |
| 305.996 ^b | 1448.66 | -391.42 | 22.754 | -2.2128 | 1.1462 | 1.5467 | 1910.7 |
| 310 | 1444.64 | -386.39 | 28.939 | -2.1927 | 1.1442 | 1.5427 | 1903.0 |
| 315 | 1439.67 | -380.12 | 36.640 | -2.1681 | 1.1419 | 1.5377 | 1893.5 |
| 320 | 1434.75 | -373.88 | 44.317 | -2.1439 | 1.1397 | 1.5329 | 1884.2 |
| 325 | 1429.88 | -367.65 | 51.970 | -2.1201 | 1.1376 | 1.5283 | 1875.1 |
| 330 | 1425.06 | -361.44 | 59.600 | -2.0969 | 1.1357 | 1.5238 | 1866.1 |
| 335 | 1420.28 | -355.24 | 67.208 | -2.0740 | 1.1338 | 1.5194 | 1857.3 |
| 340 | 1415.56 | -349.07 | 74.794 | -2.0515 | 1.1321 | 1.5152 | 1848.6 |
| 345 | 1410.88 | -342.91 | 82.360 | -2.0294 | 1.1305 | 1.5111 | 1840.1 |
| 350 | 1406.25 | -336.76 | 89.905 | -2.0077 | 1.1290 | 1.5071 | 1831.7 |
| 360 | 1397.12 | -324.52 | 104.94 | -1.9653 | 1.1263 | 1.4996 | 1815.4 |
| 370 | 1388.16 | -312.33 | 119.90 | -1.9243 | 1.1240 | 1.4925 | 1799.7 |
| 380 | 1379.38 | -300.19 | 134.79 | -1.8846 | 1.1219 | 1.4858 | 1784.5 |
| 390 | 1370.75 | -288.10 | 149.62 | -1.8461 | 1.1201 | 1.4796 | 1769.8 |
| 400 | 1362.28 | 276.05 | 164.38 | 1.8087 | 1.1186 | 1.4738 | 1755.6 |
| 410 | 1353.97 | -264.05 | 179.09 | -1.7724 | 1.1174 | 1.4683 | 1741.9 |
| 420 | 1345.79 | -252.08 | 193.75 | -1.7371 | 1.1163 | 1.4633 | 1728.7 |
| 430 | 1337.76 | -240.15 | 208.36 | -1.7027 | 1.1154 | 1.4585 | 1715.9 |
| 440 | 1329.87 | -228.25 | 222.92 | -1.6692 | 1.1147 | 1.4541 | 1703.6 |
| 450 | 1322.10 | -216.38 | 237.44 | -1.6366 | 1.1142 | 1.4500 | 1691.6 |
| 460 | 1314.46 | -204.54 | 251.92 | -1.6048 | 1.1139 | 1.4462 | 1680.1 |
| 470 | 1306.94 | -192.72 | 266.37 | -1.5737 | 1.1136 | 1.4427 | 1668.9 |
| 480 | 1299.54 | -180.92 | 280.78 | -1.5434 | 1.1135 | 1.4394 | 1658.1 |
| 490 | 1292.26 | -169.15 | 295.16 | -1.5137 | 1.1135 | 1.4363 | 1647.7 |
| 500 | 1285.08 | -157.39 | 309.50 | -1.4847 | 1.1137 | 1.4335 | 1637.5 |
| 525 | 1267.60 | -128.07 | 345.26 | -1.4149 | 1.1144 | 1.4275 | 1613.7 |
| 550 | 1250.74 | -98.828 | 380.89 | -1.3487 | 1.1157 | 1.4226 | 1591.6 |
| 575 | 1234.45 | -69.645 | 416.40 | -1.2855 | 1.1174 | 1.4187 | 1571.3 |
| 600 | 1218.69 | -40.503 | 451.83 | -1.2252 | 1.1195 | 1.4157 | 1552.5 |
| 625 | 1203.43 | -11.386 | 487.19 | -1.1675 | 1.1218 | 1.4134 | 1535.1 |
| 650 | 1188.63 | 17.720 | 522.50 | -1.1121 | 1.1243 | 1.4117 | 1519.1 |
| 675 | 1174.27 | 46.825 | 557.78 | -1.0588 | 1.1271 | 1.4106 | 1504.2 |
| 700 | 1160.32 | 75.938 | 593.04 | -1.0075 | 1.1299 | 1.4099 | 1490.5 |
| 800 | 1108.23 | 192.61 | 734.02 | -0.81926 | 1.1419 | 1.4103 | 1445.3 |
| 900 | 1061.27 | 309.84 | 875.20 | -0.65298 | 1.1538 | 1.4134 | 1412.4 |
| 1000 | 1018.66 | 427.73 | 1016.74 | -0.50386 | 1.1649 | 1.4175 | 1388.8 |
| 1100 | 979.76 | 546.30 | 1158.69 | -0.36856 | 1.1749 | 1.4216 | 1371.9 |

TABLE 35. Thermodynamic properties of carbon dioxide—Continued

| Temperature (K) | Density (kg/m ³) | Internal energy (kJ/kg) | Enthalpy (kJ/kg) | Entropy [kJ/(kg K)] | c_v [kJ/(kg K)] | c_p [kJ/(kg K)] | Speed of sound (m/s) |
|----------------------|---------------------------------|----------------------------|---------------------|------------------------|----------------------|----------------------|-------------------------|
| 800.00 MPa Isobar | | | | | | | |
| 327.673 ^b | 1495.70 | -369.91 | 164.96 | -2.1926 | 1.1961 | 1.5477 | 2052.8 |
| 330 | 1493.71 | -367.02 | 168.56 | -2.1817 | 1.1951 | 1.5457 | 2048.9 |
| 335 | 1489.46 | -360.83 | 176.28 | -2.1585 | 1.1931 | 1.5415 | 2040.7 |
| 340 | 1485.25 | -354.66 | 183.97 | -2.1357 | 1.1912 | 1.5373 | 2032.6 |
| 345 | 1481.08 | -348.50 | 191.65 | -2.1132 | 1.1894 | 1.5333 | 2024.6 |
| 350 | 1476.96 | -342.35 | 199.31 | -2.0912 | 1.1877 | 1.5294 | 2016.8 |
| 360 | 1468.83 | -330.09 | 214.56 | -2.0482 | 1.1846 | 1.5218 | 2001.6 |
| 370 | 1460.85 | -317.88 | 229.74 | -2.0066 | 1.1817 | 1.5147 | 1986.8 |
| 380 | 1453.03 | -305.72 | 244.86 | -1.9663 | 1.1791 | 1.5080 | 1972.5 |
| 390 | 1445.35 | -293.59 | 259.90 | -1.9272 | 1.1769 | 1.5016 | 1958.7 |
| 400 | 1437.82 | -281.51 | 274.89 | -1.8893 | 1.1748 | 1.4956 | 1945.4 |
| 410 | 1430.42 | -269.46 | 289.82 | -1.8524 | 1.1730 | 1.4899 | 1932.4 |
| 420 | 1423.15 | -257.45 | 304.69 | -1.8166 | 1.1714 | 1.4845 | 1919.9 |
| 430 | 1416.00 | -245.46 | 319.51 | -1.7817 | 1.1699 | 1.4795 | 1907.8 |
| 440 | 1408.98 | -233.51 | 334.28 | -1.7478 | 1.1687 | 1.4748 | 1896.0 |
| 450 | 1402.08 | 221.58 | 349.01 | 1.7147 | 1.1676 | 1.4703 | 1884.6 |
| 460 | 1395.29 | -209.67 | 363.69 | -1.6824 | 1.1667 | 1.4661 | 1873.5 |
| 470 | 1388.60 | -197.79 | 378.33 | -1.6509 | 1.1659 | 1.4622 | 1862.8 |
| 480 | 1382.03 | -185.93 | 392.93 | -1.6202 | 1.1652 | 1.4586 | 1852.4 |
| 490 | 1375.55 | -174.08 | 407.50 | -1.5901 | 1.1647 | 1.4551 | 1842.3 |
| 500 | 1369.17 | -162.26 | 422.04 | -1.5608 | 1.1642 | 1.4519 | 1832.5 |
| 525 | 1353.64 | -132.76 | 458.24 | -1.4901 | 1.1636 | 1.4448 | 1809.1 |
| 550 | 1338.65 | -103.33 | 494.29 | -1.4230 | 1.1636 | 1.4389 | 1787.4 |
| 575 | 1324.16 | -73.959 | 530.20 | -1.3592 | 1.1640 | 1.4340 | 1767.1 |
| 600 | 1310.14 | -44.627 | 566.00 | -1.2982 | 1.1648 | 1.4301 | 1748.1 |
| 625 | 1296.54 | -15.319 | 601.71 | -1.2399 | 1.1659 | 1.4269 | 1730.4 |
| 650 | 1283.34 | 13.975 | 637.35 | -1.1840 | 1.1673 | 1.4244 | 1713.8 |
| 675 | 1270.52 | 43.267 | 672.93 | -1.1303 | 1.1688 | 1.4225 | 1698.2 |
| 700 | 1258.04 | 72.565 | 708.47 | -1.0786 | 1.1706 | 1.4211 | 1683.6 |
| 800 | 1211.18 | 189.94 | 850.45 | -0.88900 | 1.1785 | 1.4193 | 1633.6 |
| 900 | 1168.47 | 307.80 | 992.46 | -0.72175 | 1.1868 | 1.4212 | 1594.8 |
| 1000 | 1129.16 | 426.25 | 1134.74 | -0.57184 | 1.1948 | 1.4247 | 1564.9 |
| 1100 | 1092.77 | 545.32 | 1277.40 | -0.43587 | 1.2020 | 1.4286 | 1542.2 |

^aSublimation temperature.^bMelting temperature.^cSaturation temperature.

11. Acknowledgments

The authors are grateful to the Deutsche Forschungsgemeinschaft for their financial support of this project.

12. References

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